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CHANGES IN HELICOPTER RELIABILITY/MAINTAINABILITY CHARACTERISTICS OVER TIME. VOLUME 2. DATA SUBMITTED BY HELICOPTER MANUFACTURERS

Norman J. Asher, et al

Institute for Defense Analyses

Prepared for:

Office of the Director of Defense Research and Engineering Defense Advanced Research Projects Agency

March 1975

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STUDY S-451

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CHARACTERISTICS OVER TIME

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Norman J. Asher John Donelson Gerald F. Higgins

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March 1975

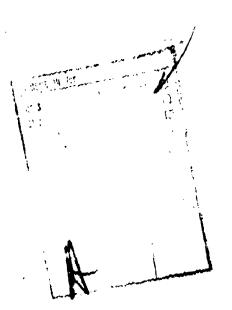
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STUDY S-451

CHANGES IN HELICOPTER RELIABILITY/MAINTAINABILITY CHARACTERISTICS OVER TIME

Volume 2: Data Submitted by Helicopter Manufacturers

Norman J. Asher John Donelson Gerald F. Higgins

March 1975



PROGRAM ANALYSIS DIVISION

400 Army-Navy Drive, Arlington, Virginia 22202

Contract DAHC15 73 C 0200 Task T-105

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Because of the bulk of the Sikorsky reports, only the most interesting sections of them are reproduced in this volume.

^{*}Three pagination sequences are used in this volume: in both Part A (BV-) and Part B (H-), the lower-case Roman and the Arabic page numbers agree with those in each of the documents here reproduced; in Part C, however, the original page numbers of the two Sikorsky documents are displayed as they were submitted (i.e., centered at the lower edge), but with our single continuous (S-) pagination also indicated (in the lower unbound corner of each page). For the reader's additional convenience, Part B (Hughes) and Part C. II (Sikorsky) are printed on paper of a different color from that used for Part A (Boeing Vertol) and Part C.I (Sikorsky).

Part A

Data Submitted by Boeing Vertol

RELIABILITY GROWTH ANALYSIS - FINAL REPORT

Prepared By
J. J. Dougherty, III & O. L. Sandora
THE BOEING VERTOL COMPANY
P. O. Box 16858
Philadelphia, Pennsylvania 19142

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for
INSTITUTE FOR DEFENSE ANALYSIS
Program Analysis Division
400 Army~Navy Drive
Arlington, Virginia 22202
ATTENTION
Mr. Norman J. Asher
Ass't Division Director

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FOREWORD

This report presents a study to identify Reliability, Maintain-ability, and Safety Growth Trends on helicopters. The work was conducted under Contract Number P. O. 20478 for the Institute of Defense Analysis (IDA), Arlington, Virginia.

IDA technical direction was provided by Mr. Norman J. Asher.

Project Engineer for the Boeing Vertol Company was Mr. J. J. Dougherty, III of the Product Assurance R&D unit. Principal Investigator for the study was Mr. O. L. Sandora, also of the Product Assurance R&D unit. Program Management and Technical Direction were provided by Mr. K. G. Rummel, Manager, Product Assurance Research & Development.

1. INTRODUCTION

Helicopters have consistently exhibited relatively high unscheduled maintenance requirements because of the great percentage of high reliability risk and high-cost components needed for the helicopters unique performance capabilities. This tendency towards high maintenance requirements has generated concurrence among both the contractor and customer that improved reliability must be achieved without a long and expensive period of in-service product improvement. High initial reliability can be achieved only through a well-executed analytical design approach and an enthusiastic and well-controlled developmental testing effort.

The primary reliability effort in the design stage is the analysis and evaluation of the aircraft design and development of Reliability Predictions. Recent work has shown that a point estimate of aircraft or component reliability is meaningless unless accompanied by a quantification of the time in the components maturity (development) cycle for which the estimate is relevant.

Reliability growth prediction techniques have been employed to estimate the number of developmental test hours required to achieve a desired level of reliability with increased confidence in the technology.

However, since reliability continues to be improved by the Product Improvement process throughout most of the inproduction life of a helicopter, it is necessary to understand this growth process. The magnitude and the factors
affecting this growth process must be determined and quantified if future aircraft programs are to be optimized.
Development costs and O&M costs must be viewed as intimately
related to reliability. The key to minimum total system
costs is the understanding of the reliability growth process
through the development and operational phases.

2. <u>DOCUMENTATION OF ANALYSIS</u>

Historically, reliability of helicopters has increased with each new generation of aircraft, as well as increasing during the in-tervice phase of each individual aircraft. In order to understand these growth patterns and the impact that aircraft reliability growth has on mission reliability, safety reliability, availability and maintenance manhour expenditures, an analysis of in-service aircraft data is essential.

This can best be achieved with a compilation of reliability growth experience at the aircraft component level, and the impact on the above mentioned parameters after component reliability is analyzed: then total aircraft reliability should be examined and conclusions drawn concerning the factors affecting this growth process.

The data contained in the following chart identifies all pertinent information developed under this contract and contained in this report.

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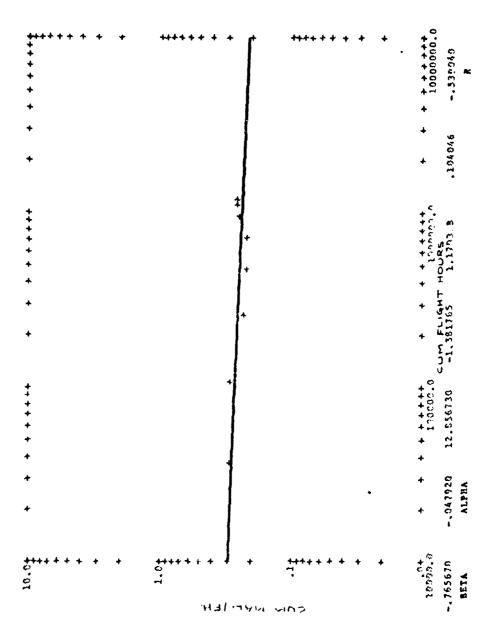
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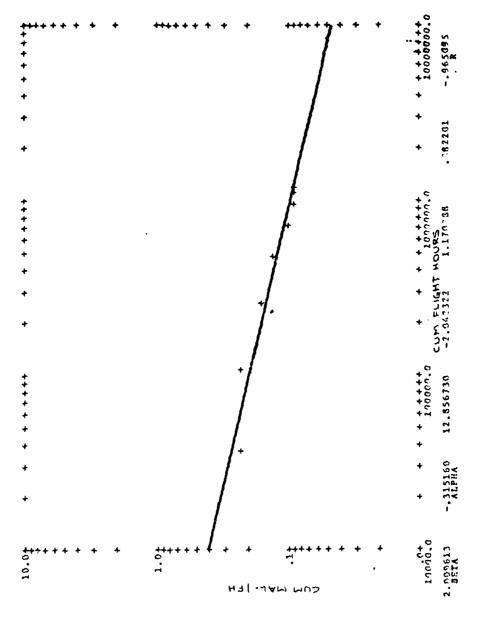
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CH-47 MAL./PH- CUM

FIGURE 1

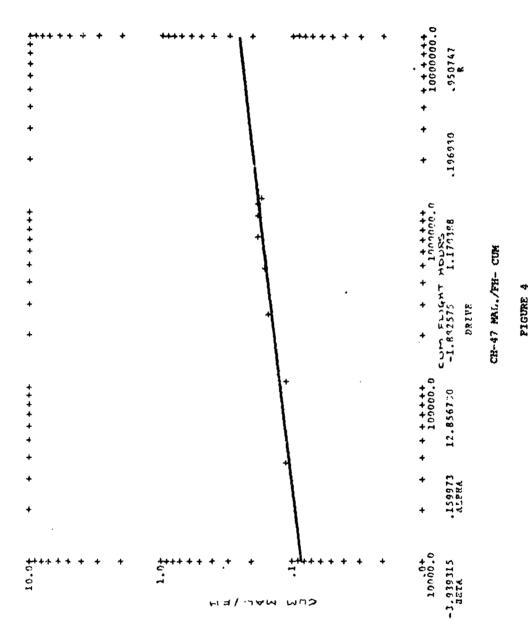
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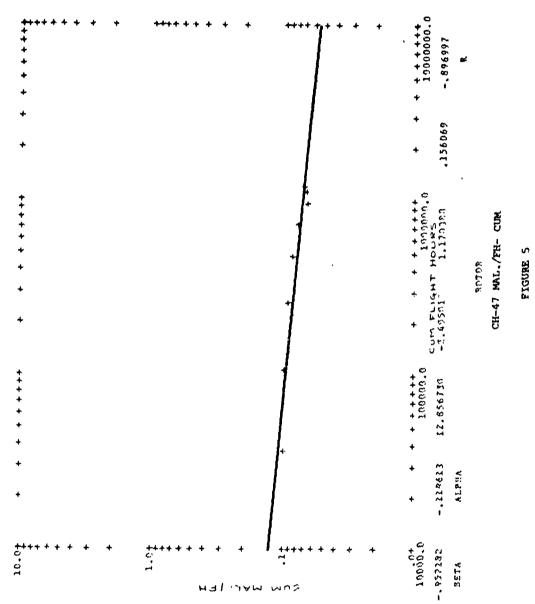


FLIGHT CONTROLS CH-47 MAL, /FH- CUM

FIGURE 3



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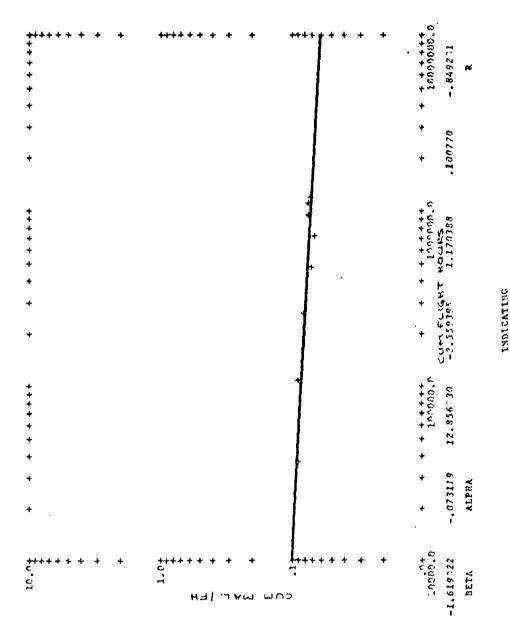
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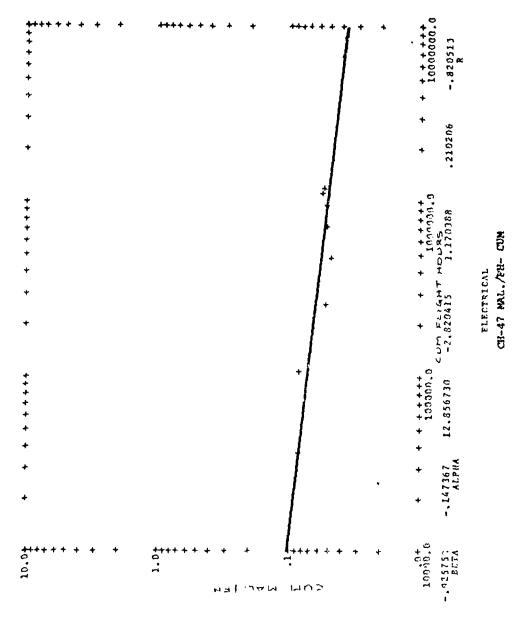
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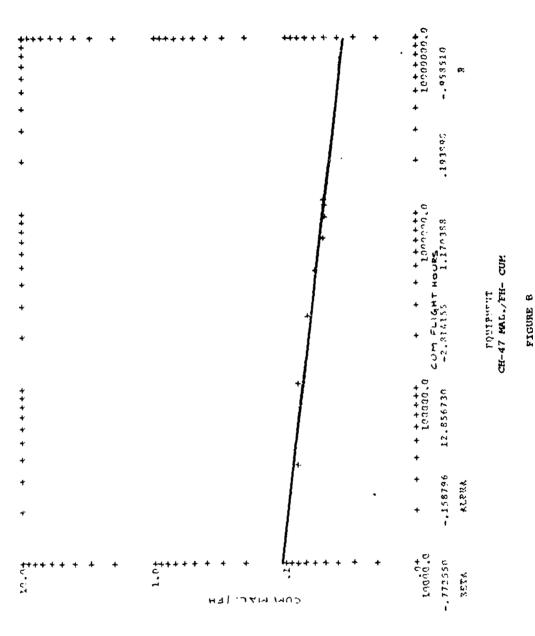
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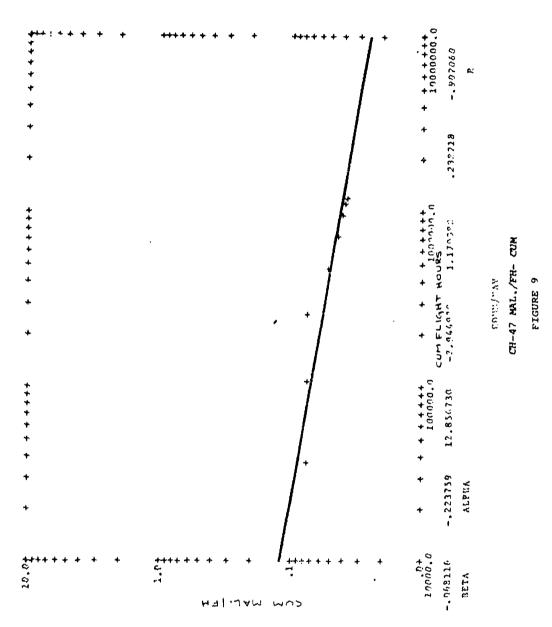
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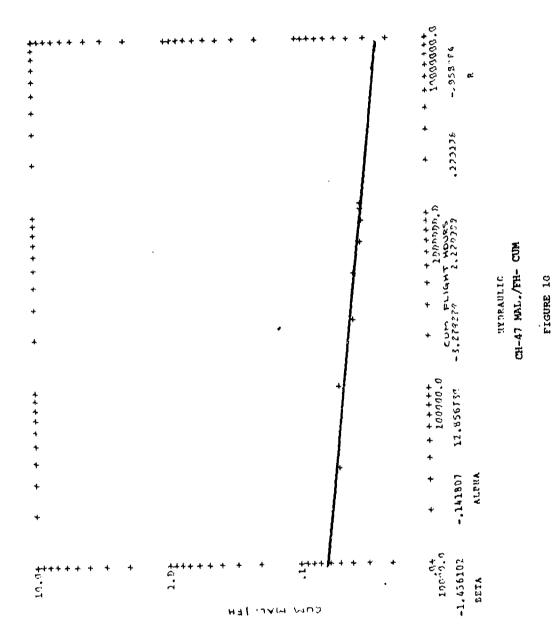
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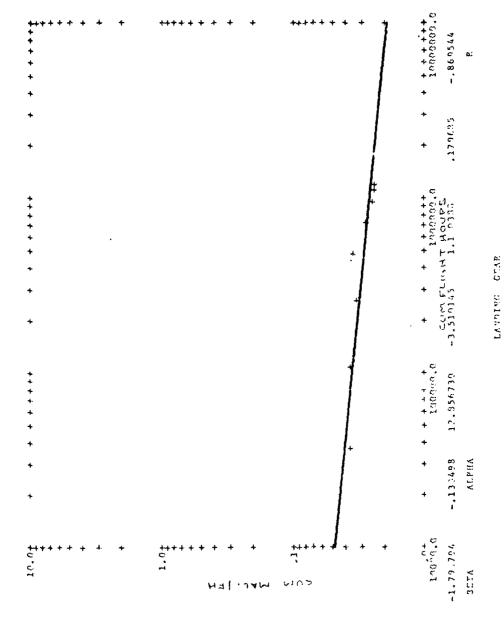




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CH-47 MAL,/FH- CUM

FIGURE 11

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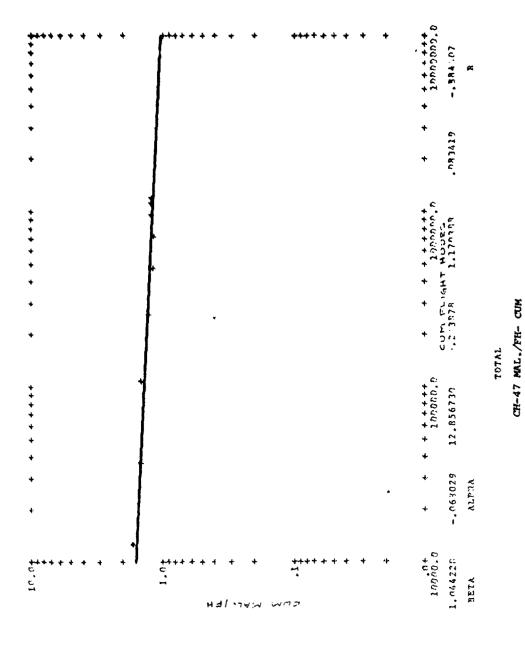
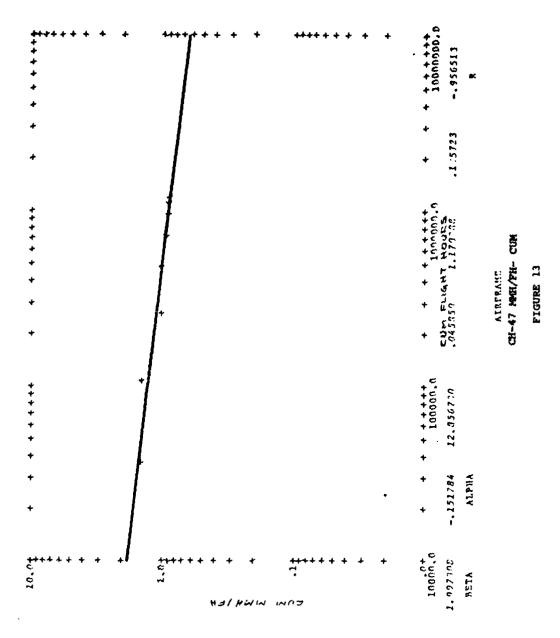


FIGURE 12

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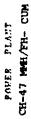
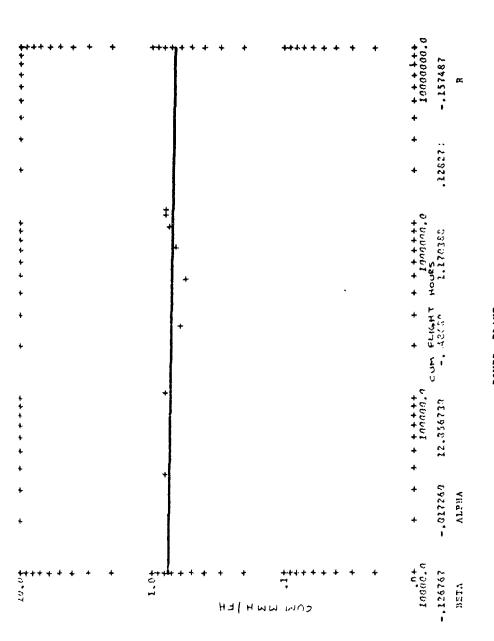
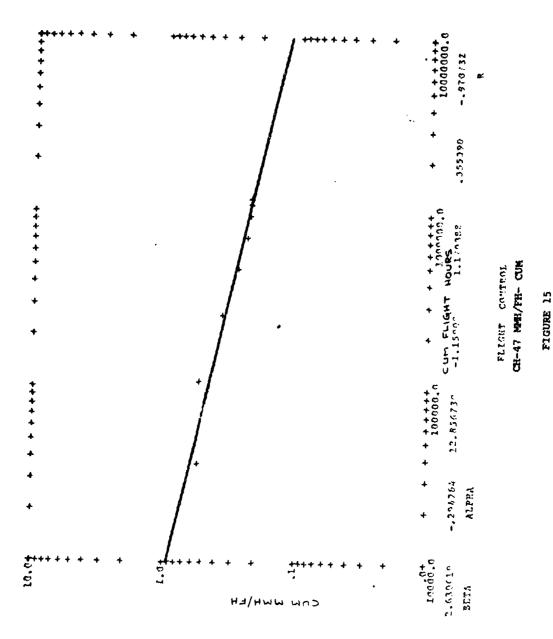


FIGURE 14





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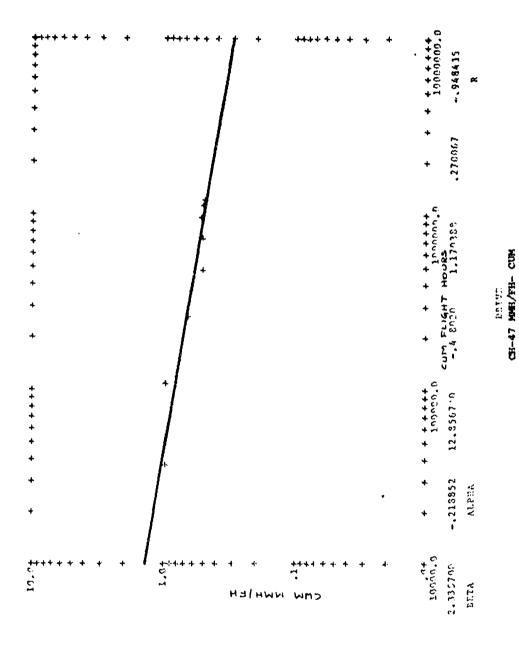


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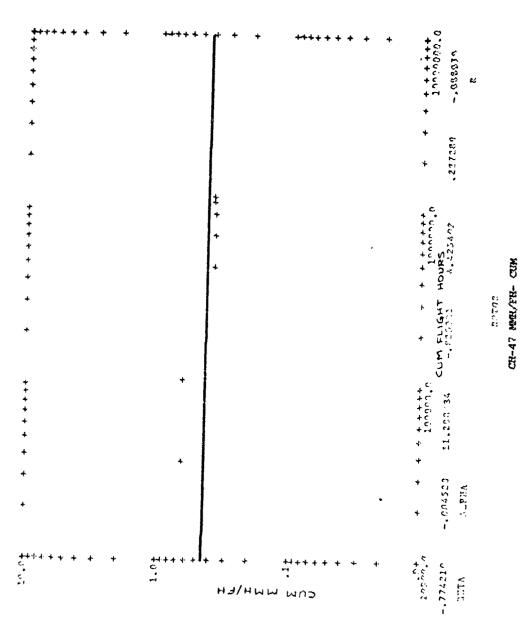
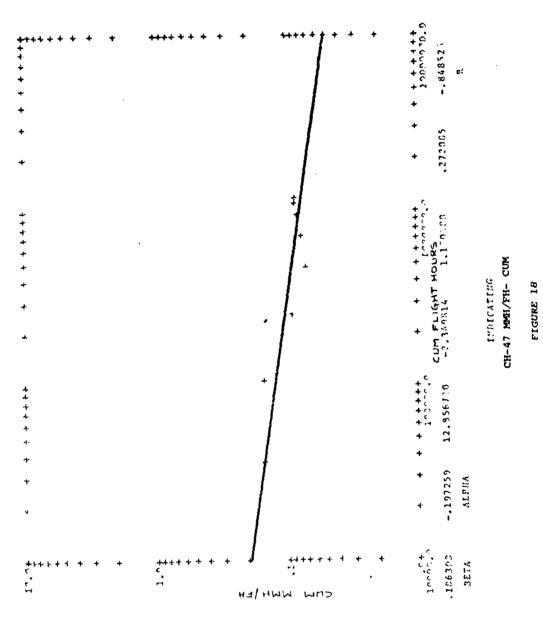


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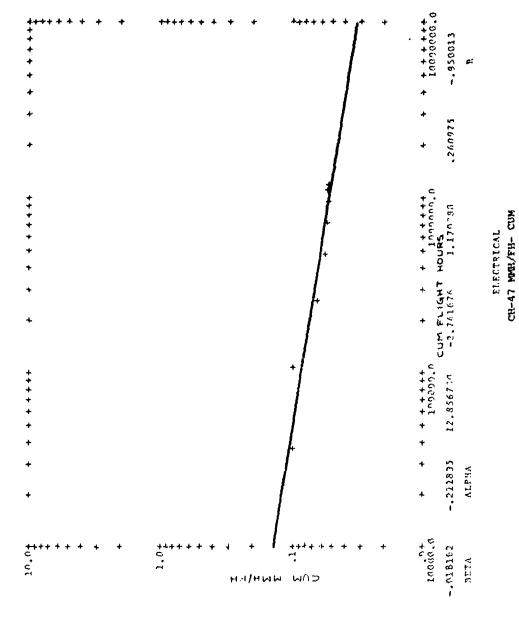


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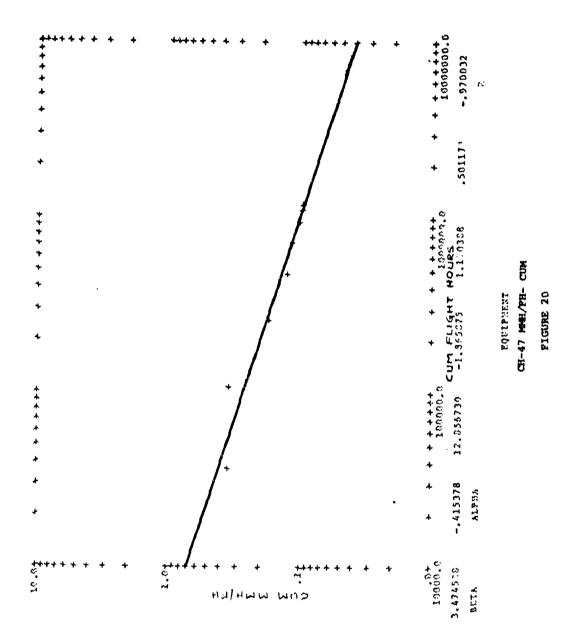
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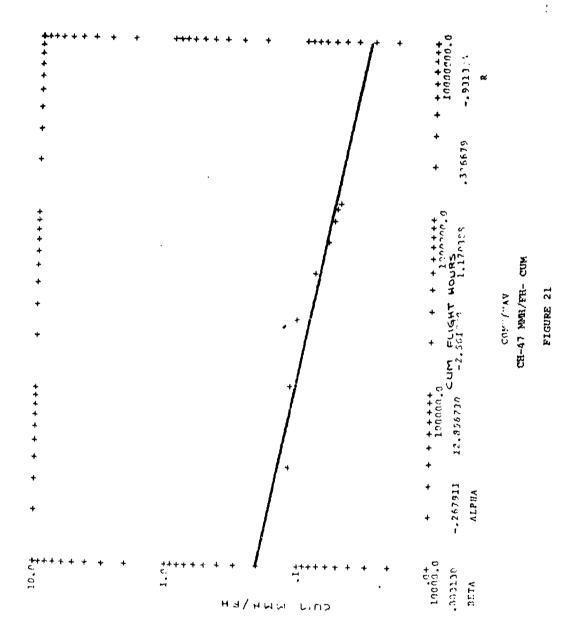
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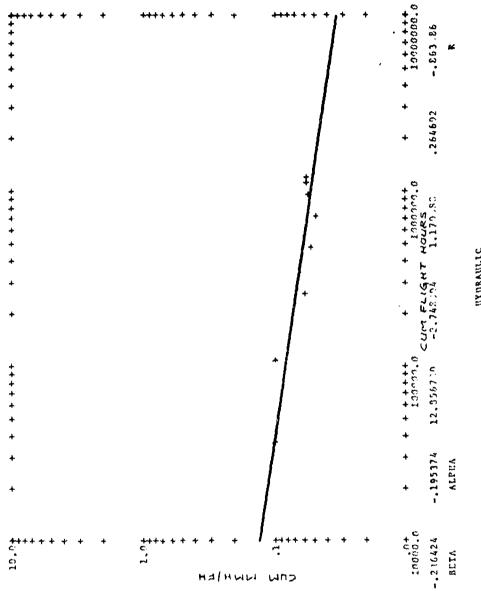
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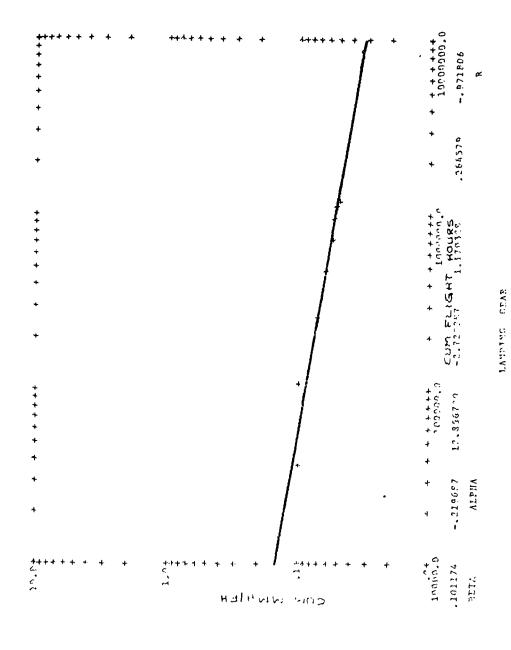
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HYBRAULIC CH-47 MMI/FH- CUM

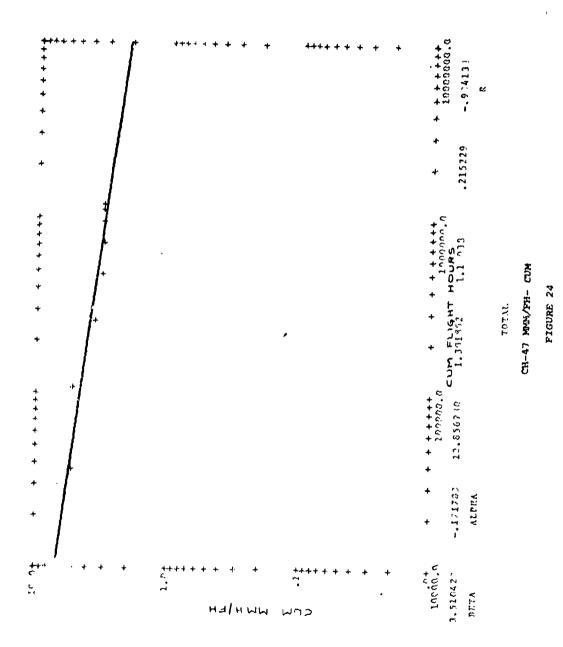
FIGURE 22



CH-47 MMI/FH- CUM

FIGURE 23

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TABLE 2 - CH-47 SYSTEM REH GROWTH parameters

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TABLE 3. SAFETY GROWTH STATISTICS

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0	FLIGHT Hours	141	9,111	2.0.076	32,604	154.462	253,628	324284	428654	287955	612219	188041							nets with 8 10 seats the	ing in a 4500, Minimum speed, 161 in the Mormal Lange.	is t. Graymstems one 53 te	and the state of the state of	800 M 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	SML CTION GALLER CO. P. C.
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	NO. MAJOR ACCIDENT'S	0	2	4	7	23	24	31	37	23	6/	•						ars. Weight 4750 pounds	to teet the very country to the		No. of the last of	r ve sons of the UNITE are the "I" modals	tipler freihors and oight.	LLE GENC US-12
SYAVY/PSTIC	FLIGHT HOURS	141	8,970	26,965	46,523	71,343	99,231	50606	128370	128031	121034	10322					 100 Tag	Alton vehicle vite 8-13 seas	(3/9) to the party of the state of		Pure y user Warne	of the season of the United		::Cn15::
		10.53	1964	1935	1900	1967	1963	6761	02.61	1663	1972	1973						Office of the engage		- 1	, n		A CALL SENSE	NGF.
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	304.5	.74				CUMULATIVE	
	17	FLIGHT	NO. NAJOR ACCIDENTS	RATE/ 100,000 7:1	FLIGHT HOURS	HO. MAJOR ACCIDENTS	RATE/ 100,000 FH
-	1,51	· .	t:	6	~	C	c
	46.2	1,42,72		91.23	1,220		91.83
	1963	13,893	12.	65,23	16,113	13	80.08
	25.7	-33,235		25.42.3	10.075	35	20.16
	1455	37,200		7.2.94	0Z0"23	α:-	55.12
-	1:0:1	589,53	1.	85.7	776.07A	65,	45.33
•	1467	12,827	6	22.04	170,901	80	39.78
~	19:5	3:17611	14	25.31	210,542	32	38.9.
	6961	78181	کر	27.49	228728	28	38.04
	026)	20753	Ś	16,24	184652	76	35.46
~	1651	27500		3,64	186987	93	32.41
	1972	23560	+	86'91	310541	97	31.23
>	(923	26714	•	22.46	337255	103	31.43
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c,	FLIGHT HOURS	NO, MAJOR ACCIDENTS	8ATE/ 100,000 FH	FLIGHT HOURS	NO. MAJOR ACCIDENTS	. PATE/ 100,000 FII
10.03						
969	1822	1		UNK		
3	.;ti	2		CONT	Č.	
1965	23.9(5	.	3.11	30,566	•:	36.47
767	52.5.3	7	21.43	13,626	11	25.21
1963		C	13.65	3,000	20	;
***	3	ن		150.041	26	13.63
1460		Ţ.		27	33	11.95
798	7		Ç (; ,	200 250	Ģ	11.24
754		13	16.15	146,031	5.4	11.81
ž	21	٥		511,537	69	10.67
6961	49 096	+	21.8	600 683	+9	27.00
19 70	78067	0)	12.8/	251819	74	10.90
12 71	69295	=	15.87	748045	35	17.7
1972	88538	9		836583	16	10.87
19 73	56	v	4.4	932253	0.47	(0.73
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CUAULATIUM	NO. INTEL ACCIDENTS	0	13	140	2,7	42.	5:3	587	6.5			
)	<u> </u>	2:8	19,734	239,512		100, 6-1	, 111 Ce4	1.36: 1	191.7.1.			
	111 . 0.00	1.		57.00	49.82	15.46	1.38	36.43	46.5			
	2002.2007	5		1.7		173	(3)	61.	12		Control Control Control	12.7 (2.1
יייים אמאנד				0.00	.17	35	455	136,363	25.794		#10000 0000 000 00 00 00 00 00 00 00 00 0	Charles Married Con-
				1000	1961	MA	12.57	71.0	16.72			1 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3

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	COUNT - MANY	2	- 1 × ·	445	135,321	155		452,006	561,110	935	871	737	228	625	650	532	634	201	•					
س	5 \$	**	8	168	135	300	160,	422	561	(65)	160,	,658	940,	1032	1 6 15 1	1,33	9611	1 50 7		~~ ~~	~~		 .	
	RATE/ 100,000 EH	51.25	79.69	72.43	68.84	63.28	61.35	5.1,33	57.10	54.73	\$2.43	50.00	\$6.63	33,110	48.75	40.4	7.5.4.25	48.34						
CUMULATIVE	NO. MAJOR ACCIDENTS	18	38	122	162	190	221	247	265	278	284	790	662	3:00	302	335	336	303						
	FLIGHT	35,116	100,382	168,423	235, 321	300, 233	360,208	10 018 918	1,00,363	5:17,911	541,925	575,357	509,670	612,682	619,438		631,856	531,438						
	RATE/ 100,000 FE	51.25	94.99	51.73	59.79	43.13	57.68	46.2.1	7.2.2a	29.17	17.63	17.64	38,00	750	34.74	7.75	20.4	7						~
> 4	NO. MAJOR ACCIDENTS	18	6.3	42	0.5	28	3.5	26	13	13	\$	Ş	ě	~	^;	Pri	~ 1	ڹ						. •
AVEN OI-H	FLIGHT	35,116	65,236	68,011	95, 85E	64,912	59,375	56,112	47,013	92.23	34,014	33,532	27,313	25,733	5.7.7		4.7.3	21:11						
	ند	1.952	1853	1954	56.75	1933	10:7	5261	6202	1930	Ž	3	3	*	Ĩ	ž	*	55				~		
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	₹ ×	36.	o a o	· _	

TABLE 3-6

FOX.	ARNY E ANGELE RES	1011	4,403	26,483	10,00	127,847	525, 523	379,011	476,744	23 23	深	254,213	(10,36	श्र	25/15	\$25 000	\$29/224				
	RATE/ 100,000 FH	90.17	75.58	68.84	53.25	43.45	<u>-</u>	Ì	15.43	34.3.	33.37	32.53	30.92	19.25	28,11		27.75				
CUMULATIVE	NO. MAJOR ACCIDENTS	1	2	Ġ.	20	32	46	. 5	66	73	62	84	26	5:3	3.6	99	R.C.				
>	Shure	1,109	2,645	13,069	37,554	73,542	119,069	3.7.335	(1) ed	202,762	53,486.2	258, 1:3	274,132	2.13,614	870 0	317,72	\$3. 8CM				
6	100,000 FH	99.17	65.23	67.23	44.32	3 1	33.63				23, 63			``	C						
SAE	NO. MAJOR ACCIDENTS	7	1	7	11	1.2	1.1	15	10			15.	2	<u></u>	C	ī	M				
H-21 A/B USAF	FLIGHT SHOURS	1,109	1,537	17,423	553.53	26, 459		35. 55	1-					77.77							
	ď	1953	1934	25.67	11	37.67		0	3	75	177	1.25		59	3	~	35		 - ;~		

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	ACCISIMIS	100,000 sm	NATORE TO THE SECOND	NO. MAJOR ;	RATE/ 100,000 FH	AIRFORCE N
	6	·	1,757	0	0	4,403
***	1		:3,024	Ą	:3.6%	26,483
7 4 (2	Σ)	62 (.	10,213	1.2	36.12	17,07
45,135	33	7.7.	5 4 27	(3)	40.75	152,54
	52		70%		55.03	20,02
267.00		() () ()	33,32	200	57.7.	374,9
V66 189	22	£3.12	203,272	15.0	51.67	436,284
27,730	35	17.5	3.7. 3.7.	382	54.73	577,370
	ž	**************************************	437.55	22.5	50.25	568351
M (2) (6)	£ 3	03.50	535,033	271	54.63	754,213
.51	17	2.5.	622,525	283	74.31	810,361
25,165))	*2.54	435,895	2157.5	53.53	825,053
	m	22.05	571,124	301	52.73	1871,137
12, 33	·	57.59	503.257	308	52.30	126°006
10, 154	2	19.53	503,821	310	52.20	357,72
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TABLE 3-8

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•	Com arms &	260,133	487,296	762,30	1063364	1381490	1699211	201 4780	2,322,630	16/9 307	72.861 ,777	34.7.207		•					
	RATE/ 150,000 FH	53.66	39.73	30.27	26,23	25,37	26.53	\$\$	E :	23.5	90.02	25,32	_						
CUMULATIVE	NO. MAJOR ACCIDENTS	\$\$	76	\$ 6.	307	327		2.5.6		163	174	607	~						
0	FLICHT HOURS	37,836	193,293	192,501	404,703	524,630	503, 322	1 24 72 1	6.67	722,673	753, 101	6,							
	RATE/ 100, 300 EH	51.44	29,75	16.04	n : : : : : :		1.7 TM			6.	12.21	5.							
	NO. MAJOR ACCIDENTS	45		13	13	٧.5 ٢		1.5		* 7	(2)	7							
H-3+ ARMY	FLZGRT HCURS	37,32,	234,103	232,212	102.01	97,730	12,533					767.128							
	ئ	22.	141	0.76		. 62	1963	165	24	19061	196	3.6							

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	Fill Care Care	3780	26 98 3						 	·	ا۔	_		285177	3067207				Ì	-	-			
	HATE/ 100,000 FH	-	43.17	30.37	ري. د	27.7.		, ,	12.25			16.22	10.75	16.25	15.92								-	
CURTINETUE	NO, MAJOR ACCINENTS		17.	32		3.2	301	121		7.2.7	217	נינ	302	338	364		-		-					
	FLIGHT	1.5.5.5	\$5.40		1.17:21		£54, 127	**************************************			1,2,3,517	1 1 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	. 2. 2.563	500	3.243.973								1	
	100,000 ER							77 2 3				17.0	(: ,		23.33							:		-
	TO. MAJOR ACCIDINES	, .	1	31				3.2	27		C;			22	22									
	FLIGTT 177 AS			1						,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			6.		257.757							!		
	ë	35	950	1957	1961	653	15/25/	776	1962	1963	19.55	5961	1966	1961	1968		1	:		!	į			. !

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TABLE 3-10

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	H-37 (NAVY)	(NAVY)				CUMULATIVE		,
	CY	FLIGHT	NO. MAJOR ACCIDENTS	RATE/ 100,000 FH	FLIGHT	NO. MAJOR ACCIDENTS	RATE/ 100,000 FH	Service of the servic
됬	1955	0	0	0	c	c	e	
~	1954	16.2	0	O	231	0	c	•••
	1957	2,338	3	106.08	3,025	3	99.17	•
	2953	7,171	S	111.56	10,196	11	107.58	16 360
	10.30	10,739	5	16.53	20.046	15	75.38	37574
	1869	326'6	23	33,19	22,084	ā(34 45	20,697
	17.61	10,03	1	2.35	10,674	20	39.33	\$5577
-~	2552	6,672	2	21.65	35.35	22	44.37	EN NO
	2963	8,230		22.10	57,509	53	50 46	428,187
	1964	8,374	3	17.15	68,783	2.	10 51	155,904
٠,	1963	5.875	Q)	71.738	25		173926
	·	7,332	¢	ę.	750,050	2.5		185379
	7	1,527	2	,	77,517	26		イネガス
پ	1968	C)	0	,	77.617	- 26	53.49	188,884
			}					

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	E	-							106753	13.836	$\stackrel{\sim}{\Box}$				183301		304639	166407 0	<u> </u>	T	<u></u>
	RATE/ 100,000				49.65	16.25	29, 39	26. 77	11.24	33.63	34.15	31,31	29.72	28.51	23.03	29,04	28.48	18.40			
CUMULATIVE	NO. NAJOR ACCIDENTS					4	6	12	B.	25	3.1	32	32	33	3.6	95	3.6	36			
	FLIGHT HOTES				6,16-1	16,548	19,733	523.55	(9) (:	27, 235	30,223	152, 188	109,009	115,725	121.267	123437	126422	(26779			
	RATE/ 103,000 FH				46.58	000	7 1 2 7	2::3:	.7.3.1	52.13	27.75	3.35	ō	15.60	18.0%	74.80	0.00	80			
	NO. MAJOR ACCIDENTS				m	~	~1	/*,	Ų.		ý.	<i>(</i> =4	Ü	-1	1	7	0	0			
(ARNY)	FLIGHT				6,164	20.201	15.27.15	5 6 7 7 7 7	f	2.70.52	16.00	11,967	7.125	6,416	5,542	2670	2485	352			
CH-37 (1	1355	. 956	E. S. F.	7	20-1	55.0	1301	1:62	. 263	800	3365	3965	296.	963	1969	1970	197			
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TABLE 3-12

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	::0/11::	TH/CH-46 ALL MODELS			S	CUMULATIVE	
	λ	FLIGHT	NO. MAJOR ACCIDENTS	л АТЕ/ 100,000 гн	FLIGHT	NO. MAJOR *	RATE/ 100,000 FH
	160						
٠	14						
,	6061	125	0	0	£ 125	0 521	0
	. 9	3, 345	1	29.89	4.3470	1 954.5	28.81
• •		19,535	С	0	15.2 t	13,025 1	4.34
	6	3 772	81	10.23	CU % 4	70.533	12,75
	7	0 1 2	2.2	29.13	750 71/ 62	15 510 31	21.22
	17.	1117	25	17.63	100	25 30 94282	19.45
	1759		5.6	16.37	P. 14. 254	7. 8 6 9 6 1275	38.53
	197	132.757	1.1 #	15.25	94 541110		4.63
•	11.61	251.601		76.57	690,500	0 7 7	15.92
	111	0:0	11	4.18	786,460	1.11	61:41
	147		7	ر. ، ، ،	6. 460	121	13.58
	4 670	Exc. 1, 5 3R1 311	ASE (1 6 1) 1				

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146 151	: ::::	SEDIA:	NF-JOR SINECIES	1100,000 TH	Though Hows	NO. MAJOR ACCIDENTS	
1	1961			0.00	3.15	انه	0.0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1.962		3	35.0		U	0.5
1	1,463			-2164		- ,	172.
126 127	3		. •	436.34		ادا د	#
1466 11.00 1.00	5.6			200	. [27.
19	1766				-	٠. ٢	ก
13 24 25 25 25 25 25 25 25 25 25 25 25 25 25	14.07			6.0	753,603	۲,	7
973	40	1	٠,	1.811	47	13	
120				77	724.53	٠. ح	Į
(47) 1.5 2.4 (F 11) 2.7 11.2 2.4 (F) (7.2 2.4 (F) (7.2 2.4 (F) (7.2 2.4 (F)	3,5	6 7 2		152.91	1 0 0 1 7 9 6	101	
000 257.7.2.1 1.7.2.1 Bo	11.01	2.	84		1,120,500	1. 7.	۱, ع
1.52 1.542. 180	(3)	-		2.64	1,196,200	. 29	81:31
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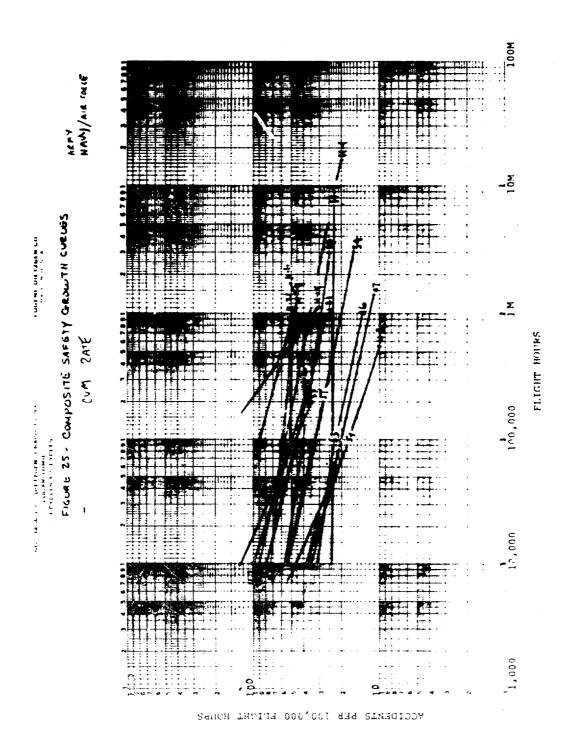
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č	En en contra de la contra del la contra de la contra del la contra del la contra de la contra del la con	10. MAJOR ACCIDENTS	PATE/ 100,000 FH	FLIGHT	NO. HAJOR ACCIDENTS	35TE./ 100,000 FH
13.6.	636.6		17.750	2,753	1	36. 50
15:41	041.7%			21,523		13.93
~ %	3) ::23	- 13		51186	ກ	25.29
	<u> </u>	8	20.22	802,08	21	23.27
1970	106	7	4.94	116334	23	20.85
160	62	"	13.70	154/32	29	18.88
103	- -	4	258	200846	33	6,43
1973		11	25,02	244 815	44	17.17
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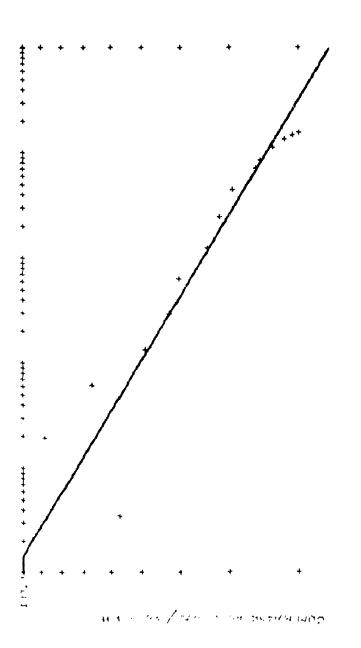
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175.90 2,711 2 175.90 2,711 2 17.10 3,710 3,711 2 17.10 2,710 3,710 3,711 3,710 3,711 3,710 3,711 3	11:15 0 11:15 0 11:	10.90 2.711 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	21:2:10	2000 1000		Forest Trans	NO. MAJOR ACCIDENTS	RATE/ 100,000 FH
2 13. 2. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3. 3.	19: 90 3,711 2 19: 40 7, 216 3 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2/3/6			1, :: ,	2	=
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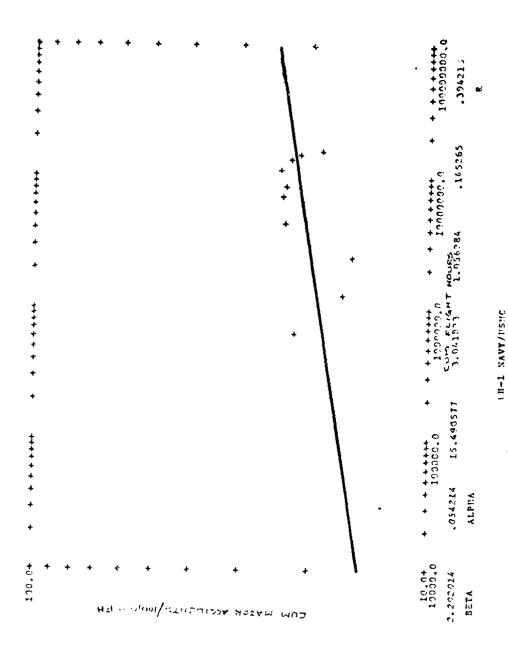
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FIGURE 26



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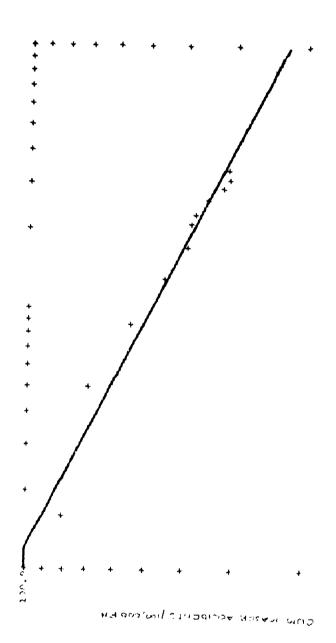
FIGURE 27

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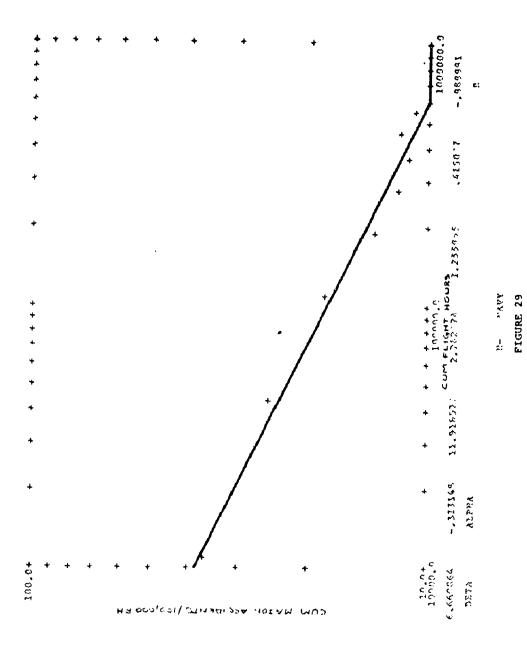
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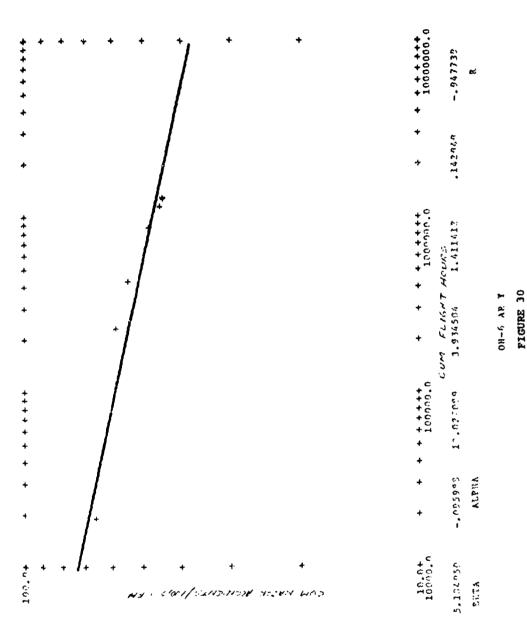
"-2 SAYY FIGURE 28



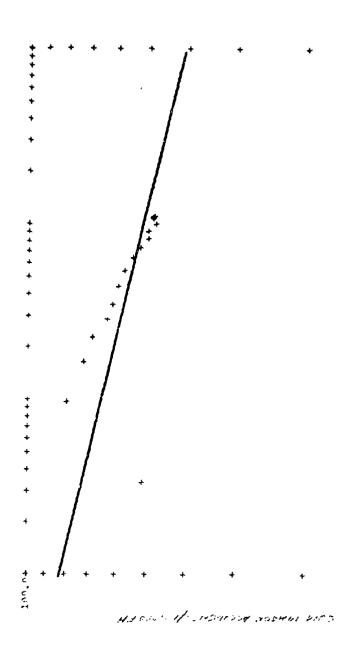
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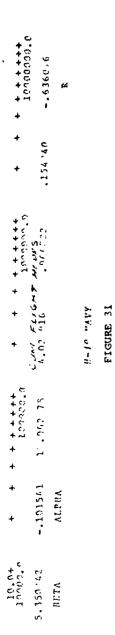
BV-51

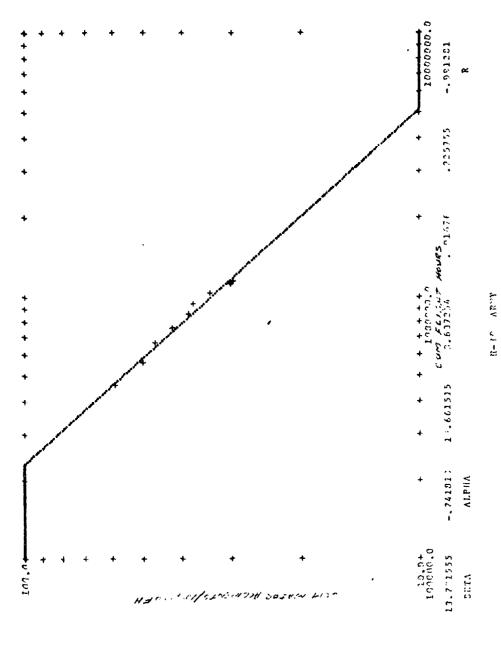


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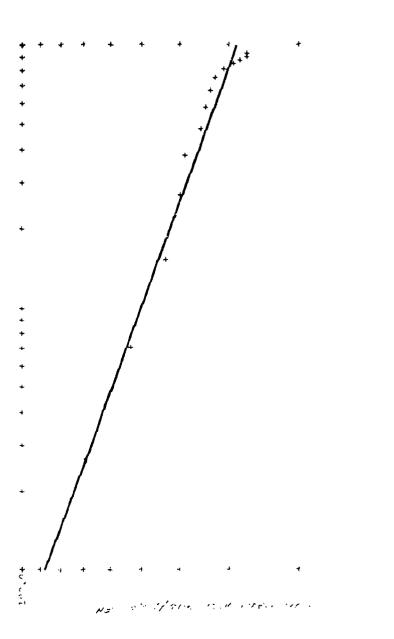


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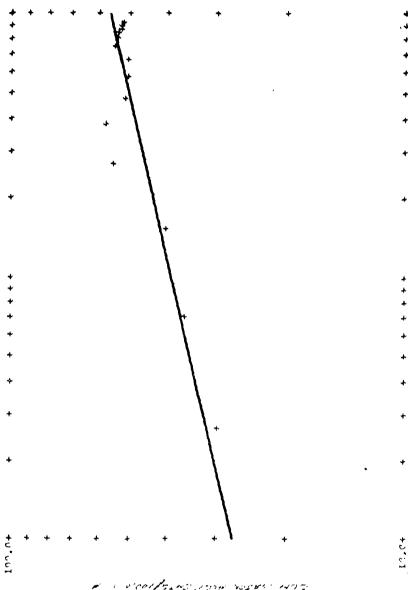




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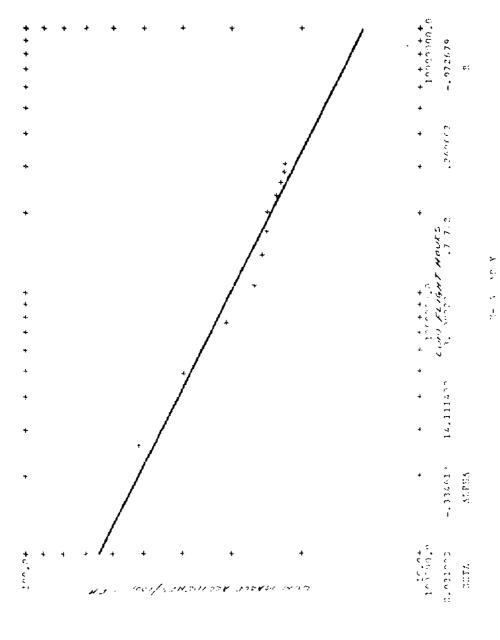




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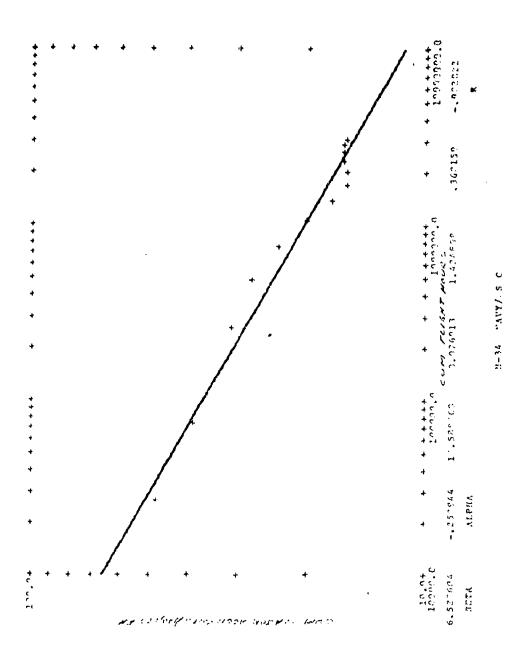
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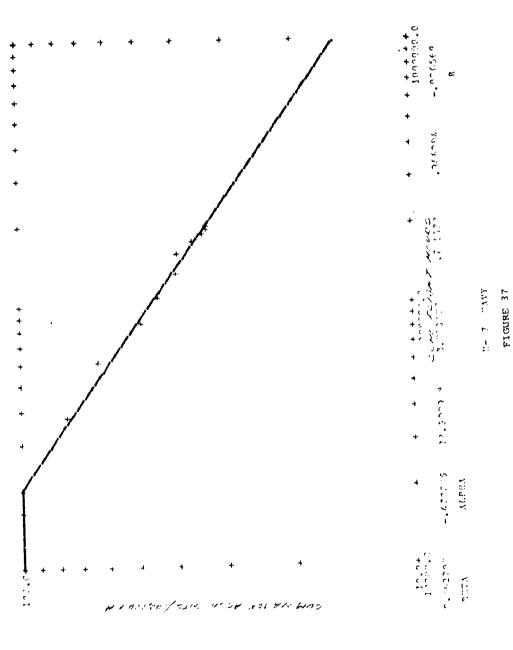


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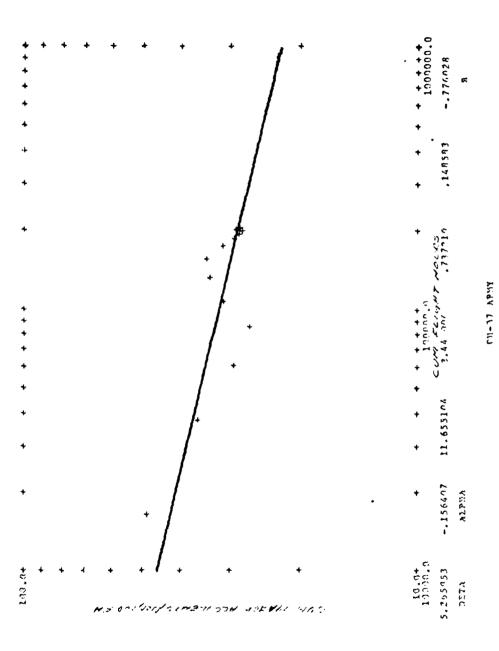
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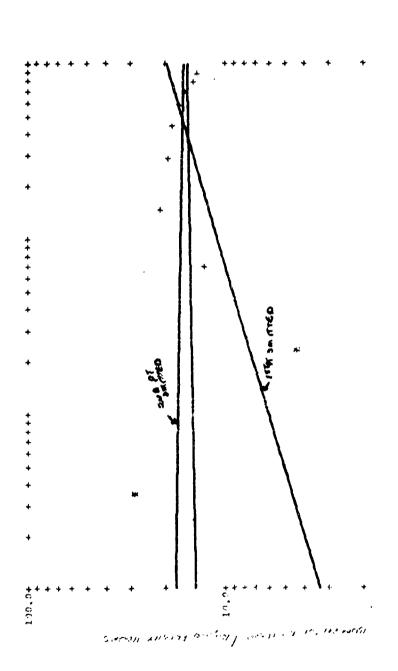
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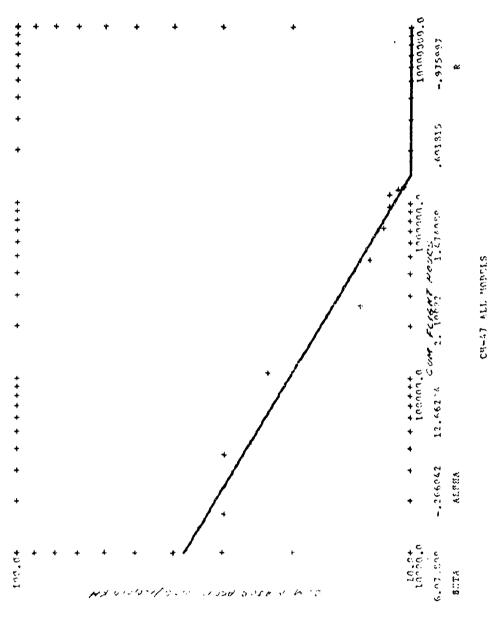
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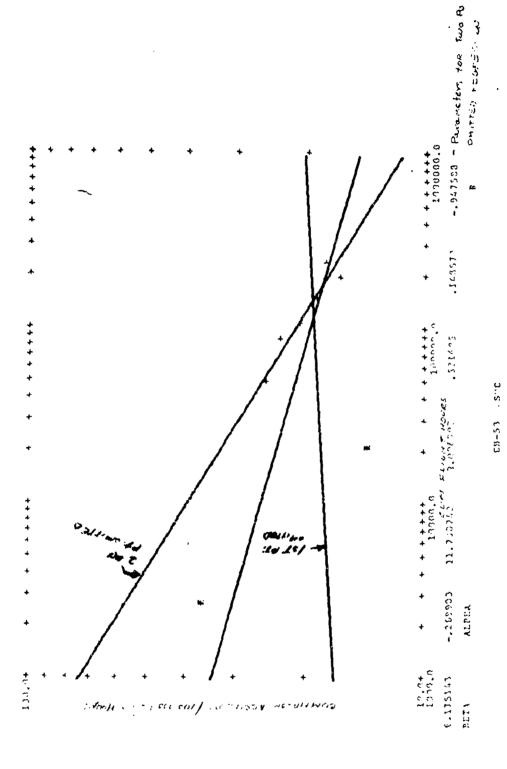
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FIGURE 39

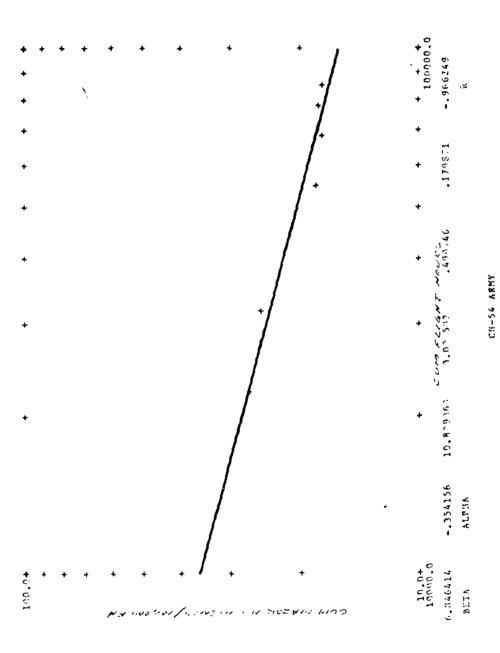


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FIGURE 42

SAFETY GROWTH PARAMETERS

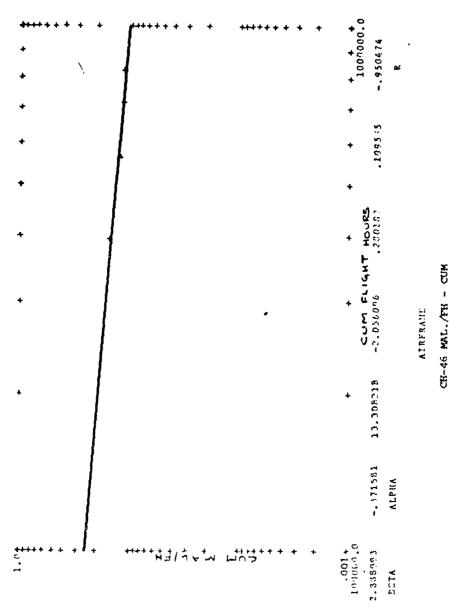
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H-2 NAVY	7.796		.339	978
H-3 NAVY	6.661	١	.327	066
OH-6 ARMY	5.185	١	960.	948
H-19 NAVY	5,350	<u> </u>	. 102	-,636
H-19ARMY	13, 772	1	. 742	166
H-21 A/B USAF	6.706	1	.243	982
H-21C ARMY	1.848		.158	906.
H-34 ARMY	8,031	1	,335	973
H-34 NAVY JUSING	6.528	1	.254	983
H-37 NAVY	9, 362		.479	766
H-37 ARMY	5.266	<u> </u>	.156	776
UH/CH-46 MORCH	2,985		370.	-,073
CH-47 ALL MODER	6,019	1	.266	976
CH-53 USMC	6.175	1	.270	. 948
CH-54 ARMY	6.846	1	.354	996

BV-65

TABLE 4

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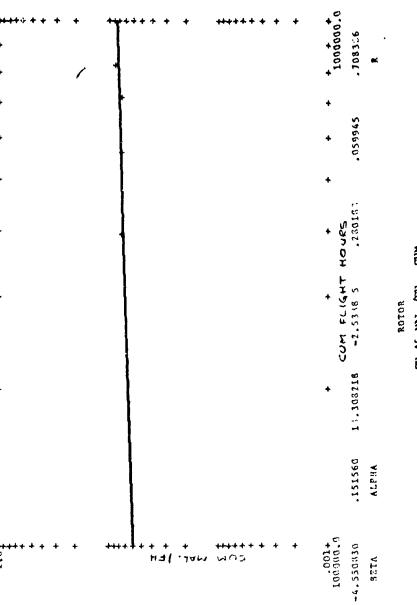
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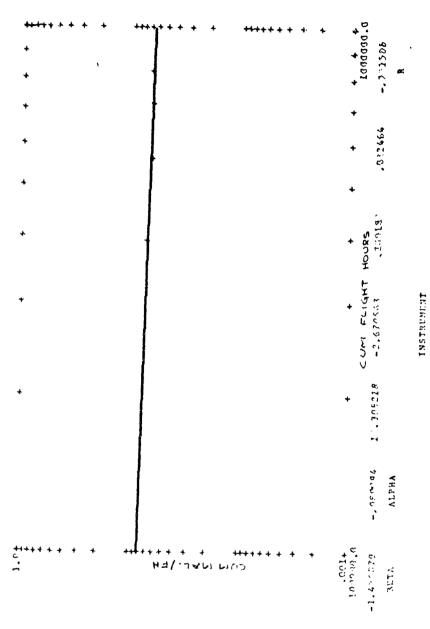
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BV-67



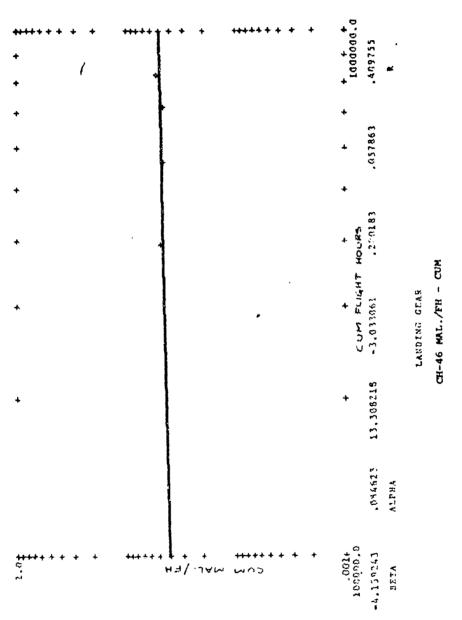
CH-46 MAL./FR - CUM

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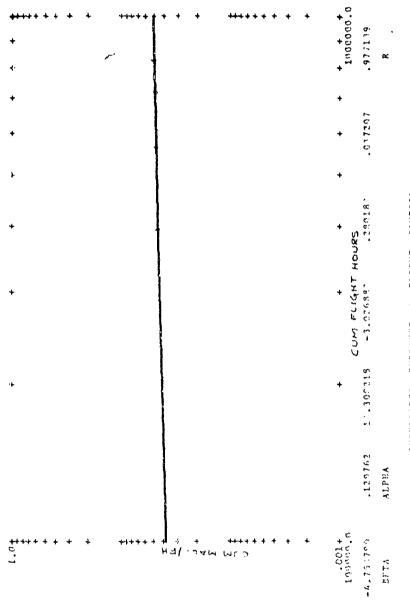
CH-46 MAL./FH - CUM

147-19



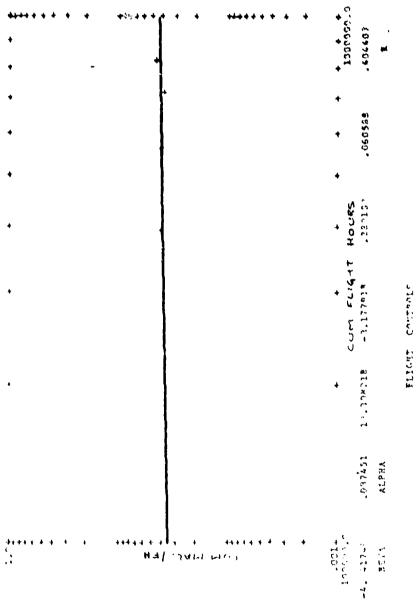
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BV-70



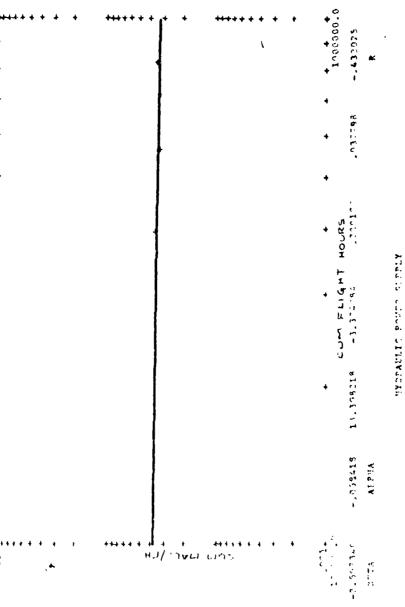
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CH-46 MAL./FH - CUM



CH-46 ML AH - COM

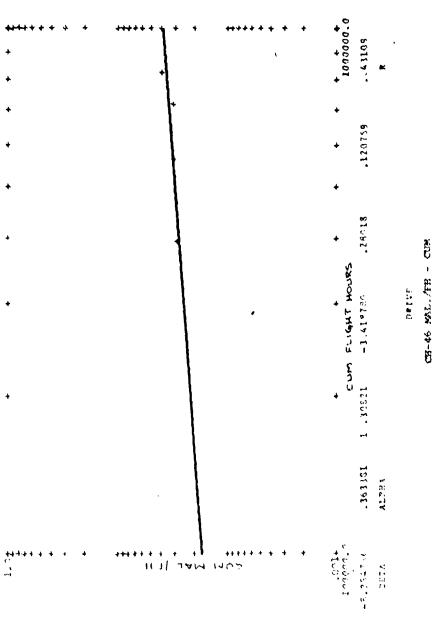
FICURE 48

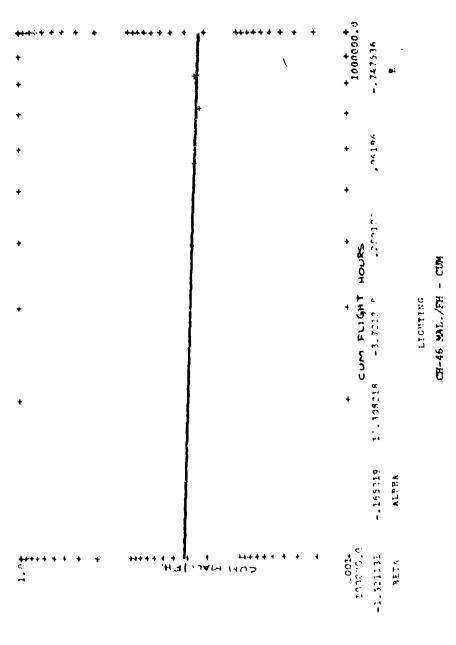


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CH-46 MAL. /FH - CUM



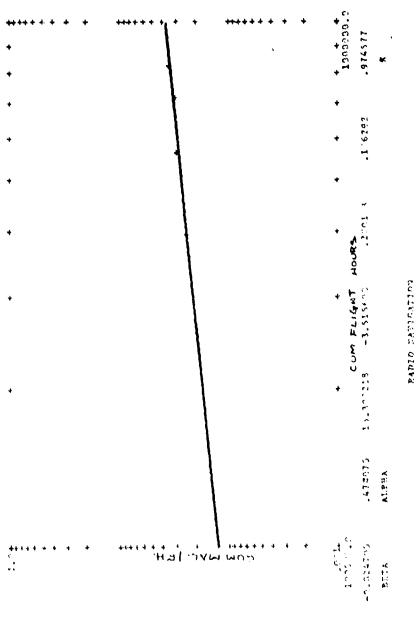




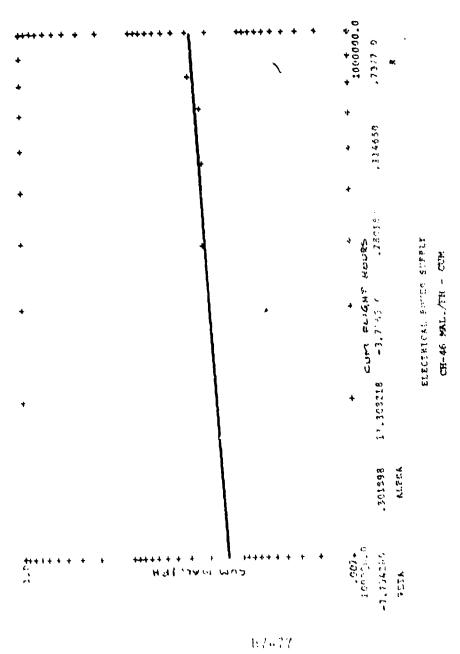
PV~74

FIGURE 52

CB-46 MAL./FH - CUM



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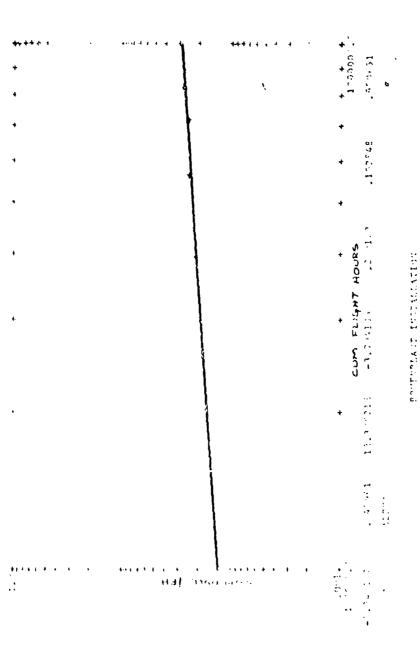
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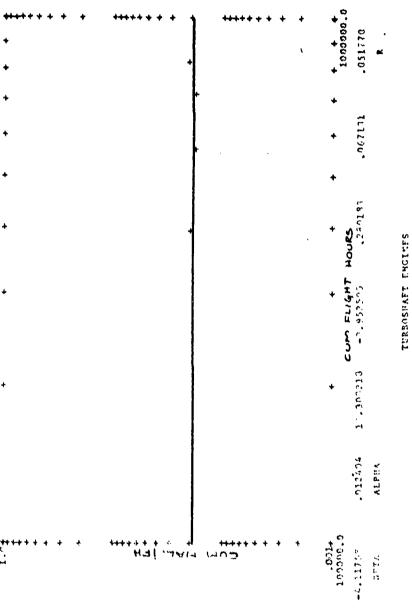
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PIGURE 53









CH-46 MAL./FH - CUM

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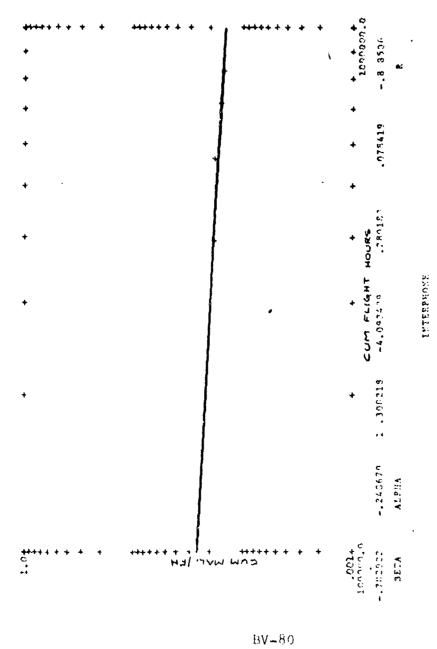


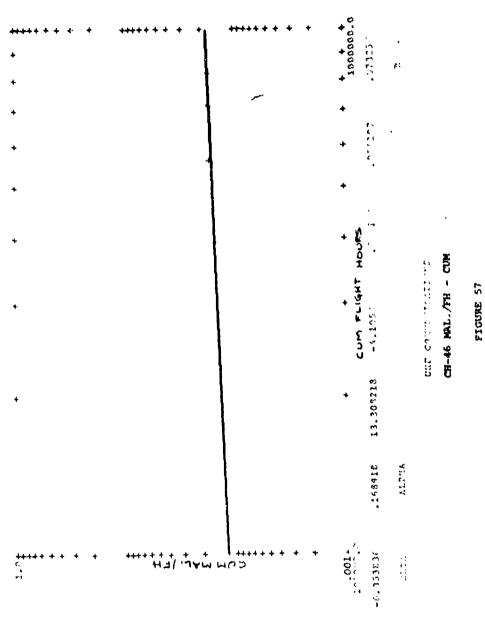
FIGURE S6

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CH-46 MAL. /FH - CUM





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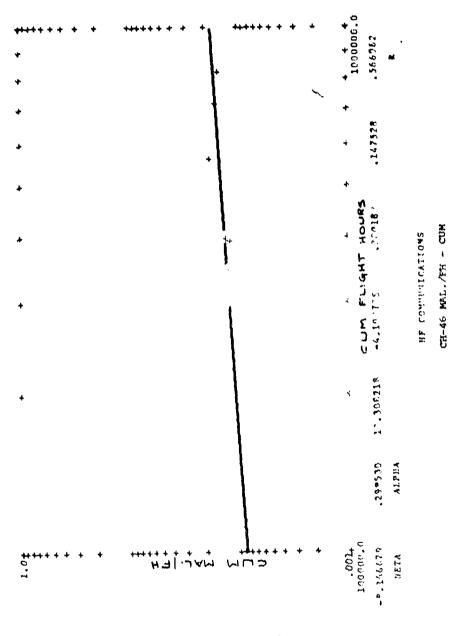


FIGURE 58

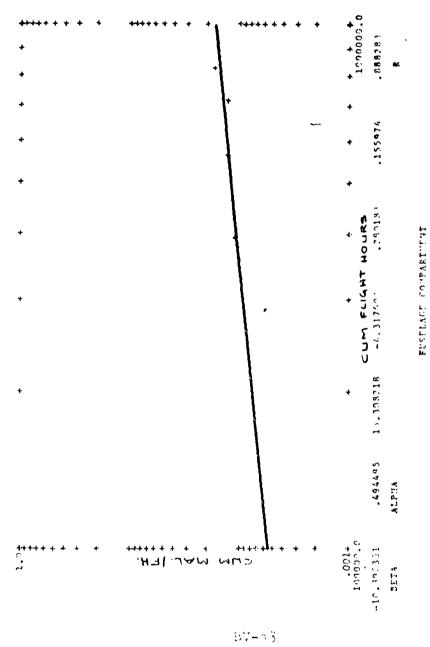
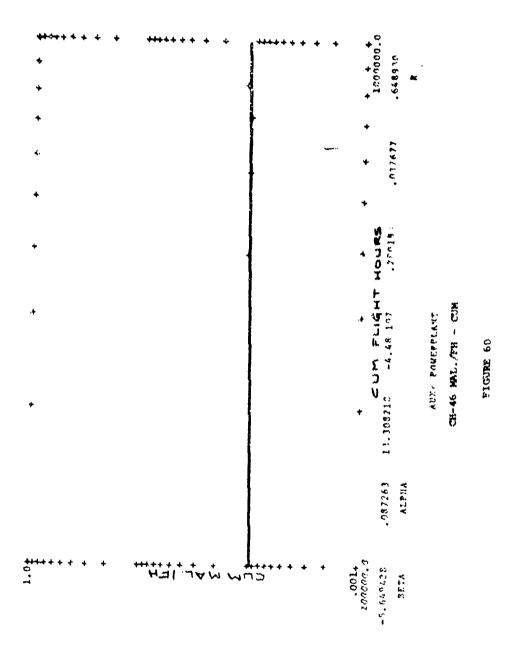


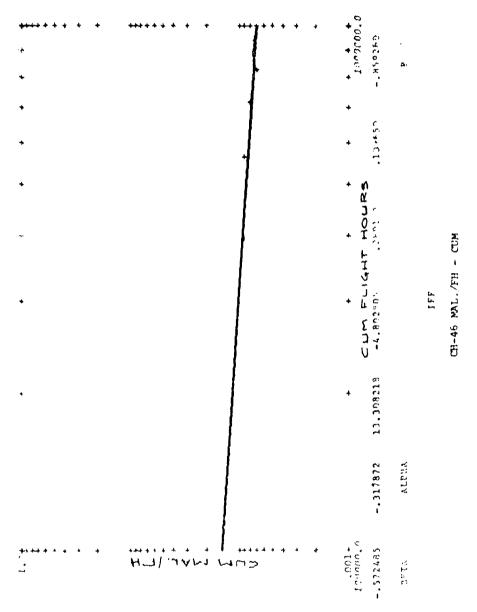
FIGURE 59

CH-46 MAL./FH - CUM

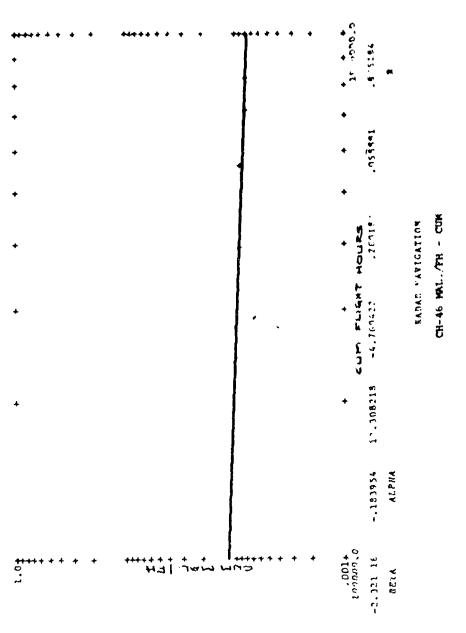
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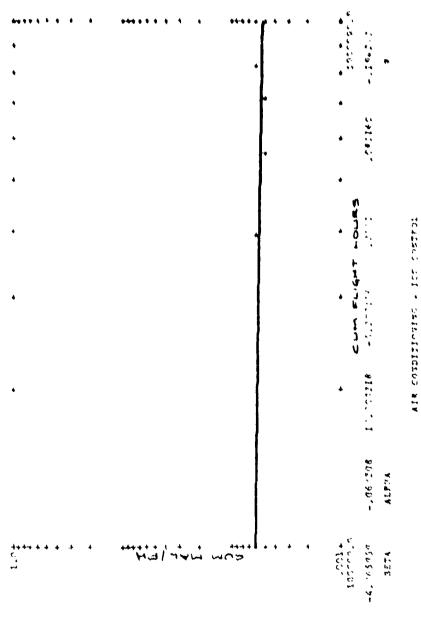


FIGURE 63

CB-46 PAIL 'T'I - CCH

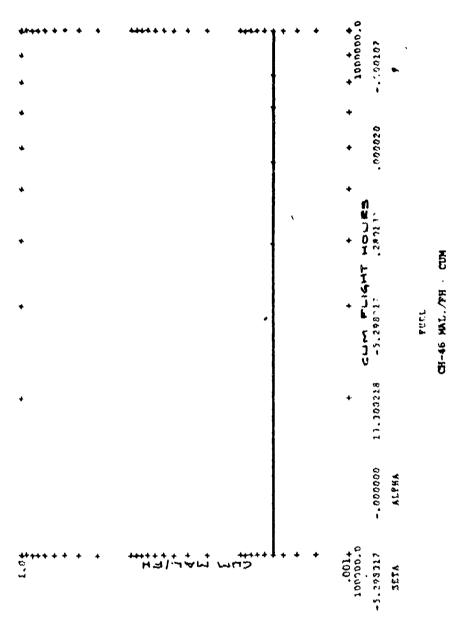
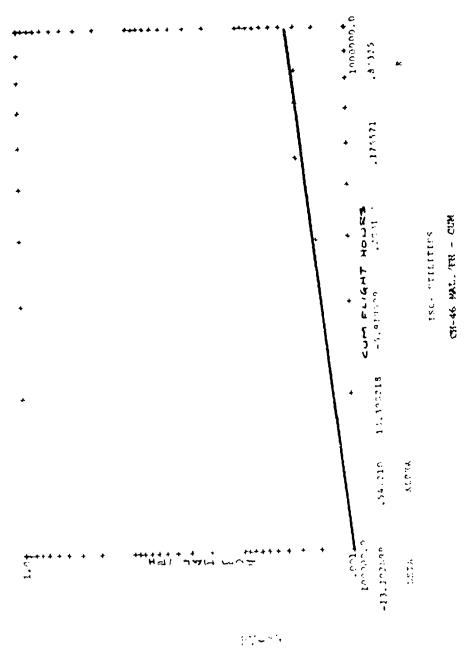
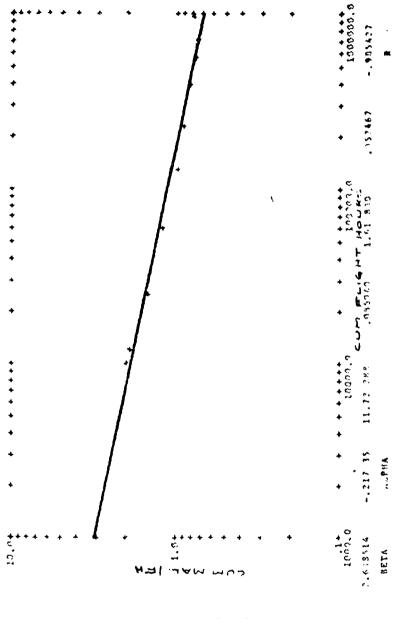


FIGURE 64

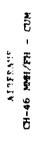


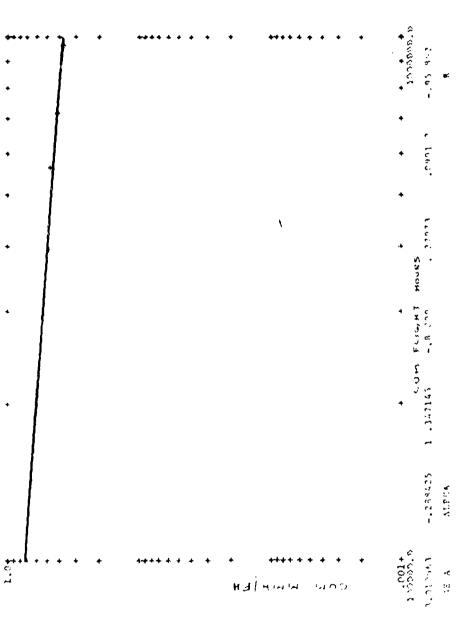


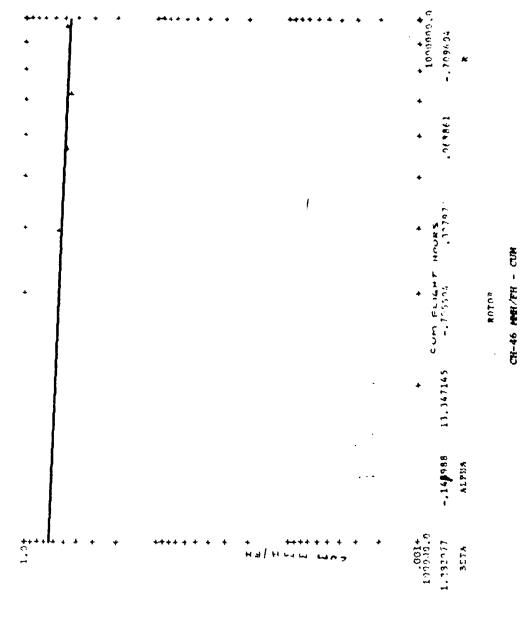
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FIGURE 64

CH-46 NMI/FH - CUM

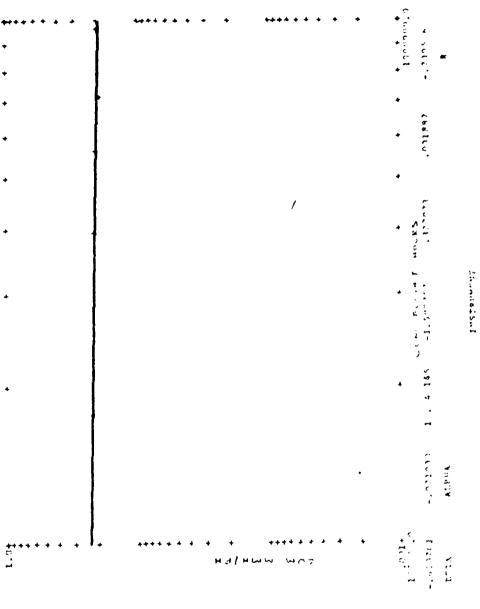


FIGURE 70

LANDING GEAR CH-46 MMH/FH > CUM

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FIGURE 71

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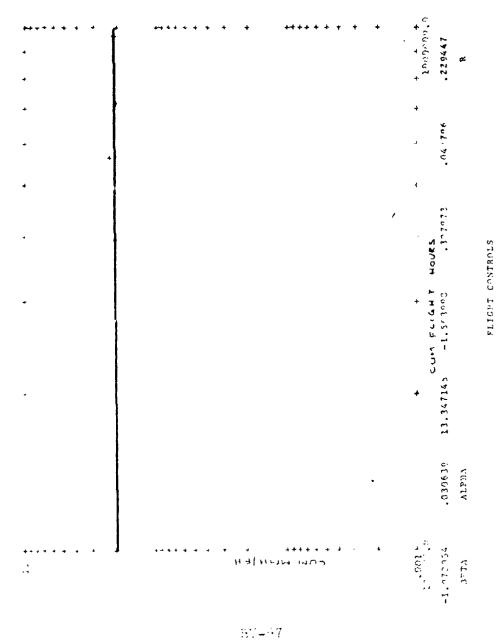
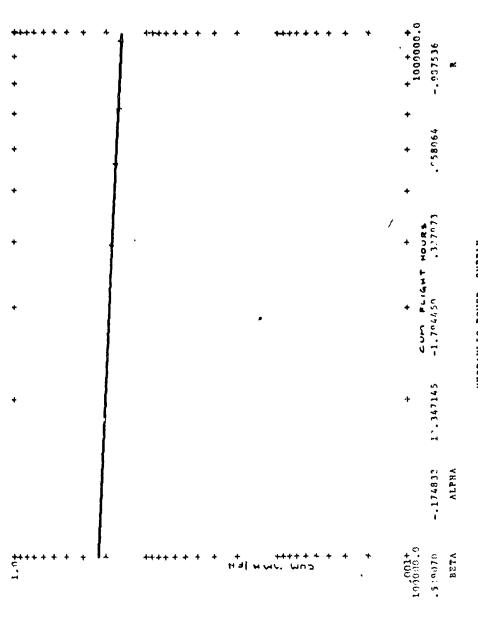


FIGURE 72

CH-46 MMI/FH - CUM



HYDRAHIIC POWER SUPPLY CH-46 MM/FH - CUM

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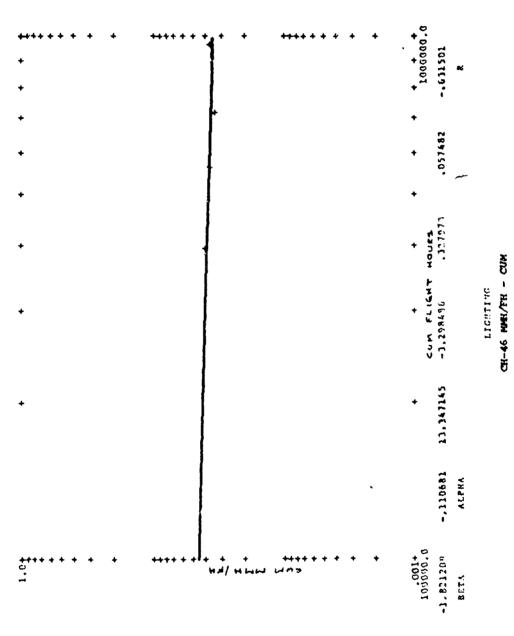
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CH-46 MMH/FII - CUM

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FIGURE 74

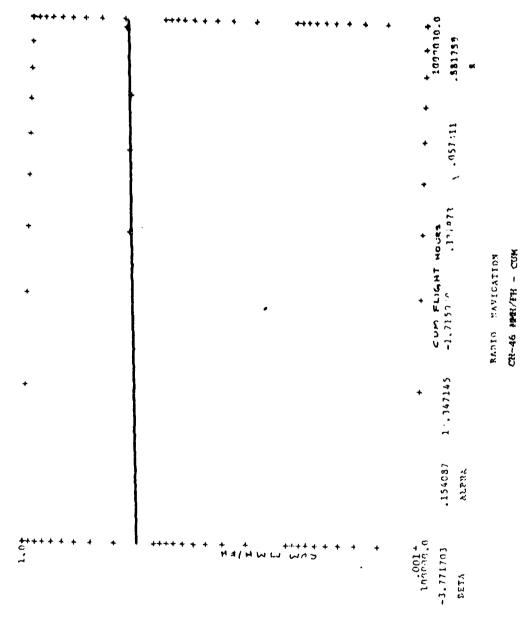
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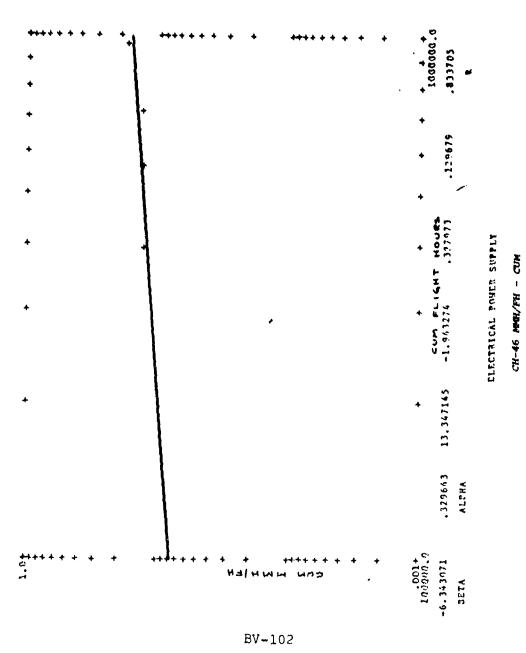
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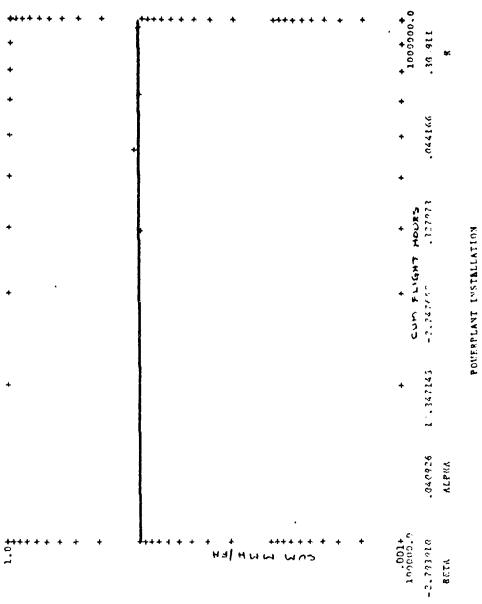
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BV-100



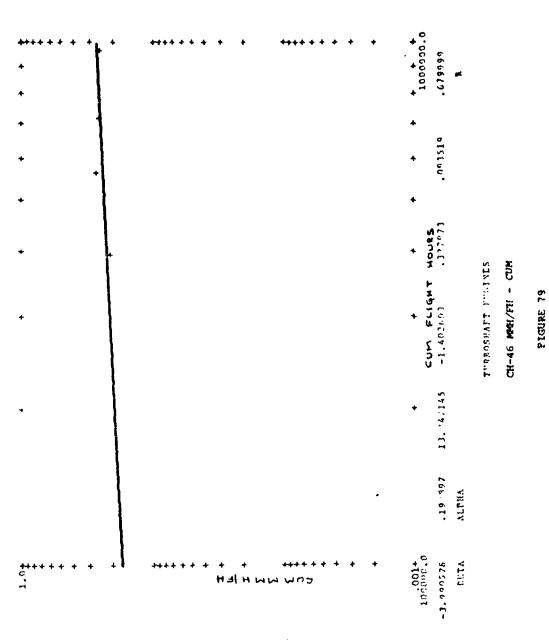
BV-101



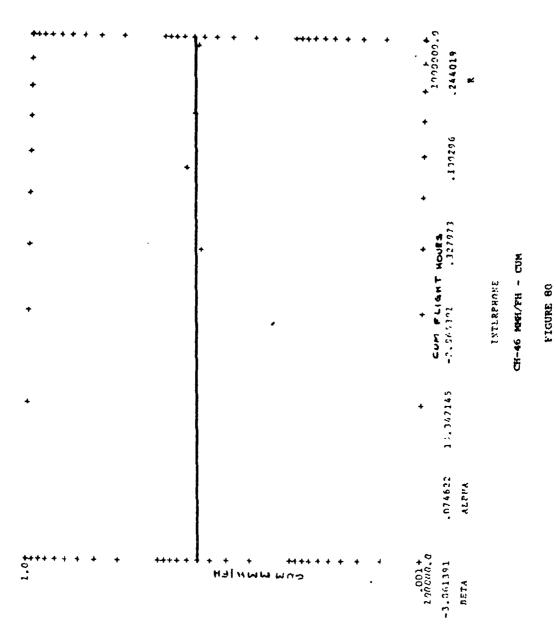


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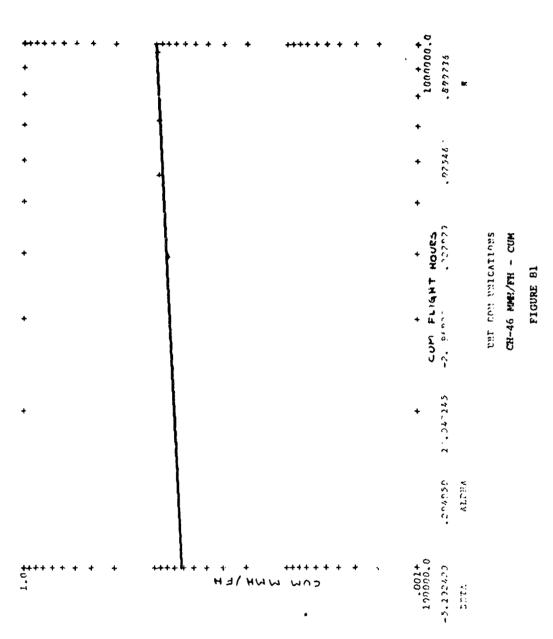
CH-46 MM FH - CUM



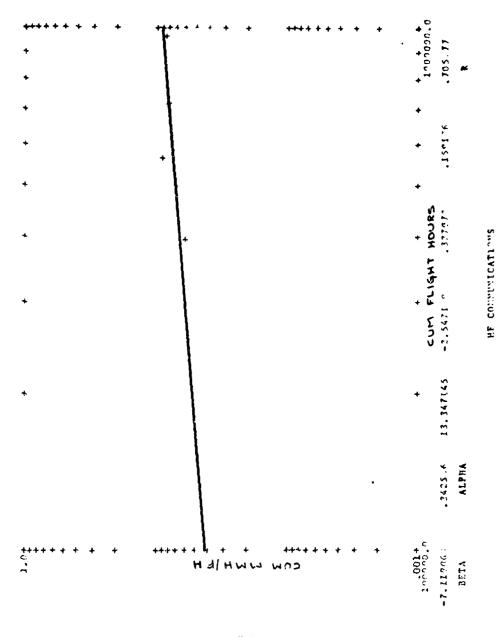
BV~104



BV-105

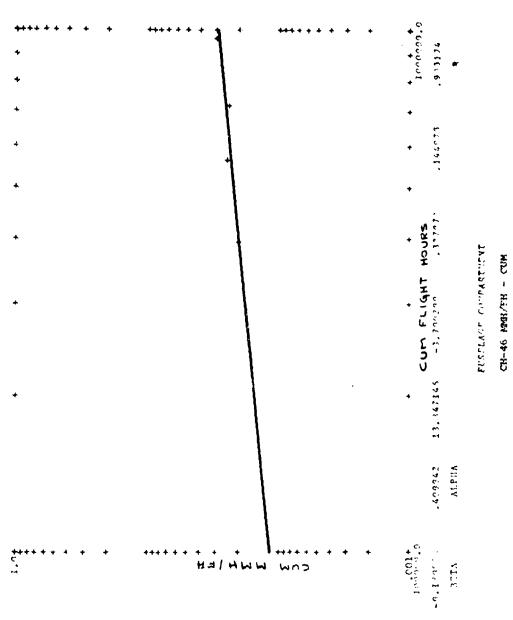


BV-106



CH-46 MPH/FH - CUM

BV-107



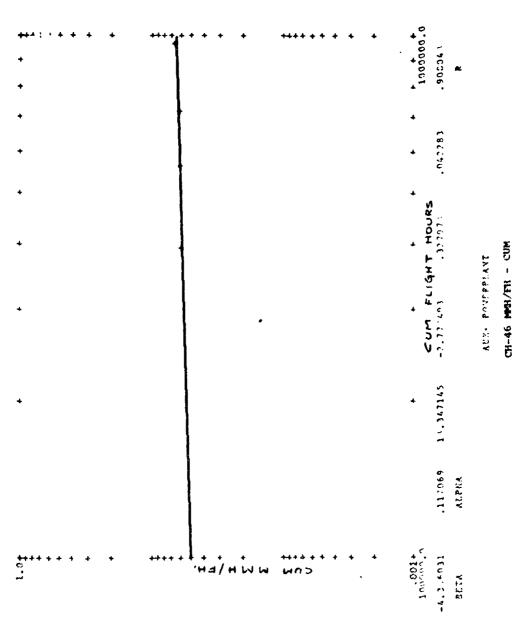
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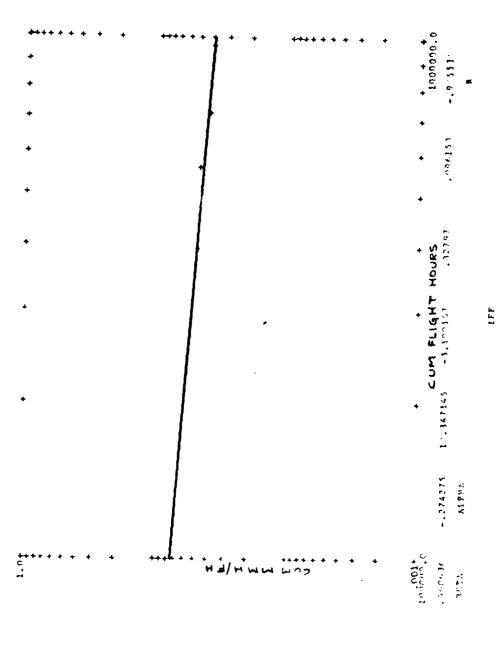
EV-168



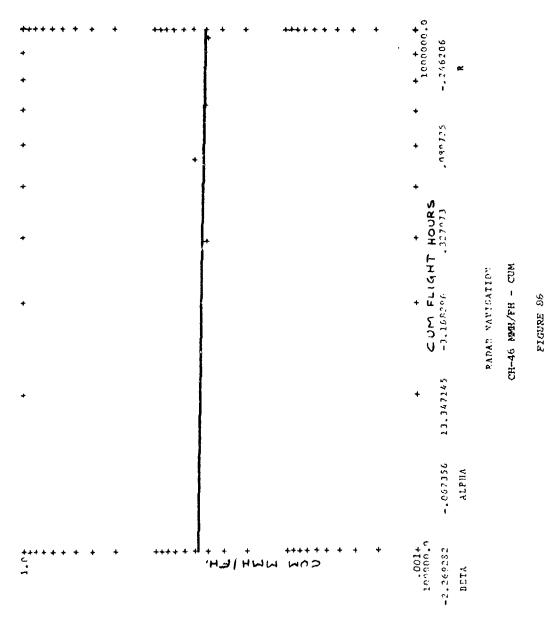
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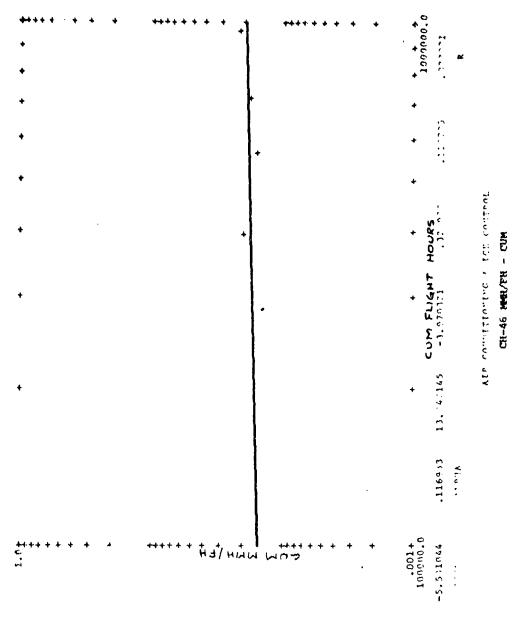
BV-175



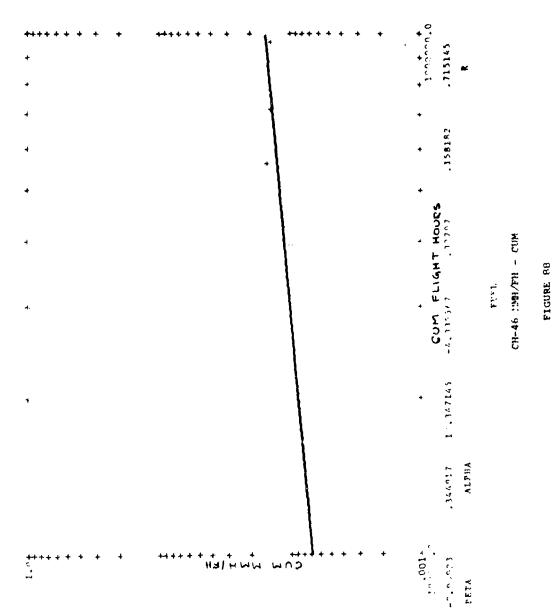
CH-46 MMI/FH - CUM



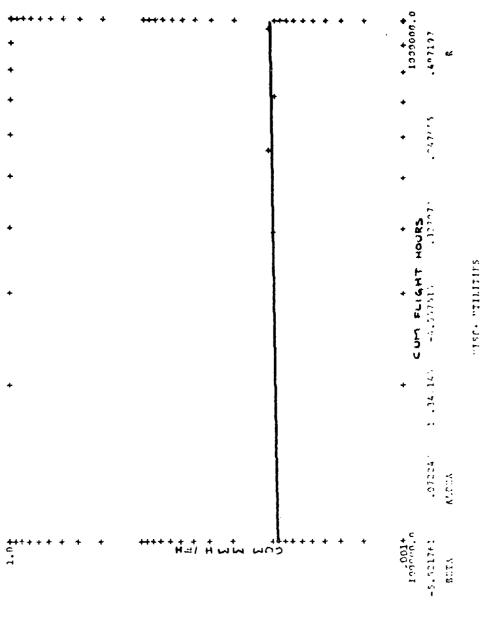
BV-111



BV-112



37-113



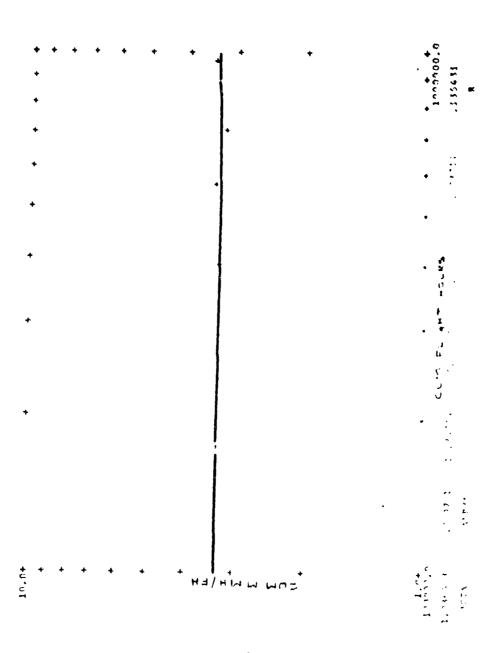
CH-46 NORI/FH - CUM

FIGURE 89

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BV-114

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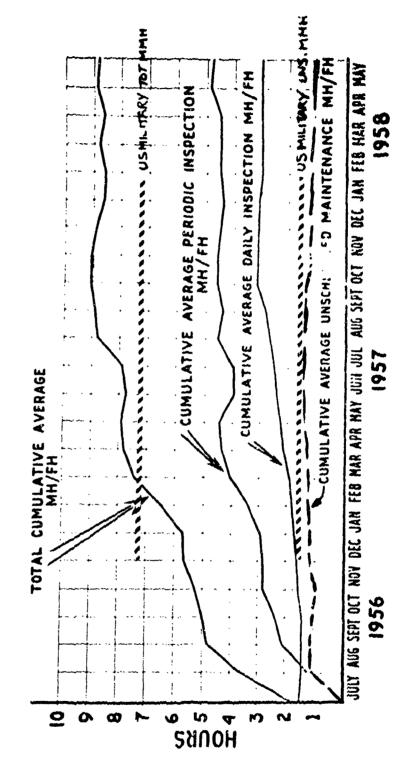


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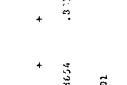
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TABLE 9 - LH-47 COMPLETE & GROWTH STATETICS

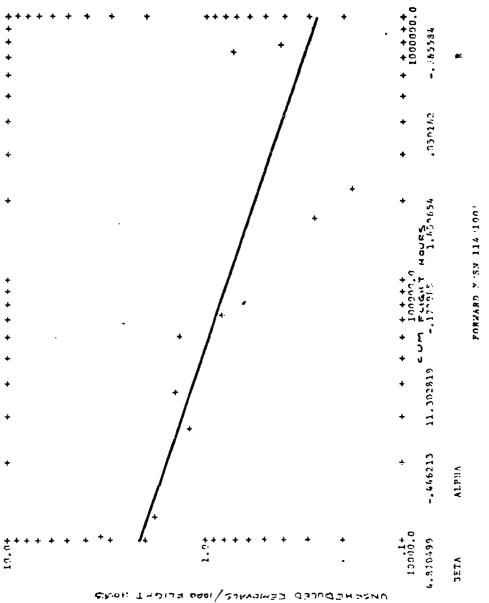
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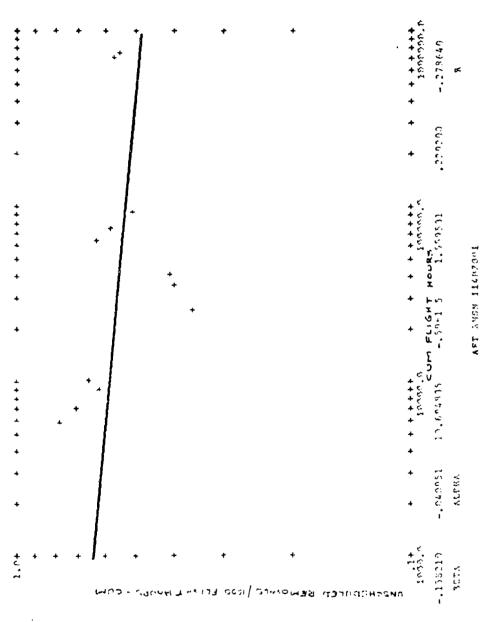


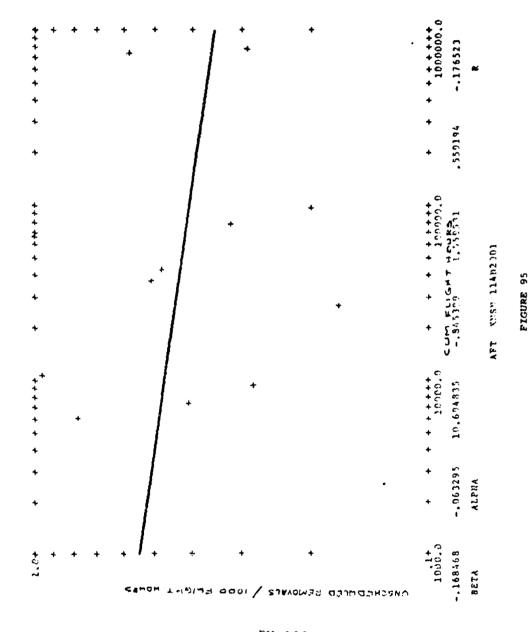
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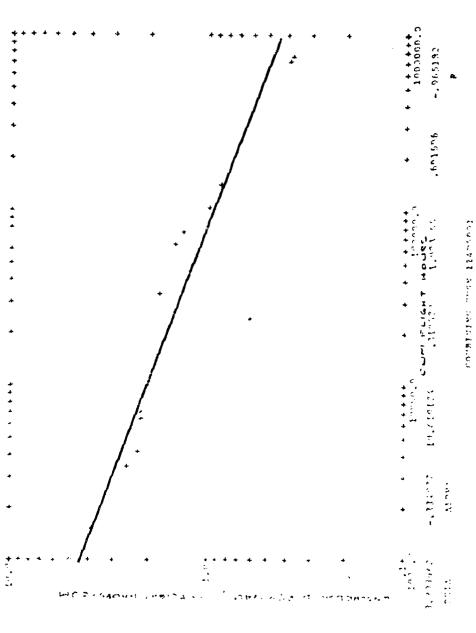




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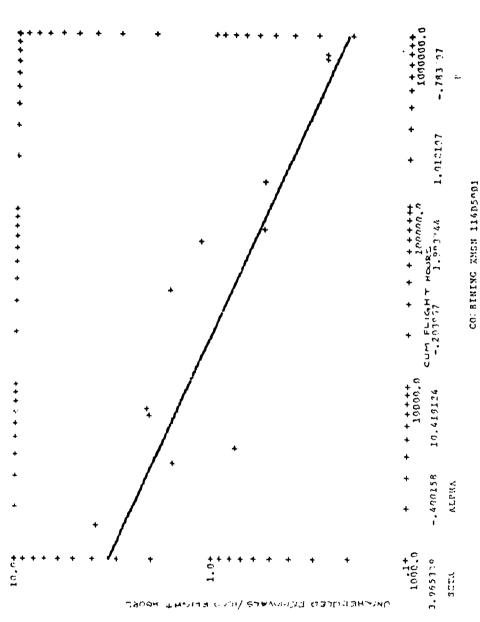
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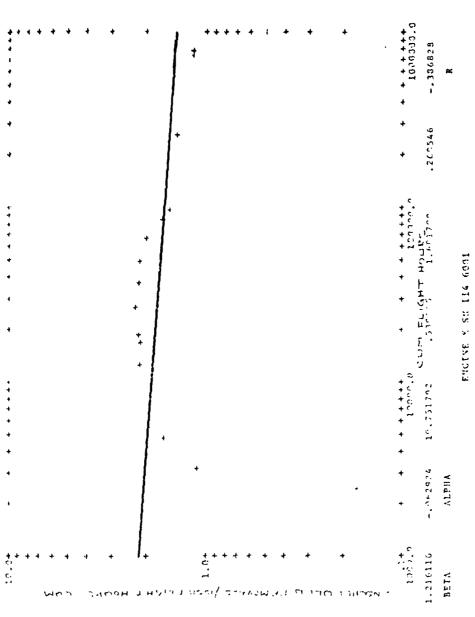
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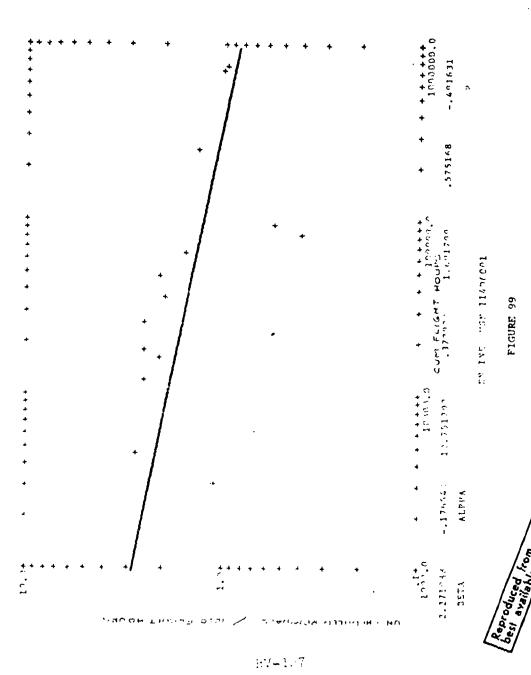


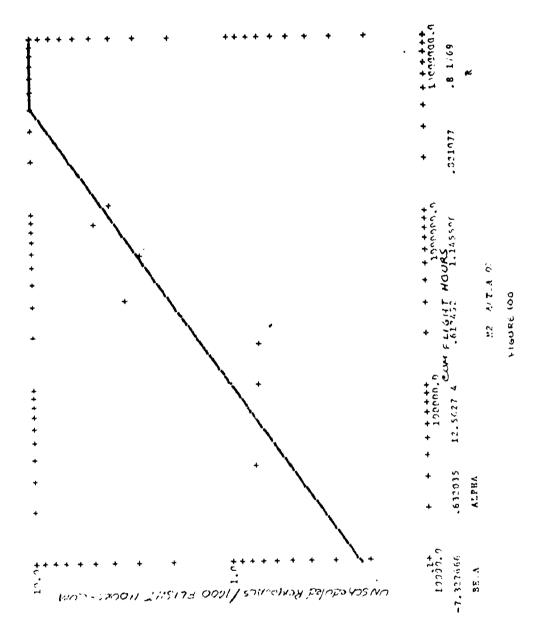
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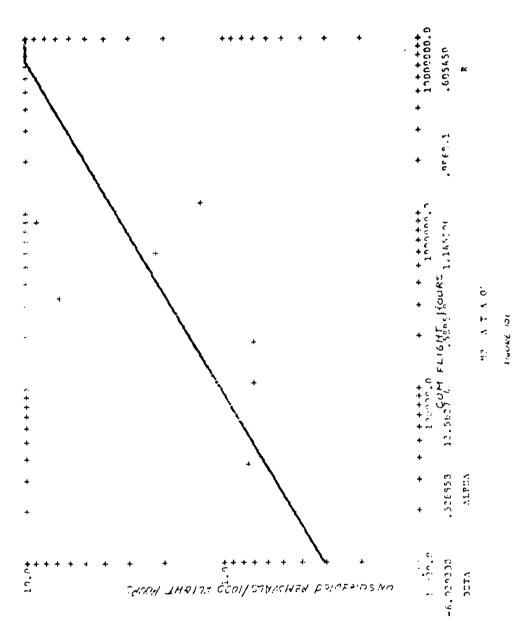


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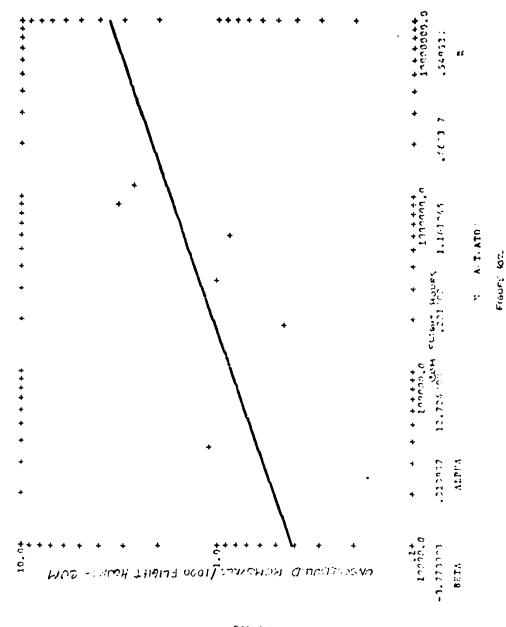




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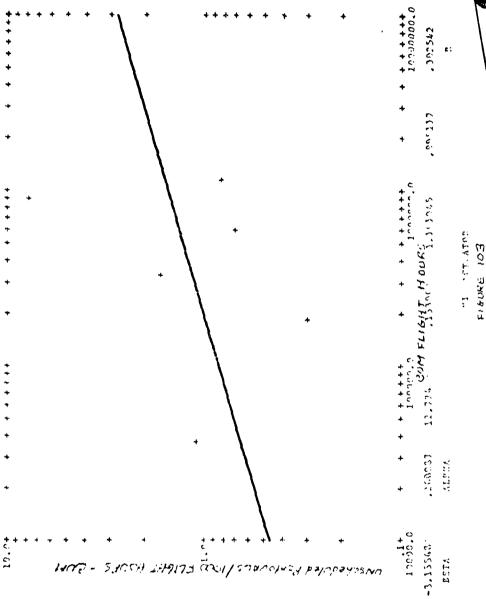


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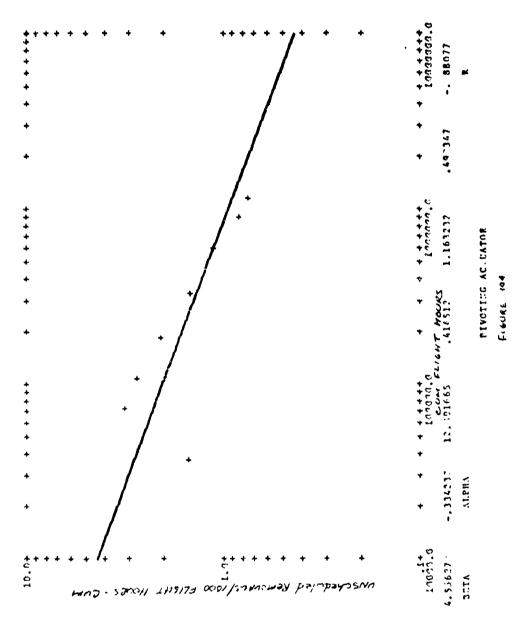


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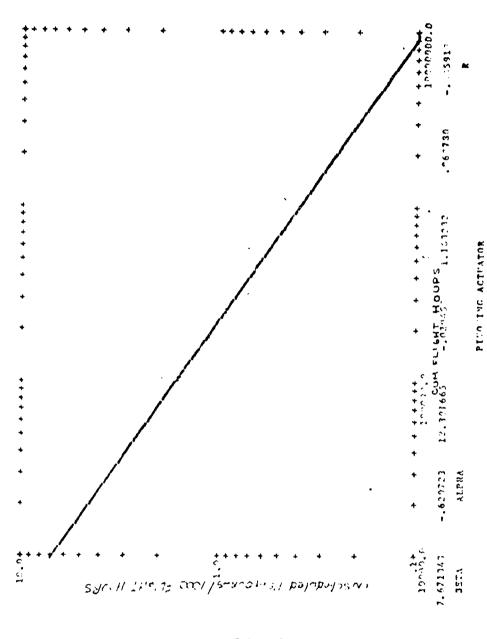


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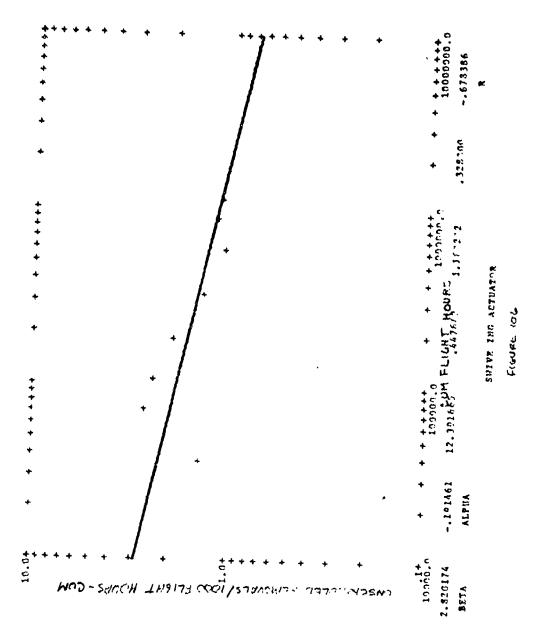


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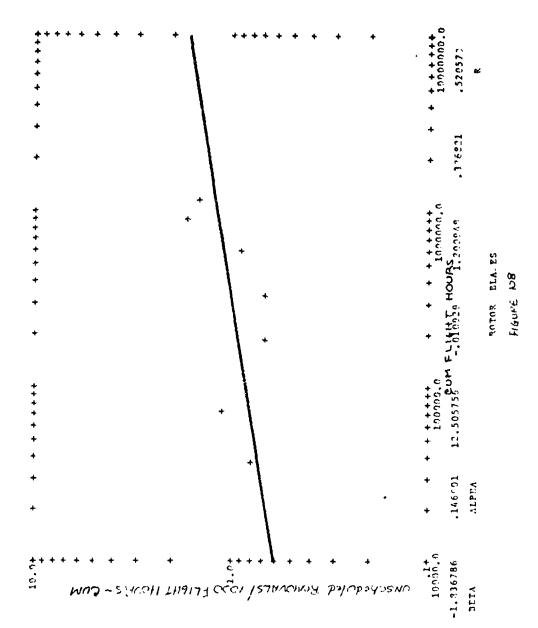
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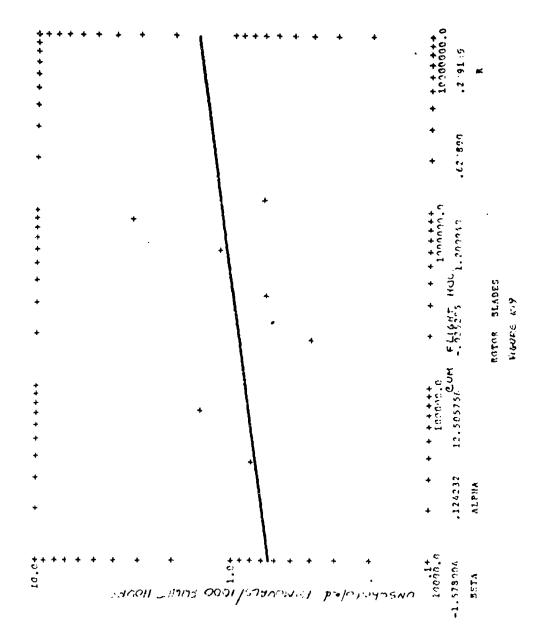
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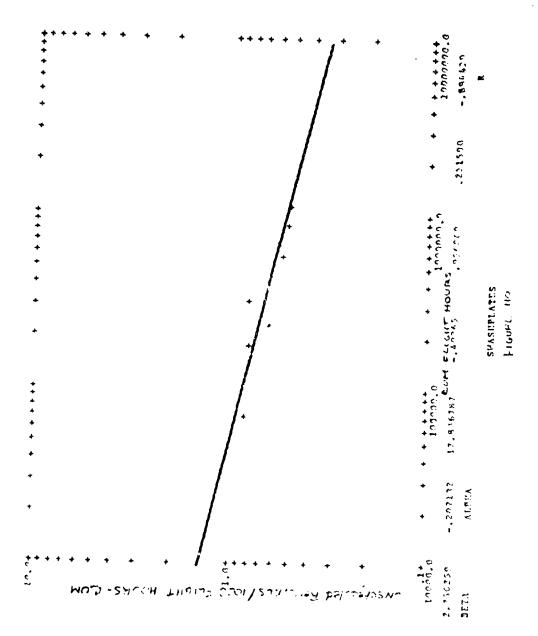
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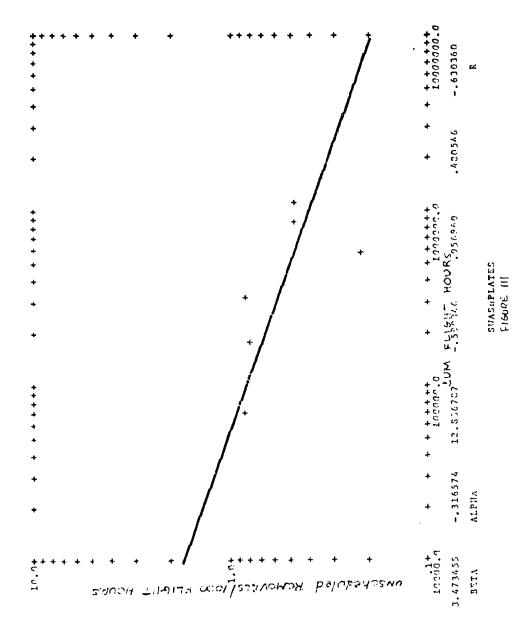


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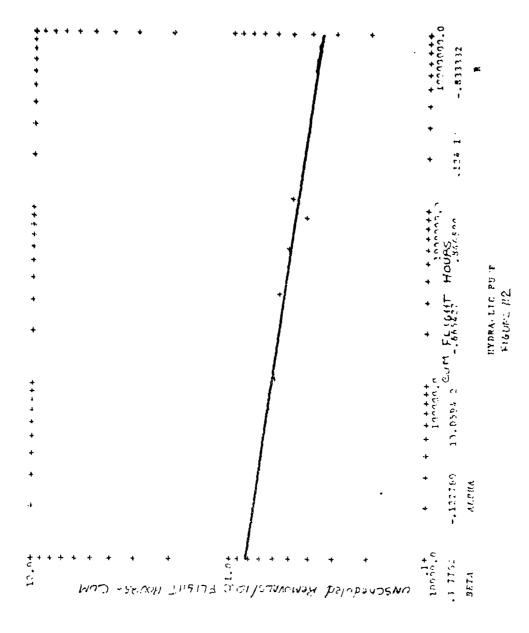
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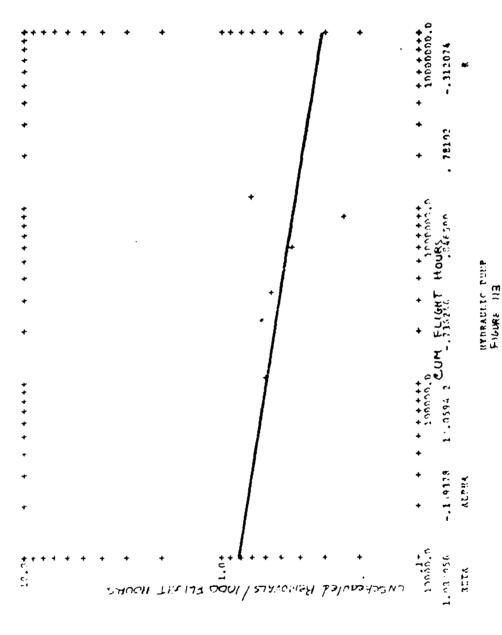
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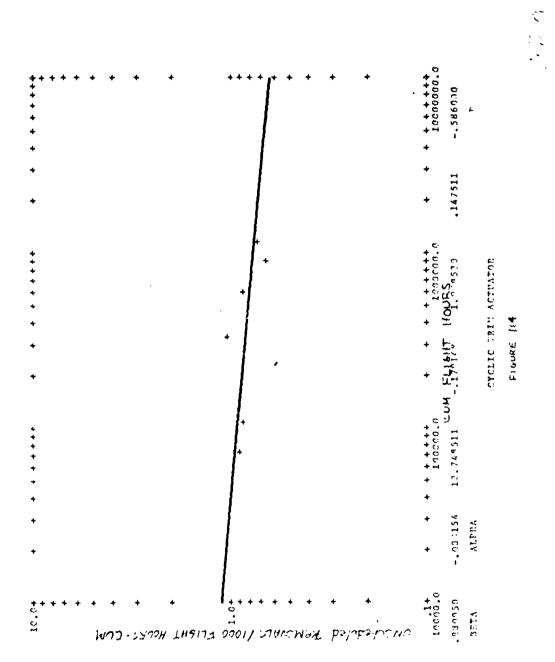
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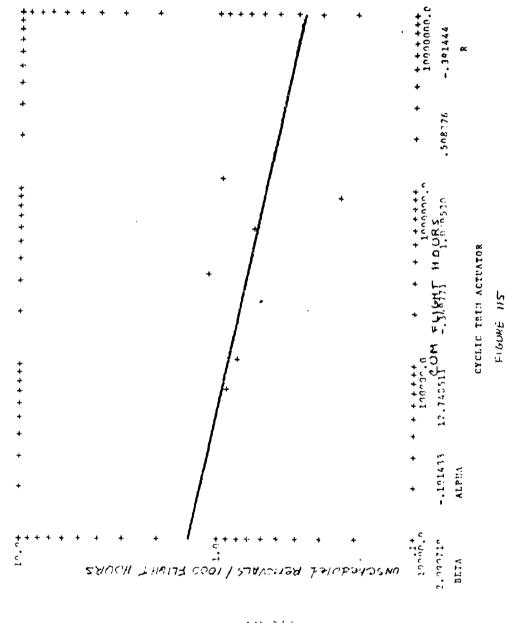


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BV-141



PV-142



BV-143

TABLE 10 - CH-47 XMSN R GKOWTH PARAMETERS

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NO OCILIONAL I	B	8.	œ	B.	8	ď
FORWARD XMSN	5.293	450	5.293450786 4.870446766	4.870	446	766
ZAZX FIA	158	¥9	158041279168064177	168	+90	177
COMBINING XMSN	3.809	-,335	3.809 335965 3.965400 783	3.965	400	783
ALEXE XXXX	1.216	063	1.216063367 2.271177492	2.271	177	492

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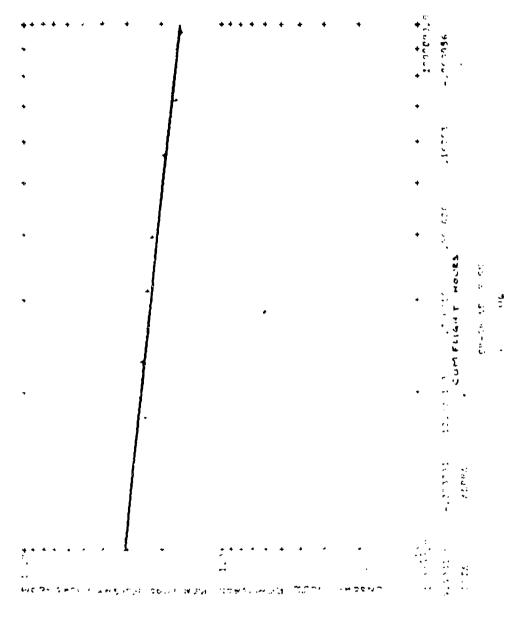
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TAPLE 12 - CH-46 COMPONENT R GROWTH STATISTICS

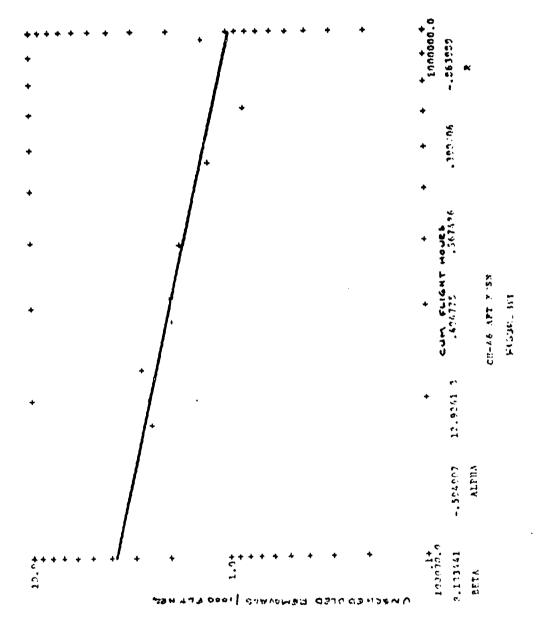
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380/12	•	1.380	.4 1.780 2.371 .165	.165	.352	1.182	.352 1.782 1.277 1.252	1.252	911	.778 .748 1.244.	1.244
621845	371/29 61 1 166 1.748 2.240 .339	1.748	2.240	.339	112:	1.705	i 1.705 1.619 1.488	1.488	120	.120 .610 1.110	1.110
563 306	1.4.1 St. 2.1 65. 0 2 65. 23	1.245	1261	.546	80+	··		1.887 1.216 1.249 1.152	1.216	1.249	1.152
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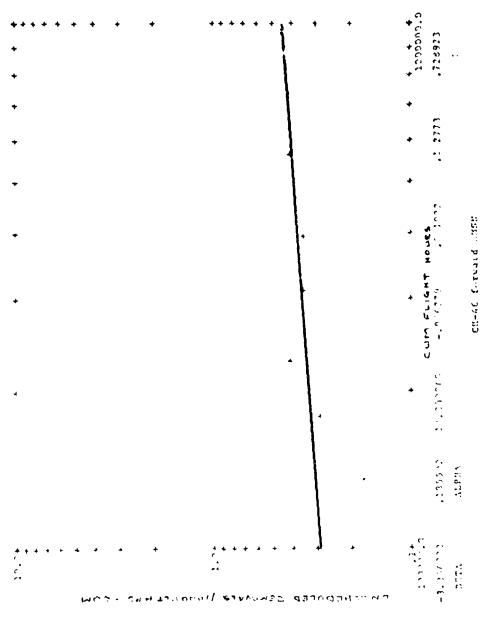
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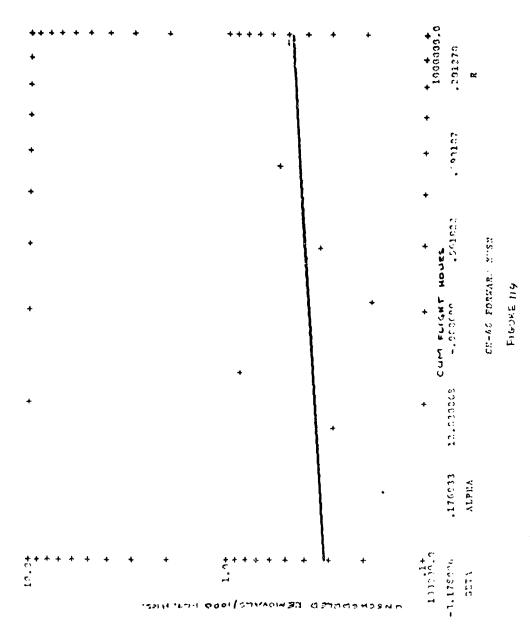


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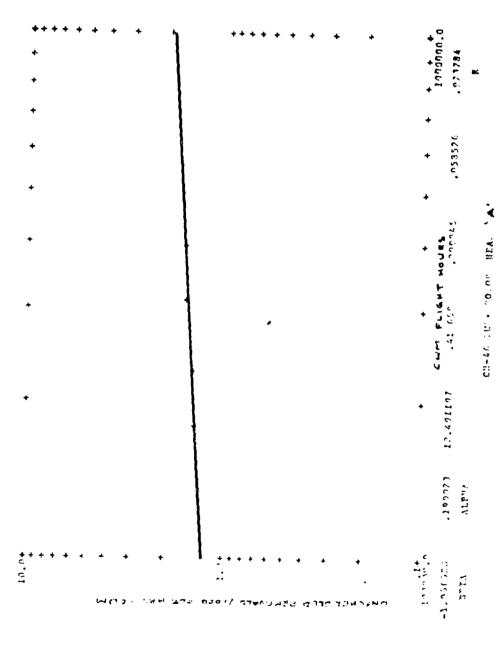


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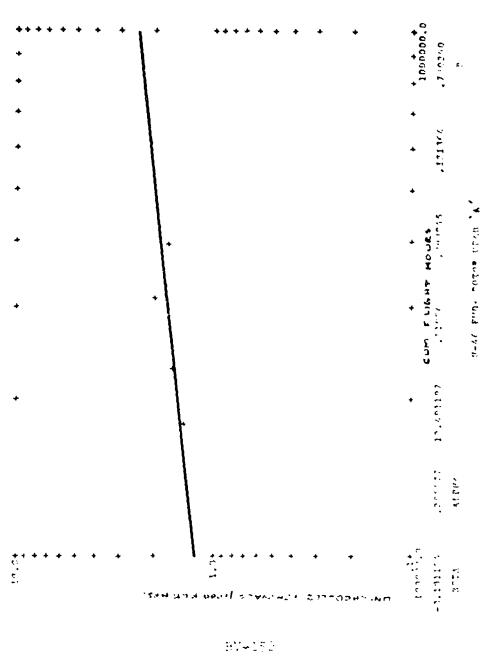
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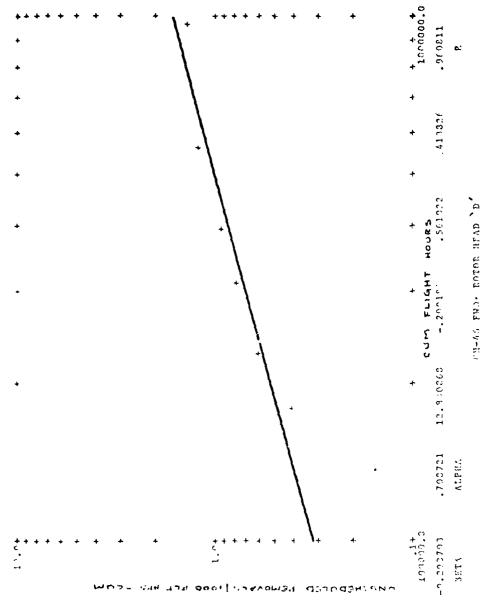
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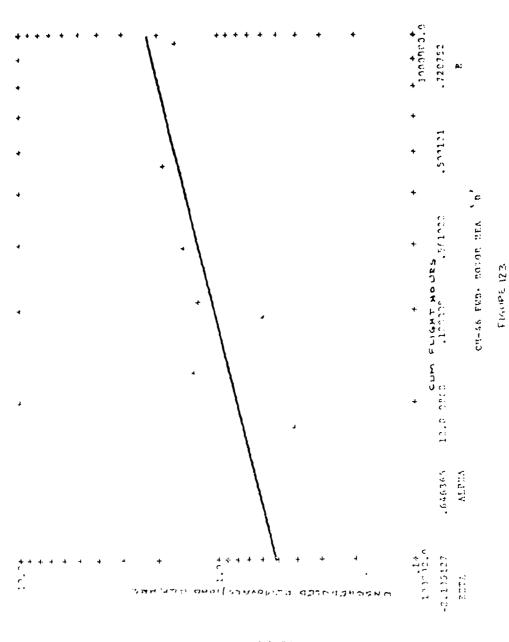
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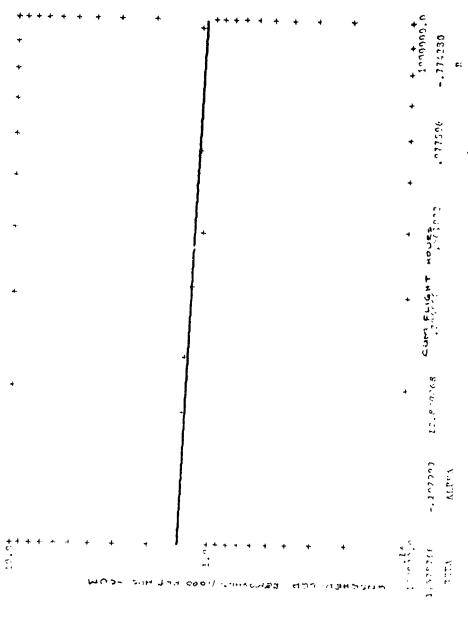
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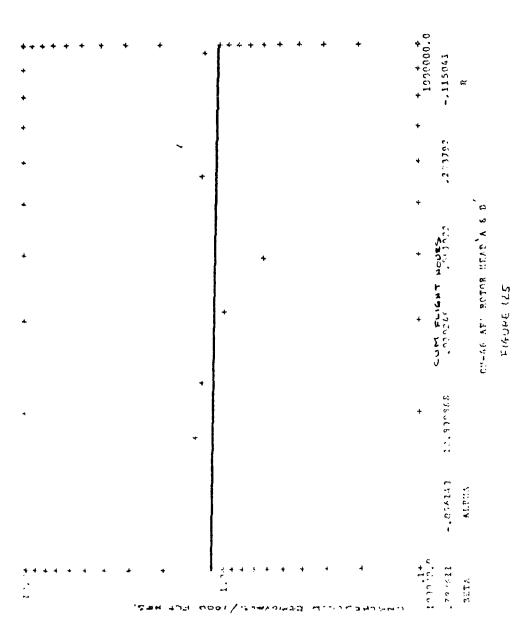
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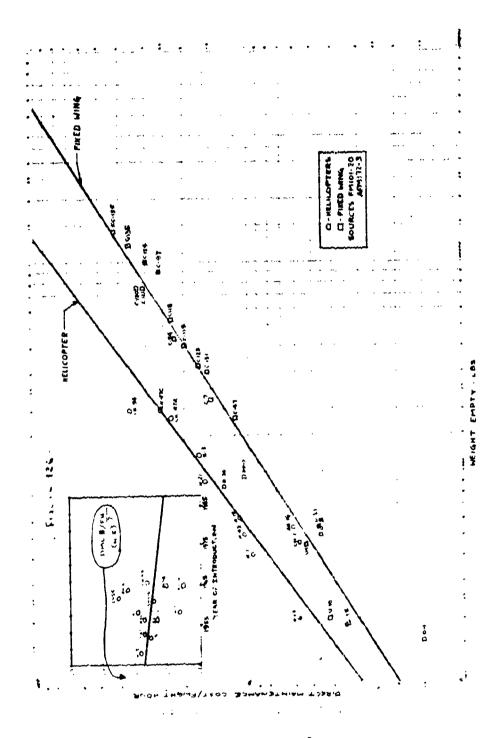
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BV-111

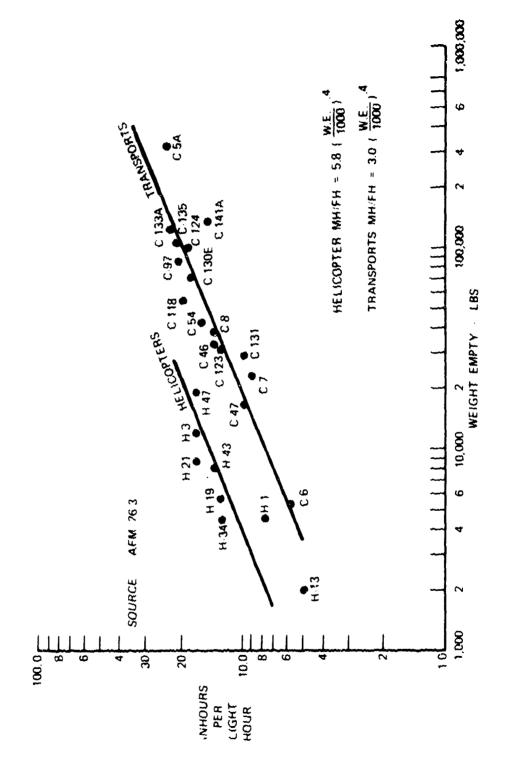
GKOWTH PARAMETERS (Z TABLE 13 - CH-46 COMPONENT

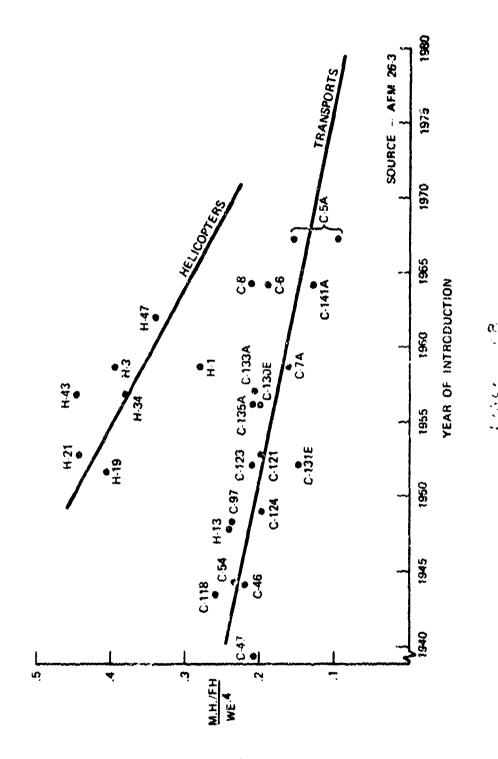
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AFT XMSN.	4,403	284	961 8.183	8.183	595	86 4
FORWARD XMS N.	-3.367	.,86	621.	.729 -3.179	113	,201
FWD ROTOR HEAD'A'	-1.957	061.		.974 -3.181	.296	0£1.
FWD. ROTOR HEAD D	-9.294	601.	196.	-961 -6.105	. 646	.72 {
AFT ROTOR HEAD ALD 1.579 107 774	(1.579	10J	+24	191.	95 0'-	5



BV-158

USAF HELICOPTER & TRANSPORT MAINTENANCE





BV-160

Part B

Data Submitted by Hughes

YOH-6 AND OH-6A HELICOPTER RELIABILITY STUDY

MIGHES HELICOPTERS
CULVER CITY, CALIFORNIA

PREPARED BY:

P. B. IVONS

RELIABILITY ENGINEER

APPROVED BY:

C. E. DAVIS

SUPERVISOR

RELIABILITY & MAINTAINABILITY

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HELICOPTER RELIABILITY STUDY

ARPA TASK ORDER T-105

PURCHASE ORDER NO. 20434 - HUGHES HELICOPTERS

2 December 1974

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IDA PROJECT T-105 TABLE OF CONTENTS

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IDA PROJECT T-105

1.0 INTRODUCTION

This report provides OH-6A Prototype and early Production Helicopter flight test hours and failure data as required under IDA project T-105 (IDA Purchase Order 20434). These data are presented in the following manner:

- a. Failures in each IDA subsystem category.
- b. Failure types in three categories: Mission, Flight Safety and System (Unscheduled Maintenance Actions).
- c. Failure totals and failure rates per flight hour.
- d. A monthly breakdown of flight hours and failures is presented when such information was available.
- e. Maintenance manhours per flight hour data are provided when such information was available.

2.0 DATA SOURCES

2.1 PROTOTYPE YOH-6 IDENTIFICATION

The prototype aircraft are identified in the following table. Note that the flight hours given are from first flight thru May 24, 1966 which is the date of the first flight of production aircraft No. 1 (65~12916).

TOTAL TIME

M. COE.
5/24/66
76 7∜
264
403
720 WW
269
324
810
309
608
64.74

^{*} Tie-down endurance vehicle; flown 13 hours prior to start of endurance tests.
** Detailed data provided for 8:7 hours.

2.2 PROTOTYPE DATA SOURCES

The prototype aircraft were flown in various tests at many scattered locations during the time period in question. The result is that the available historical data regarding maintenance, flight hours, and failure rates is fragmented. The best sources proved to be that for ships maintained at Culver City and for the competitive fly-off tests which were more closely observed and reported. The day-to-day Culver City maintenance and flight records for YOU-6 No. 3 and No. 5 were located and used. Competitive fly-off tests at Fort Rucker

(Logistical Evaluation and Tactical Suitability) provided total flight hour and failure data for YOH-6 No. 6 and No.8. The combined flight time for these four aircraft is 2300 hours and provides a representative sample. The competitive fly-off tests are described in paragraphs following:

2.2.1 Logistical Evaluation Test

Prototype No. 6 was flown to Fort Rucker in Feb. 1964 and began flight test which accumulated 1000 hours by June of that year.

The primary purpose of the test was to evaluate parts failures and replacement requirements when the aircraft was flown on an accelerated program. The flight periods were scheduled for 25 hours with a 15 minute turnaround. Four mission profiles were used which included nearly every type of flight that can be performed with a helicopter. In all, a total of 3867 landings and takeoffs were made during the 1000 hr. test period. This type of flying quickly brought any subsystem or component deficiencies to light.

Secondary proposes of the test were an evaluation of the preliminary MAC, component replacement schedules, mechanics training, and both standard and special tool requirements.

2.2.2 Tactical Suitability Test

This test was also performed at Fort Rucker using Prototype No. 8 primarily and No. 10 for a short period. The tests were conducted from March thru 'une of 1964 and were intended to check the OH-6 within the whole tactical environment. An engineering system of ratings was used in making evaluations. Tests included transportability, groung handling and hoisting, ease of maintenance, manhours required for replacement of major components, avionics suitability, flight characteristics and mission suitability. The preliminary MAC was evaluated as was personnel requirements. The flight evaluations required 230 flight hours.

2.3 PROTOTYPE TRACKING

Efforts to locate the YOU-6 aircraft and data were non-productive in general. Fowever, the following history was derived from the memories of Hughes personnel who were present during the period.

- No. 1 Static Tests Only
- No. 2 (19696F) Was flown 13 hours and then tied down in a whirl cage at Culver City for endurance tests. The aircraft was not moved at conclusion of tests and the airframe is still in place.
- To. 3 (19697) Underwent general testing at Culver City and armament firing at Camp Pendelton and Twenty-nine Palms. Crashed during low level firing run when the pilot inadvertently flipped a fuel switch instead of a gun safety switch. Aircraft was totaled. Pilot and passenger suffered minor inviries.

No.	4 (N9 62-		This aircraft is believed to have undergone flight testing at Wright Patterson. Present whereabouts unknown.
No.	5 (N9 62-	4216)	Under ent extensive testing primarily from the Culver City base. Tests included FAA certification. Present whereabouts
No.	ύ (62		unknown. This aircraft was used in log-evaluation (1000 hour) tests at Fort Rucker; was later sent to Fort Bragg and may
No.	7 (62	?-4212)	presently be at Wright Patterson. Underwent tests at Edwards AFB. Tests were primarily of an engineering evaluation type to provide data for the Pilots Flight Handbook. Suffered a tail boom chop during
No. 8	8 (62	2-4213)	high altitude tests and was rebuilt. Present whereabouts unknown. Flown at Edwards AFR and later was used in Tactical
			Suitability Tests at Fort Rucker. This aircraft was flown in record breaking speed and endurance runs and is believed to be in a museum at Fort Rucker now.
No.	9 (62	2-4214)	Was flown at Edwards AFB, Bakersfield, and Yuma. Last known location was Aberdeen, Wash.
No.	10 (62	?-4215)	Was used in armament testing at Fort Rucker and Hunter- Ligget. Suffered a blade strike (trees) but was not badly damaged. Later was shipped to Paris for the Airshow. Present location unknown.

2.4 PRODUCTION OH-6A IDENTIFICATION

Production aircraft for which data are provided in this report are identified in the following table. Such history as is available is provided.

HUGHES PROD. NO.	ARMY SER. NO.	DELIVERY DATE	HISTORY
1	65~12916	10/66	l'sed in Stateside
2	65~12917	10/66	general testing and
3	65~12918	10/66	training. No. 3 & 6
4	65~12919	10/66	later suffered crash
6	65~12921	10/66	damage and were re-
8	65~12923	12/66	paired at HTC. No.
10	65-12925	12/66	2 & 8 are bailed;
11	65~12926	12/66	No. 2 at HTC, No. 4
12	65~12927	12/66	was destroyed in a crash.
14	65~12929	1/67	Used in R&M demo. (ARU).
15	65~12930	2/67	No.15 later destroyed in
• ,			a crash.
2 5	65-12940	2/67	!!sed in confirmatory
29	65-12944	4/67	tests (AKN). No. 25,
31	65-12946	4/6/	29 A 31 later suf-
40	65~12955	4/67	fered crash damage
50	65~12965	5/67	and were repaired
,0	0.2 XE 10.2	2, 2	at HTC.

2.5 PRODUCTION DATA SOURCES

Data sources for production OH-6A are the R&M Demonstration (Fort Rucker), Confirmatory Tests (Fort Knox) and Hughes Service and Operation Reports from the field. Additional description of source data follows:

2.5.1 R&M Demonstration

The R&M (reliability and maintainability) demonstration tests were performed at Fort Rucker during the period of Feb, 1967 thru Aug, 1967. Production aircraft No. 14 and No. 15 were each flown a total of 500 hours. Close records were kept of all failures which were divided into three categories, Mission, Flight Safety, and System. The failures in each category were charged to the major subsystem (8 total) as appropriate. Nine different mission profiles were flown during this program to provide a representative sample of all expected normal flights of the aircraft.

Maintenance manhour records were kept for all maintenance actions during the program and notations are provided as to the chargeable or non-chargeable nature of the actions. Non-chargeable maintenance actions are those concerning CFE (entine and avionics), actions due to incorrect maintenance practice, and accident or incident damage.

2.5.2 Confirmatory Test Data

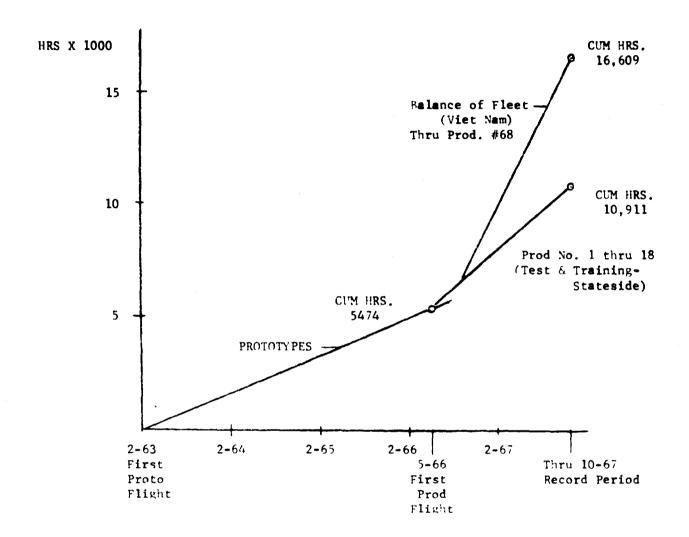
Confirmatory tests were conducted at Foit Knox during the period from Sept. 1967 thru June 1968. Five aircraft, (Prod No. 25, 29, 31, 40 and 50) were flown during the tests for a total of 5269 hours.

In these tests, primary concern was the pinpointing of problem subsystems and components, the development of solutions for these problems, and confirmation of the "fix" with resultant increase in reliability.

The data available provides system and component total failures without notation as to which may have been classed as mission failures. An assumption can be made however an judgement of the nature of the failure. The data are not divided into calendar periods as regards flight hours or maintenance actions.

2.5.3 Additional Production Helicopter Data

Data was extracted from Service and Operation Reports for nine production belicopters listed in Paragraph 2.4. The data for these aircraft covers the period from delivery through October, 196%; a total of over 4000 hours. The cut-off date, and those particular aircraft, were chosen because of their engagement in test or training activities within the United States. Dates



FICURE 2-1 TOTAL FLEET HOURS FOR RECORD PERIOD

beyond this period, and later mircraft, do not provide a representative sample due to cartime activities. Henever, a graph of the total OH-6 fleet hours for the record period is provided in figure 2-1. The failure rate data is provided only in terms of total failures and flight hours. Monthly breakdown information is not evailable.

3.0 SUBSYSTEM CATEGORIES

IDA subsystem categories used in this report include Hughes subsystems as shown in the following chart:

IDA SUBSYSTEM CATECORY	HUCHES SUBSYSTEMS
Complete helicopter	01 Complete Helicopter
Rotors	10 Main Rotor
	16 Tail Rotor
Airframe Components	20 Fuselage
	35 Tail Boom
	36 Stabilizer
	40 Utility Equipment
	60 Landing Cear
	70 Flight Controls
Transmissions and Drives	50 Drive System
Power Plant	77 Engine Controls
	80 Power Plant
	81 Fuel System
	82 Exhaust
	83 Oil System
Instruments	41 Electrical
	42 Exterior-Interior Lighting
	45 Instruments
Communications	44 Radio
Weapon Systems	47 Armor, Armament

4.0 CRITERIA AND DEFINITIONS

The following criteria were used in preparing this report. Abbreviations used in the tables are also defined.

- FS Flipht-Safety failures of the catastrophic type
- MSSS Mission failures of the type causing cancelled flight plan, premature return-to-base, or precautionary landing.
- System failures are unscheduled maintenance actions due to pilots squawks or defects found during inspections. Includes items for which maintenance may be deferred without creating a flight safety hazard.
- 1979 Failure rate per flight hour.
- $\epsilon_{\rm c}$ marreable items are all qualifying failures listed above.

NC - Non-chargeable items include parts removed for access to faulty parts, parts removed in error during fault isolation, parts damaged due to incorrect maintenance practices, cannibalization, accident damage, and scheduled (TBO) removals.

CUM - Cumulative

LOC - Location during test period:

AAB - Aberdeen or Phillips AAB

AKN - Fort Knox

ARU - Fort Rucker

EAF - Edwards AFB

HTC - Hughes, Culver City

5.0 SUMMARY

5.1 PROTOTYPE DATA SUMMARY

					FAI LUR	ES	
SHIP NO.	LOC.	FLT. HRS.	MSN	FS	SYS	CUM	FR/FH
3	нтс	264	8	0	105	113	0.4280
5	HTC	807	18	0	331	349	0.4325
6.	ARI'	1000	17	0	76	9 3	* 0.0930
8	ARI	230	9	0	93	102	0.4434
				-			
TOTALS (a11)	2301	52	0	605	657	0.2855
TOTALS (excludin # 6)	1301	3 5	0	5 2 9	564	0.4335

Failure rates for Ship 6 appear low when compared to other prototype aircraft. This is possibly due to the type of testing performed. Records used are for the 1000 hour log evaluation test at Fort Rucker. The flight time there was accumulated as quickly as possible and deferrable type maintenance actions may not have been recorded. CFE failures (engine and communications equipment) were not recorded or charged. Refer to Table 6-5 for system details.

The data for ships No. 3, 5, and 8 were derived from day-to-day records and include all GFE. Some difficulty was experienced in determining which maintenance actions were due to failures and which were work requirements for specific tests. Bias, if any, is toward the high failure rate side. Refer to tables 6-1 through 6-4 and 6-6 for detailed data.

5.2 R & M DATA SUMMARY (PRODUCTION)

				FAI	LURES	i	
SHIP NO.	LOC.	FLT HRS.	MSN	FS	SYS	CUM	FR/FH
12929	ARU	500	8	0	154	162	0.3240
12930 TOTAL	ARU S:	500 1,000	$\frac{8}{16}$	0	190 344	198 360	$\frac{0.3960}{0.3600}$

Refer to tables 6-7 through 6-10 for detailed data. GFE failures were not recorded or charged.

5.3 CONFIRMATORY DATA SUMMARY (PRODUCTION)

				FAIL	URE:	S	
SHIP NO	<u> Loc</u>	FLT HRS.	MSN	FS	SYS	CUM	FR/FH
12940	AKN	1,032					
12944	AKN	1,068					
12946	AKN	1,037					
12955	AKN	1,053					
12965	AKN TOTALS: .	1,077 5,269	73	0	972	1,045	0.1983

Refer to table 6-11 for details. The data includes GFE failures. A monthly breakdown for these particular tests is not available.

5.4 ADDITIONAL DATA SUMMARY (PRODUCTION)

		,	•		FAILU	RES	
SHIP NO.	LOC.	FLT HRS.	MSN	<u>FS</u>	SYS	CUM	FR/FH
12916	ARU	474	12	0	39	51	0.1075
12917	HTC	183	6	0	13	19	0.1038
12918	ARU	564	10	0	37	47	0.0833
12919	EAF	286	11	0	79	90	* 0.3147
12921	ARU	900	20	0	84	104	0.1156
12923	ARU	352	2	0	15	17	** 0.0483
12925	ARU	483	5	0	16	21	** 0.0435
12926	ARU	652	6	0	16	22	* * 0.0352
12927 TOTALS (ALL)	AAB	$\frac{132}{4,026}$	<u>5</u> 77	0	<u>19</u> 318	<u>24</u> 395	0.1818

- * The failure rate data for this aircraft appears high, placing it in the same category as the prototype and R&M ships. The type of testing undergone at Edwards AFB is unknown, as are the criteria used in defining failures.
- The failure rate data for these aircraft appears low and outside the general pattern. The cause is probably inadequate reporting during the time period. When the questionable data are excluded from the totals (table below) the failure rate per flight hour is lowered. However, the first total including all "good" and "bad" data may be closer to the general average.

		<u>FAI</u>	LURE	S	
FLT HRS.	MSN	FS	SYS	CUM	FR/FH
2,905	59	0	208	267	0.0919

Refer to tables 6-12 and 6-13 for details of the data used, GFE failures (Avionics) are not included and a monthly breakdown is not available.

6.0 DETAILED DATA TABLES

Refer to tables 6-1 through 6-13 following.

TABLE 6-1 PROTOTYPE DATA (SHIP NO. 3)

	62.6 + /15.60P	CUM	المناوات المراوات ا	FAILU	RES (CHA	RGEABLE)	***********
MONTH	FLI CHT HOURS	FLICHT HOURS	<u>"SK</u>	<u>FS</u>	<u>8Y8</u>	TOTAL	ER/FII
4/63	9,8	9,8	1	0	g	10	0,9800
5/63	19,9	29,7	2	0	11	23	0.8417
6/63	12.1	41.8	0	0	11	34	0.8612
7/63	33. N	74.8	0	0	11	45	0.6283
8/63	24.5	99,1	2	0	14	61	0.6357
9/63	23.0	122,1	0	0	4	70	0 5896
10/63	6.4	128,5	0	n	2	72	0.5758
11/63	33.8	162.3	2	0	4	83	0.523"
12/63	25.5	187,8	0	0	12	95	0.5165
1/64	20.8	208,6	0	0	4	99	0.4842
2/64	18.1	226,7	n	()	3	102	0.4597
3/64	13.7	240.4	0	0	2	104	0.4409
4/64	17.2	257,6	1	0	8	113	9,4386
5/64	6.8	264.4	0	0	1	114	0.4374

^{*} Crashed during armament tests--Pilot error

TABLE 6-2 PROTOTYPE DATA (SHLP NO, 3) TOTAL FAILTRES PER SUBSYSTEM

1 - AR	OF ON CARLE					HONTH	T.							
4 63 5 63 67	•	69/9	2/63	8/63	69/6	10/63	10/63 11/63	12/63	1/64	2,'64	3/64	4/64	2/64	TOTAL
10 13 1	-	_	=	4	3	C1	Ξ	12	4	~	~	6	-	114
;	c:		C1	Cı	c	=	C)	0	c	0	C	C	C	=======================================
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0 4 3	~		-	~	~	e	~	<u>_</u>	~	c	c	-	e	19
0 0 0	=		0	c	e	c	e	C	c	c	c	C	C	0
0 0 ;	C		c	ē	c	=		C	c	c	c	c	C	
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1 4 1	-		~	۰	ء	-	æ	2	-	c	~	_	-	67
NO. 1 2 2	~		C •	~	c	c	c	-	C	~	C	0	C	12

TABLE 6-3 PROTOTYPE DATA (SHIP NO. 5)

		CUM			FAI LURE		
	FLICHT	FLIGHT				CUM	
MONTH	HOURS	HOURS	<u> ~2%</u>	<u>FS</u>	SYS	TOTAL	FR/FH
9/63	4.5	4.5	0	0	7	7	1.5555
10/63	21.7	26.2	1	0	15	23	0.8778
11/63	26.5	52.7	0	0	8	31	0.5882
12/63	5.0	57.7	2	0	12	45	0.7798
1/64	55.8	113.5	2	0	21	68	0.6017
2/64	33.9	147.4	1	0	13	82	0.4833
3/64	17.0	164.4	1	0	15	98	0.5918
4/64	22.0	186.4	0	0	32	110	ი. 5863
5/64	49.5	235.9	0	0	17	127	0.5140
6/64	112.7	348.6	2	o	18	147	~ 0.3964
7/64	38.2	384.8	1	0	18	166	0.4096
8/64	24.3	411.1	n	0	9	175	0.4057
9/64	26.6	437.7	1	0	19	195	0.4300
10/64	1.4	439.1	0	0	3	198	0.4354
11/64	18.4	457.5	0	0	7	205	0.4354
12/64	10.9	468.4	Ö	•	2	207	0.4380
1/65	6.1	474.5	n	Ó	3	210	0.4387
2/65	1.2	475.7	Ö	Ŏ	2	212	0.4418
3/65	34.0	509.7	ĭ	Ŏ	5	218	0.4238
4/65	23.2	532.9	ō	Ŏ	6	224	0.4166
5/65	3.9	536.8	Ō	0	3	227	0.4192
6/65	4.1	540.9	n	Ö	2	229	0.4198
7/65	9.2	550.1	Ö	Ō	3	232	0.4182
8/65	15.5	565.6	ì	Ö	8	241	0.4227
9/65	11.1	576.7	ō	0	4	245	0.4215
10/65	6.4	583.1	Ō	0	3	248	0.4220
11/65	9.0	592.1	ì	Ō	5	254	0.4258
12/65	ñ.8	600.9	Ō	0	3	257	÷ 0.4245
1/66	11.2	612.1	1	Ö	10	268	0.4349
2/66	28.0	640.1	Ō	0	4	272	0.4219
3/66	18.8	658.9	1	0	6	279	0.4206
4/66	11.8	670.7	0	0	5	284	0.4205
5/60	25.8	696.5	1	0	6	291	0.4149
6/66	12.2	798.7	0	0	5	296	0.4148
7/66	6.0	714.7	0	0	1	297	0.4127
8/66	4.1	718.8	Ö	0	3	300	0.4146
9/66	16.8	735.6	n	0	3	303	0.4091
10/66	32.5	768.1	1	Ó		309	0.4127
11/66	0.0	7 6 8.1	Ô	Ô	5 7	316	0.4219
12/66	0.0	768.1	ñ	ñ	;	323	0.4311
1/67	36.6	804.7	0	0	1	324	0.4125
2/67	1.8	806.5	ŋ	0	1	325	0.4129
3 67	0.0	806.5	n	0	17	342	0.4329
4/67	11.0	817.5			4	346	n.432n
***		V11.	$\frac{0}{18}$	$\frac{0}{0}$	328		

Periodic Inspection

inspection following transfer of aircraft

Conformity inspection

Best Available Copy

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TABLE 6-2 PROTOTYPE DATA (SHIP NO. 3) TOTAL FAILURES PER SUBSYSTEM

				•				1	
TOTAL	114	15	33	0	32	0	m 0 m	0	67
2/64	0	cc	CC	- c	cc	c C	000	c	10
79/7	6 6	- 0	ش ج	- c	m c	- 0		: C	7
3/64	0 9	cc	0	cc	CC	cc	C C) c	6.0
2/64	0	cs	- c	cc	- 0	c c	cc -	- c	0 7
1/64	4 C	c c	- c	- c	c c	20	C C .	c c	e 0
12/63	12 0	- c	⋄ ≎	cc	e c	60	66	cs	10
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8/63	16 2		~-	~ =	۳۵	7 0	cc	c c	9 6
7/63	= ~	. m.c	. ~=	~ c	64 C	- 0	5 5	C C	2.53
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818. (Att cott)	HHIRO	FLICOPITE ROLL RESERVED BY	ALRUKATE	COMPS XMS1 - 3	DRIVES	PLA'31 [XS1, N	COMMIN- COMMIN- ICATIONS	SYSTEMS	TOTAL REPOYALS

TABLE 6-4 PROTOTYPE DATA (SHIP NO. 5) Sheet 1 of 3 TOTAL FAILURES PER SUBSYSTEM

1/63 12/63 1/64 2/64 3/64 4/64 5/64 8	C = CHARGEABLE NC = NOW CHARGE	C = CHARGEABLE NC = NOW CHARGFABLE						MONTH	=						
14 23 14 16 12 1 5 7 5 5 4 4 4 2 12 5 5 6 6 1 1 0 1 0 1 0 0 1 0 0 1 0 0 0 0 0 0 0 0 1 NSTALLED 1 11 99 99 5 1	9/11 89/01 89/6				3/64 4		5/64	79/9	1/64	8/64	79/6	10/64	11/64	12/64	1/65
3 5 3 2 2 2 4 6 1 2 4 6 6 1 1 0 1 1 0 3 2 4 4 4 1 0 0 0 1 1 1 1 0 0 0 0 0 0 1 0 0 0 0 1 0 0 0 0	x x	14 5	23	14	16	12	17 5	20	19	6 0	20	e 0	7	7 -	60
5 12 5 5 6 2 2 2 1 0 1 1 0 1 1 0 0 1 0 0 2 4 4 2 4 4 3 2 4 4 0 0 1 0 0 1 0 0 0 0 1 0 0 1 0 0 1 1 1 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	£ 2	n 2	SO	60	2	2 1	7		0 0	2 0	e 0	10	1	0 -	00
1 0 1 0 0 1 0 0 1 0 0 3 2 2 4 4 4 0 0 1 1 1 0 0 0 0 0 1 0 0 0 1 0 0 0 1 0 0 0 1 1 0 0 0 1 0 0 0 0	- 5	2	12	2 2	5	9 7	2	e	9	9 0	6 4	0	2 0	-0	~0
3 2 4 4 4 6 4 6 6 1 1 1 1 1 1 1 1 1 1 1 1 1	CO	,	00		0	00	- 0	00	00	00	0 7	00	-0	-0	00
2 4 2 4 0 0 0 2 2 0 0 0 0 0 11 0 0 0 10 0 0 10 0 0 10 0 0 11 11 9 9 5 1 6 3 3 3 2 1	3.5	0	2	2 0	7	7 -	7 7	10	9 2	0	2 -	1 0	7 1	00	~ 0
0 0 1 0 0 0 0 0 0 INSTALLED 11 11 9 9 9 5 1 6 3 3 2 1	 .	2 0	7 0	2 2	7 7	0 0	0	7 0	2 2	00	40	00	00	00	0
INSTALLED 11 11 9 9 5 6 3 3 2 1	0	0	00	0	0 0	0 0	0 0	c 0	00	0 0	00	00	00	0	00
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	7 8	11 6	11	o. €	6 2	2 1	12 2	71	32	4 0	7 7	-0	e =	-0	00

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TABLE 6-4 PROTOTYPE DATA (SHIP NO. 5) TOTAL TAILTRES PER SUBSISTEM

COMPLETE C 2 / 65 3 / 65 6 / 65 6 / 65 6 / 65 6 / 65 6 / 65 6 / 65 6 / 65 6 / 65 6 / 65 6 / 65 6 / 65 6 / 65 6 / 65 7 / 65 8 / 65 1 / 65 <th>SUB SYS. CATFOORY</th> <th></th> <th>CEAR C NON</th> <th>C = CHARCEABLE MC = MON CHARCE</th> <th>FACLF</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>MOX</th> <th>MONTH</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th>	SUB SYS. CATFOORY		CEAR C NON	C = CHARCEABLE MC = MON CHARCE	FACLF						MOX	MONTH							
C. 2 6 6 3 2 3 9 4 3 6 3 11 C. 0 0 0 0 1 0 0 1 3 3 1 C. 0 0 0 0 0 0 0 1 1 1 2 3 3 3 4 3 4 3 4 3 4 3 3 4 3 3 4 3 3 4 3 4 3 4 3 4 3 3 4 3 3 4 <th></th> <th></th> <th>59/7</th> <th>37.65</th> <th>4/65</th> <th>59/5</th> <th>59/9</th> <th></th> <th></th> <th></th> <th></th> <th>11/65</th> <th>12/65</th> <th>1/66</th> <th>2/66</th> <th>3/66</th> <th>99/5</th> <th>99/5</th> <th>9/9</th>			59/7	37.65	4/65	59/5	59/9					11/65	12/65	1/66	2/66	3/66	99/5	99/5	9/9
SYC 00 1 0 1 0 1 0 0 1 0 0 0 0 0 0 0 1 1 1 1 1 1 2 NG 00 00 00 00 00 00 0 0 0 0 0 1 1 1 1 1	COMPLETE HELICOPTER	u U	çı C	နင	90	۵ ۳	2 2	۳ ٥	б	7 C	9	9 -	m m	11	4 C	7 0	<u>-</u> م	7 8	N W
No. Color Color	ROTORS	ر بر د	cc	- 0	00	- 0	cc	2 0	2	- c	- 0			2	0 0	- 0			9 0
St. Ct. O.	AIRFRAME COMPS.	ı X	€+ €	٥٠٠	e 5	00	c c	- 0	0	- c	- c	9	0	9	- c	2	- c	0	0
C	XMS V A DRIVES	u Z	cc	cc	00	- c	cc	cc	0	0 0	cc	0	10	- 0	0	0	. 0 0	00	00
S	POWFR PLAKT	<u>ن</u> لا ن	cc	~ ¢	- c	၁၁	00	cc		cc	cc	- 0	00		cc	0	0	7 -	0 0
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										GFE INCLUDED										
	TOTAL	346	88	61	28	133	54	23	2	63	18	57	12	6				16.	701	2
	19/7	4	0	~	0		С	С	C	c	0	7	C	c	C			-	٠ ح	>
MONTH	3/67	11	0	~	0	œ	0	С	С	٣	С	*	c	_	С			ď	· c	>
	2/67		=	0	C	c	С	С	c	. c	C	~	C	c	С			c	C	>
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	10/66 11/66 12/66	,	c		О	۲.	C	С	c	c	C		С	C	0	LLED		-	- c	>
	10/66	ç	-		0			c	С	_	c	2	С	_	С	INSTALLED		-	- ح	٥,
ABIF	9/66	3	c		С	c.	0	9	S	s	c	0	c	c	c	NO WEAPONS		~	· c	>
· CCARCEABLE - SON CHARCEABLE	3/66	~	c	0	c		c	c	=		c		0	c	c	92		-	c =	:
C = CCARCEASLE	99/7	_		9	_	-	c	С	C	c	С	S	c	0	C			c	; c	>
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STB STS. (AFFCORY		STAIME	HELICOPTFR	ROTORS		AIRFRAME	COMPS.	XMSN	DRIVES	POWER	PLANT	INSTS, A	ELEC.	COMMIN-	ICATIONS	WEAPON	SYSTEMS	TOTA1	REMOVA15	CHO CARIO

TANE 6-5 PROTOTYPE DATA (SHLP NO. 6) TOTAL FALLIKES PER SPESYSTEM

C = CLARCEABLE AC = AON CHARCEABLE

ST STS.

HT HRS.	6:	ũ	29	31	11	33		
1000 FLI CHT MH/FH	0.529	0.073	0.252	0.081	0.041	0.083		
HNE 1964 - Total	529.3	73.0	252.0	80.6	41.1	82.3		
s. 1964 THRU Sched. M H	186.8	44.4	65.7	25.8	24.0	22.8		
RECORD PERIOD - FEB. 1964 THRU MUNE 1964 - 1000 FLICHT HRS. Posched, M.H. Sched, M.H. MH/FH	342.5	24.6	146.4	54.8	17.1	59.5		
RECOS					EXCLUDES G F E		C F " - NOT REPORTED	- NOT REPORTED
	93	28	29	x	x ,	20		
	÷	ن	_	U	J	ပ		
	COMPLETE HELI COPTER	ROTORS	ATRERAME COMPS.	XMSN & DRIVES	POVER PI A NT	INSTS N FLEC.	COMMIN- ICALIONS	WEAPON SYSTEMS

PINKNOMN

TOTAL REMOVALS

	- 3/64 thrn 6/64									
C = CHARCEABLE NC = NON CHARCEABLE	RECORD PERIOD -	102 20	. 19	23 5	7 7 7	20	28	& O	NOT REPORTED	41
) = 0 NC =		C	C	C	C	C NG	ON C	C NC	ION	C
SUB SYS. CATECORY		COMPLETE HELICOPTER	ROTORS	AIRFRAME COMPS	XMSN & DRIVES	POWER PLANT	INSTS. & ELEC.	COMMIN- ICATIONS	WEAPON SYSTEMS	TOTAL REMOVALS
					H-1	7				

TABLE 6-7 R&M DATA (65-12929)

		CUM			FAILURE	S	
MONTH	FLICHT HOURS	FLICHT HOURS	MSN	FS	<u>sys</u>	CUM TOTAL	fr/fh
2/67	18.8	18.8	0	0	o	0	
3/67	146.2	165.0	2	0	13	15	0.0909
4/67	33.3	198.3	1	0	3	19	0.0958
5/67	104.1	302.4	2	0	55	76	0.1818
6/67	142.6	445.0	2	0	51	129	* 0.2898
7/67	0.0	445.0	-	*	13	142	0.3191
8/67	55.0	500.0	1	0	19	162	0.3240

* Periodic Inspection

Total man hours = Scheduled + Unscheduled = 308.2

Maint. man hours per flight hours = 308.2/500 = 0.616 Hr.

TABLE 6-8 R&M DATA (65-12929) TOTAL FAILURES PER SUBSYSTEM

SUBSYS.) =)	C = CHARCEABLE	BLE						
CATECORY	ا بيز بو	io se:	NC = NON CHARCEABLE		MONTH				
		2/67	3/67	79/7	29/5	29/9	19/1	19/8	TOTAL
COMPLETE	ပ	۵	15	4	57	5 3	13	20	162
HELI COPTER	УС	0	m		7	6	0	, -	21
ROTORS	Ú	ø	々	فيو	σ	œ	0	7	24
	NC	٥		۵	7	2	0	0	5
AIRFRAME	Û	0	7	, 1	23	21	Ŋ	1.	79
COMPS	NC	0	7	0	4	5	0	0	11
XMSN &	ر	0	0	0	3	7	2	ю	6
DRIVES	NC	0	0	0	0	~	0	~	2
POWER	ب	0	~ ···	~1	f ~	11	m	2	25 EXCLUDES G F E
PLANT		0	0		-		0	O	3
INSTS. &	ڼ	0	٣	7	15	12	m	9	0,5
ELEC.	NC	0	0	0	0	0	0	0	0
COMPATING TO			9 H	NOT REPORTED	PORTED				
CONTRACT									
WEA PON SYSTEMS			NONE 1	NONE INSTALLED	ED				
TOTAL REMOVALS	υÿ	00	2	7	15	18 6	20	φ	50 12

TABLE 6-9 R&M DATA (65-12930)

		CUM			FAI LUR	ES	
MONTH	FLI CHT HOURS	FLI CHT HOURS	MSN	FS	SYS	CUM TOTAL	FR/FH
2/67	17.3	17.3	0	0	0	0	
3/67	116.2	133.5	2	0	15	17	0.1273
4/67	74.7	208.2	2	0	20	39	0.1873
5/67	27.5	235.7	1	0	14	54	0.2291
6/67	112.4	348.1	2	0	92	148	~ 0.4251
7/67	96.6	444.7	1	0	23	172	0.3867
8/67	55.6	500.3	0	0	26	198	0.3960

* Periodic Inspection

Total Manhours = Scheduled + Unscheduled = 374.8

Maint. Manhours per flight hour = 374.8/500 = 0.749 Hr.

TABLE 6-10 R&M DATA (65-12930) TOTAL FAILURES PER SUBSYSTEM

SVB SYS.	3 = 3%	C = CHARGEABLE XC = XON CHARG	HARGEABLE NON CHARGEA ^A LE	E E					
		2/67	2/67 3/67	4/67	29/5	MONTH 6/67	19/1	8/67	TOTAL
COMPLETE HELICOPTER	သူ	00	17	22	15	96	24 0	26	198 2
FOTORS	S S S	0 0	గద	7 0	r 0	17 Q	9 2	00	31 0
airframe Comps.	C NC	90	\$ 0	% C	7	8° 0	t3 0	15	9 8 0
XMSN & DRIVES	C NC	00	00	10	00	& C)	9	m 0	14 0
POWER PLANT	C NC	00	4~	5	0 3	17 0	40	0	30 EXCLUDES GFE
insts. & elec.	S. N.C.	00	اس م <i>ا</i>	40	0 2	61	ma	40	37
COMMUN- ICATIONS	C NC	ir ক		E "OT REPORTED	6				
WEAPON SYSTEMS		NON	NONE INSTALLED	LLED					
TOTAL REMOVALS	S S S	00	10	\$ 4	12 0	34	13	10	84 16

TABLE 6-11 CONFIRMATORY DATA (PRODUCTION)
TOTAL FAILURES PER SUNSYSTEM

	cler. 5/68	FIVE AIRCRAFT FAILI'RE TOTALS FOR 5269 FLT, HRS,	AVAILASILITY - ACTUAL - 83.47							
C = CHAR'EABLE NC = NON CHARCEASLE	RECORD PERIOD FROM 9/67 CHEC. 5/68	1045 155	83 23	283 15	9 13	220 INCLUDES G F 18	222 83	62 INCLUDES G F	166 0	446 83
SUR SYS C = CHAR CATETORY NC = NON		COMPLETE C HELICOPTER NC	ROTORS C NC	AIRFRAME C COMPS, NC	XMSN & C DRIVES NC	POWER C PLANT NC	INSTS. 6 C ELEC. NC	COMMUN- C ICATIONS NC	WEAPON C SYSTEMS NC	TOTAL C REMOVALS NC
ග යි		Φ₩	řZ	¥Ϋ́	모급 H-22	at a	<u> </u>	8 1	3 50	Z Z

TABLE 6-12 ADDITIONAL PRODUCTION DATA

SERIAL		CUM			FAILURES		
NO. 65-	FLICHT HOURS	FLICHT HOURS	MSN	FS	SYS	CUM TOTAL	FR/FH
		Period of	Record from	1966	delivery to	11/1/67	
21916		4 74	12	0	39	51	0,1075
21917		183	6	0	13	19	0.1038
21918		564	10	0	37	47	0.0833
21919		286	11	0	79	90	0.3147
21921		900	20	0	84	104	0.1156
21923		352	2	0	15	17	0.0483
21925		48 3	5	0	16	21	0.0435
21926		652	6	0	16	22	0.0352
21927		132	5	0	1.9	24	0.1818

TABLE 6-13 ADDITIONAL PRODUCTION DATA TOTAL FALLURES PER SUBSYSTEM

	TOTAL	305	30	۲,	7 4	151	17	11	'n	78	2 -	75	7 47		
	12927	24	~	9	0	10	-	***	0	2	•	\$	0		
	12926	22	~	2	0	-		w	0	4	Q	2			
(RECORD PERIOD FROM 1966 DELIVERY TO 11/1/67)	12925	21	~	7	0	10	~	4	0	2	O	~	0		
DELIVERY	12923	17	~		0	œ	0	m	0	m	0	,			
FROM 1966	12921	104	12	20	4 7	41	9	10	0	11	Q	22	2		
ord period	12919	96	7	7	0	35	7	5	ပ	33	C	10	0		
(REC	12918	47		7	0	15	-	æ	0	11	0	11	0	TED	
4 85.F	12417	14	J	¢	0	r		2	2	•	ω	ŗ	0	NOT REPORTED	NOT REPORTED
C = CHARTEABLE NC = NON CHARTEABLE 5-	12916	5.1	6	5	Đ	16	2	æ		11	ω	16	c)	EL U	NOT R
C = Cl NC = 3 65-		Ų	NC	Ú	N.C	၁	UN	ن	NC	Ú	»KC	C	NC		
SUB SYS CATECORY Ser. No.		COMPLETE	HELICOPTER	ROTORS		AIRFRAME	COMPS.	XMSN 6	DRIVES	POWER	PLANT	INSTS. &	ELEC.	COM NIN- ICATIONS	WEA PON SYSTEMS

H**~**24

UNKNOWN

TOTAL REMOVALS Part C

2.

Data Submitted by Sikorsky

Sikorsky Aircraft -----

TITLE Operations Reliability Maintainability Engineering Frogram Quarterly Eva. Lation Report

REPORT NUMBER . . RP-64276

PREPARED UNDER Contract W. . : \ \ - 11-680-0512 (31 Mod 2008

MEPORY DATE May ..., 1966

HEPORT PERIOD

This report is applicable to the following discreft stadel(s) and contract(s): MODEL CONTRACT

CH-54A

DAA-J01-680-0512 (41) P008

Prepared by Holbert Checked by M. A. Wachs

Approved by S. S. S. Sienney

MEV.	CHAMAED	-	ADDED PAGE(S)	DELETED PARE(S)	DEBÔMPTION	DATE	APPROVAL
::	1.2				9th Quarterly Sumulative Report 10th Quarterly Cumulative Report 11th Quarterly Cumulative Report	15 May 15 Aug 15 Dec	70 70 70
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HEVISIONS CONTINUED ON MEXT PARE



MEPORT NO SER-64276 hev. ... MODEL CH-54A

ABCTRACT

The quarterly Evaluation Report is submitted for the eleventh quarterly period of field data collection as part of the Operations Reliability/ Maintainability Engineering Program, defined in Contract DAA-J01-68C-0512 (31), Data Item 08-010, DA Form 3149-F. The data is cumulative for the 33 month period and all information not compiled in the prior reports has been included as part of up-dating for this report.

CH-54A Operations Reliability data accumulated a total of 47,993 flight hours for the 33 month period. The reliability levels for a one-hour mission based on this data are:

Total Reliability

.7845

Mission Reliability

.9875

Analysis of maintainability data shows the following derivations.

Average Active Maintenance Dountime/Flight Hour	2.3 hrs
Elapsed Mean Time to Repair	1.9 hrs
Average Manhours/Down Hour	2.8 MH
Active Maintenance Manhour/Flight	6.4 MMH/FH
Operational Availability	54.3%

The stable nature of the 2.8 manhours per down hour and ϵ .4 manhours per flight hour values may reflect the maturing of the program and the continuing effort to improve our computer program.

The increase in operational availability from 54.1% to 54.3% is the lirect result of a decrease in reported administrative down time.

Sikorsky Aircraft ----- A.

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REPORT NO CHILLEGETÉ PAR LA CHILLEGE PAR LA CH

ANALESIS.

Sikorsky Aircraft ----- Q.

MEPONY NO SER-64276 Rev. 3

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SUM:ARY

U. J. Army CH-54A operations in the 33 months of ORME data reporting have accumulated 47,993 flight hours and exhibit the following MTBF's (Mean Time Between Failures):

1.1 Failures

4.1. hours

Mission Aborts

80.1 hours

These MTBF's convert to the following reliability levels for a one-hour mission:

Total Reliability*

(1 hour)

.784.

Mission Reliabilly **

(1 nour)

.9875

Hardware discrepancies required 37,562 maintenance man-hours for local corrective maintenance.

Relatively few components contribute to a high percentage of the total aircraft unreliability. At the system level, powerplant, rotors and blades, transmission, instruments, hydraulics and communications account for 67.3% of all primary failures. Powerplant, APP, hydraulics and transmission a count for 73% of all mission abort failures.

The "top ten" components in each of the following categories account for more than:

ili of all failures

15% if all mission abort failures

Now of Hil local corrective maintenance time to repair primary failures

31% of all local corrective maintenance manhours to repair primary failures

^{*} Total Reliability - Probability of no failure in the specified time. This category applies to all classes of failure regardless of degree of severity and includes aborts, downs, minors, and malfunctions with no effect.

^{**}Mission Reliability - Probability that a CH-54A will experience no mission aborting failure in a one-hour mission.

METORT NO. SER-64276 Rev. J. CH-54A

SUMMARY (Cont)

The 33 month cumulative reliability statistics show a slight change in reliability relative to the 30 month figures submitted in the last quarterly report as shown:

	30 Montn Cumulative	33 Month Camulative
CH-54A Total Reliability (1 hour)	.7850	.7845
CH-54A Mission Reliability (1 hour)	.9870	.9875

The distribution of failure rate among systems has changed slightly since the last report. Powerplant, rotors and blades, and transmission remain the top three failure rate systems. Lower MTHF's for instruments, nydraulics and communications now rank these three systems as the fourth, fifth and sixth major sources of unreliability. These six major areas account for 67% of the total aircraft failure rate. Powerplant, APP, hydraulics and transmission still rank as the top four major contributors of mission aborts and are responsible for 73% of the abort rate.

The "top ten" lists of components, R-1, R-2, and R-3, show slightly less impact on total sircraft reliability from top ten components.

Top ten components' contribution to aircraft unreliability have changed only sliketry from that of the previous report:

	30 Month Cumulative	33 Month cumulative
Based on Callure rate	27/0	~5.%
Based on number of failures	22%	
Raseq on abort rate	27%	25%

Sikorsky Aircraft ----

SUMMARY (cont)

New Components in top ten lists and the components they replace from the last quarterly are as follows:

Top Ten Category	New Components In Top Ten List	Components Deleted From Top Ten List
Number of Failure (List R-2)	Rotor Brake Package Assembly P/N 71428	MCB Oil Cooler V Belt P/N 3V600
Abort Rate (List R-3)	Cargo Hoist UP Pressure Tube P/N 6465-62051-061	
Unscheduled Maintenance Manhours (List R-5)	Turbo shaft Engine Exhaust Duct P/N 571076	AFCS Servo Assembly P/N S6265-62551-10

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SUMMARY (Cont)

Projections of component MTBR's (Mean Time Between Removals) based on 33 month cumulative data show slight deterioration from the 30 month cumulative figures submitted in the last report. Higher rates of failure and damage beyond local repair yield generally lower MTBR's. (Note that MTBR's continue to consider overhauls and scrappage arising from both primary failures and damage.)

COMPONENT	MTBR	M. hk
	Based on 30 Month Cumulative Data	Based on 33 Month Cumulative Data
Main Rotor Head Assembly	302 hr	291 hr
APP Clutch Assembly	309 hr	311 hr
Tail Rotor Blade	374 hr	345 hr
Main Hotor Damper Assembly	391 hr	395 hr

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DISCUSSION

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Total Reliability

Figure A-1, the total reliability block diagram covering all major systems shows a 4.12 nour total mean time between failures and .7845 total aircraft reliability for a one-hour mission. The system code digits shown in the block diagram define system boundaries and the hardware included. They are defined in Appendix A2-1 of the ORE Handbook.

There were no changes in the total MTBF or the Reliability covering major systems from the last quarterly report.

	30 Month Cumulative	33 Month Cumulative
MTBF	4.12 hr	4.12 hr
Reliability (1 hour)	.785	.785

Figure A-1 shows powerplant, rotors and blades, transmission, instruments, hydraulics and communications as the major contributors to unreliability. Taken together these major systems account for 67.4% of all failures observed in the reporting period. Figures A-2 through A-7 show the breakout of total reliability among the individual system codes within these areas.

Powerplant - Figure A-2 highlights the engine and engine exhaust areas. Major problem items are tailpipes, flex shafts, fuel controls and exhaust ducts.

Rotors & Blades - Figure A-3 shows both tail and main rotor blades and the main rotor head to be major contributors to unreliability. Major problem items are tail rotor blade erosion, main rotor blade tip caps, and main rotor nead droop restrainers.

Transmission - Figure A-4 highlights the rotor brake, main transmission and MGB oil cooler. Rotor brake pucks & support brackets are large contributors to unreliability. Main transmission faitures are distributed among many component parts. Oil cooler V belts are the highest single contributors to MGB oil cooler unreliability.

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Instruments

- Figure A-5 highlights the instruments (from detector to indicator). The generator tachometer, servo network and the fuel flow transmitter are the major sources of unreliability.

Hydraulics

- Figure A-6 highlights the cargo hoist and flight control hydraulics. Hoist up pressure tube, hoist pump, 1st stage hydraulic pump and the 2nd stage hydraulic manifold are the major sources of unreliability.

Communications - Figure A-7 highlights the ARC-54 VHF radio sets.

Corrective action procedures for increasing the reliability of various components and systems are discussed in detail in SER-64272-1 Monthly Progress Accomplishment Report.

Mission Reliability

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Figure A-8, the total mission reliability block diagram, shows an 59.12 hour total mean time between failures for mission aborts and .9875 onenour mission reliability.

improvement in mission abort MTbF from These levels represent a 5% ine last quarterly report.

	30 Month Cumulative	33 Month Cumulative
MTBF, aborts	76.6 nr	80.2 nr
Mission heliability (1 hour)	.9870	.9875

Figure A-B snows powerplant, APP, hydraulies and transmission continue to be the major contributors to the mission abort rate. Taken together these four major systems account for 73.5% of all mission aborts observed in the reporting period. Figures A-9 through A-12 show the breakout of mission reliavility among the individual system codes within these four areas.

Fowerplant

- Figure A-9 highlights the engine and engine hydraulic start. Fuel controls, engine start hydraulic lines, fuel pumps & flex shafts are important mission abort items.

Sikorsky Aircraft

MODEL CH-54A

APP

- Figure A-10 highlights the APP itself. The APP fuel pressure switch and the APP fuel control are significant abort items.

Hydraulics

- Figure A-11 shows cargo hoist hydraulies account for 55.8% of all hydraulic aborts. Fressure lines are a significant source of mission aborts.

Transmission

- Figure A-12 shows the main transmission and the main gear box cil cooler to be major contributors among transmission systems. The oil cooler V belt is a large single source of aborts.

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TOTAL KELIABILITY BLOCK DIAGRAM - POWERPLANT SYSTEMS

MTBF - 21.8 Hr

Reliability (1 Hr) - .9540

ENGINE CONTROLS MTBF 175.2 R .9943 293020 ENGINE HYD START MTBF 489.7 R .9980 293030 ENGINE EXHAUST MTBF 91.4 R .9891 293010 ENGINE MOUNTS MTBF 539.3 R .9982 293040 MISF 1714.0 R .3934 POWERPLANT 293000 MFBF 298.1 R .9967 EAPS 293050 TURBOSHAFT ENGINE MTBF 46.5 R .9787 JFTD12A-4A

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Figure A-2

Sikorsky Aircraft ----- A.

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POTAL BELIABILITY BLOCK DIAGRAM - ROTOR AND BLADE SYNTEM

MINE - NAME

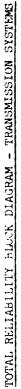
Reliability (1 Hr) - .9665

TAIL ROTOR BLADES MTBF 92.5 R .9892 151600 MAIN ROTOR BLADES MIBF 99.4 R .9900 151500 TAIL ROTOR HEAD MTBF 241.2 R .9959 001171 MAIL HOTOR HEAD MTBF 117.3 R .9915 151000 U__0 00 %e.c∃

Figure A-3

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MTBF - 30.9 hr Relie

Reliability (1 Hr) - .9676

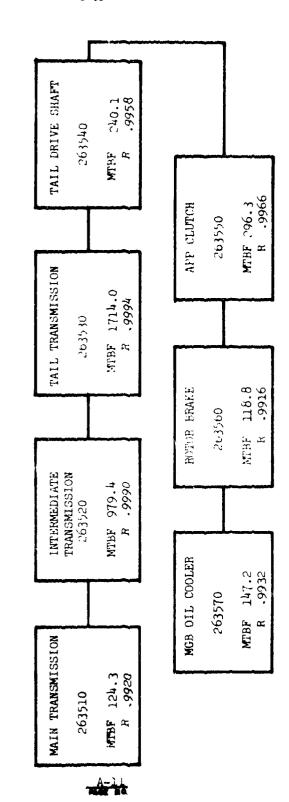


Figure A-h

TOTAL RELIABILLY SLOCK DIAGRAM - INSTRUMENTS SYSTEM

MILBY - 53. C Hr

Reliability (1 Hr) - .9812

MAY INSTRUMENTS MTBF 11998.2 R .9999 514530 ENG INSTRUMENTS MTBF 342.8 P. 9971 214540 FLT INSTRUMENTS 514520 MTBF 290.9 н. 9966 NUMBER TRANSPORTER 514550 MTBF 47992.6 R .9999 A111-43 1988 A111 R JOSES 77.55 MIRF TILE WARNING INSTRUMENTS MTBF 750.0 R .9987 514560 5066. IN STRUMENTS MISE 132.8 514590 ٠٢.

A-12

Figure A-5

TOTAL RELIABILITY BLOCK DIAGRAM - HYDRAULICS SYSTEM

MTBF - 57.4 Hz

Reliability (1 Hr) - .9826

TAIL ROTOR SERVO UTILITY HYDRAULIC 3999.4 .9998 MTBF 432.4 R .9977 456530 045954 MTBF FLT CONT. HYDRAULIC MTBF 1090.7 F .9991 MTBF 243.6 R 9959 AFCS SERVOS 456520 456550 CARGO HOIST HYD PRIMARY SERVO MTBF 461.5 R .9978 MTBF 130.4 R ,9924 456510 756560

Figure A-6

REPORT NO. SER 64276 RPV J MODEL CH-54A

TOTAL RELIABILITY BLOCK DIAGRAM - COMMUNICATION SYSTEM

MTBF ~ 65.5 Hr

Reliability (1 Hr) - .9847

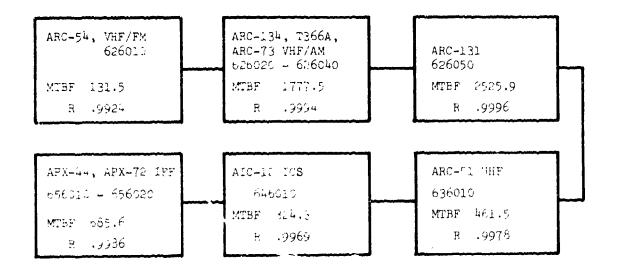
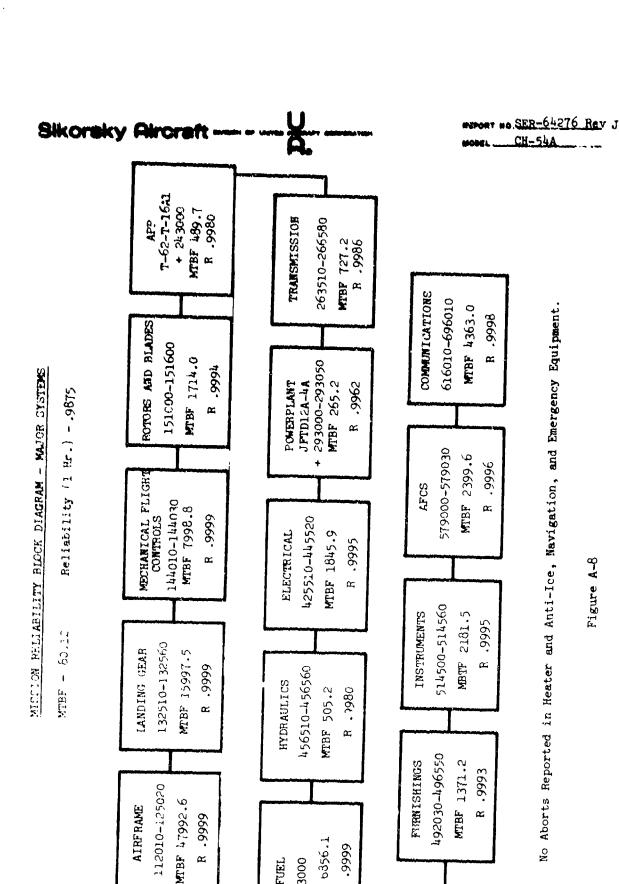


Figure A-7



MTBF 6356.1 R .9999

463000 FUEL

A-15 Page No.

S--16

MISSION RELIABILITY BLOCK DIAGRAM - POWERPLANT STATEMS

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MTBF - 165.2 Hr

Heliability (1 Hr) - ,9962

ENGINE CONTROLS MTBF 4799.3 R .9998 ENGINE EXHAUST MTBF 1654.9 P. .9994 293010 293020 MTBF 47992.6 R .9999 ENGINE HYD START MTBF 1654.9 R .9994 POWERFLANT 293000 293030 TURBOSHAFT ENGINE MTBF 15997.5 R .9999 .9977 JFTD12A-4A 293050 EAPS MTBF R

No Aborts in Other Powergiant System Codes

Figure A-9

A-11

MISSION RELIABILITY BLOCK DIAGRAM - APP

MTBF - 499.7 Hr Reliability (1 Hr) - .9980

APP HYD START
T-62-T-16A-1
243000
MTBF 639.9
RTBF 2086.6
R .9964

Figure A-10

MISSION RELIABILITY BLOCK DIAGRAM - HYDRAULIC SYSTEMS

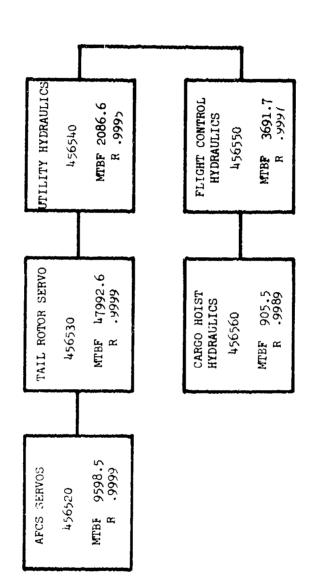
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MTBF - 505.2 Hr

Reliability (1 Hr) - .9980



No Aborts in Other Hydraulic System Codes

Figure A-11

MISSION HELIABILITY BLOCK DIAGRAM - TRANSMISSION SYSTEMS

MTBF - 727.2

Reliability (1 Hr) - .9986

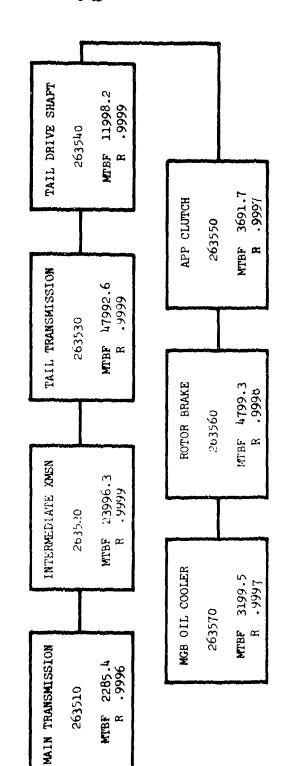


Figure A-12

MEPONT NO. SER-64276 Rev. J

Failure Rates and Reliabilities (Data Item 08-010-1)

SYSTEMS

Table A-1, Section D of this report, provides the failure rates, reliabilities, and abort rates observed in this reporting period by system.

Thirty-three month cumulative behavior shows an increase in the reliability in a number of the systems relative to the 30 month cumulative behavior documented in the previous quarterly report.

Table A-1 shows a high concentration of primary failures in the following areas: powerplant, rotors and blades, transmission, instruments, hydraulics and communications. Taken together the systems in these major groupings account for an observed .163 failures per flight hour, 6 7% of the total .243 failures per flight hour for the overall aircraft.

The ten individual system codes with the highest observed failure rates are as follows:

System Code	Nomenclature	Failure Rate (Failures per hr)	Reliability (1 hour)
JFTD12A-4A	Turboshaft Engines	.021503	.9787
293010	Engine Exhaust	.010939	.9891
151600	Tull Rotor Blade	.010814	.9892
151500	Main Rotor Blade	.010064	.9900
514500	Instruments	.009731	.9903
151000	Main Rotor Head	.008522	.9915
263560	Rotor Brake	.008418	.9916
263510	Main Transmission	£ 40800.	.9920
456560	Cargo Hoist Hydraulics	.007668	.9924
626010	ARC-54 VHF/FM	.007605	.9924

Taken together these ten system codes account for .103 failures per flight hour, 43% of the aircraft total.

Table A-1 shows a continued high concentration of mission abort failures in four areas: powerplant, APP, hydraulics, and transmission. Taken together the systems in these four major groupings account for an observed .0092 aborts per flight hour, 74% of the total .0125 aborts per flight hour for the overall sircraft.

The ten individual system codes with the highest observed abort rates are as follows:

System Code	Nomenclature	<u>Failure Rate</u> (Failures per hour)	Reliability (1 hour)
JFTD12A-4A	Turboshaft Engines	.002271	.9977
T-62-T-16A1	APP	.001563	.9984
456560	Cargo Hoist Hydraulics	.001104	.9989
495020	Cargo Winch	.000667	.9993
S 293020	Engine Controls	.000604	ا پا999.
293030	Engine Hydraulic Start	.000604	.9994
24 3000	APP Hydraulic Start	.000479	.9995
263510	Main Transmission	.000438	.999€
514500	Instruments	.000346	.9996
425520	Generator	.000354	.9997
263570	MGB Cil Cooler	.000313	.9997

Taken together these ten system codes account for .0088 abort failures per flight hour, 71% of the aircraft total.

The MGB Oil Cooler System code is a new entry in this list replacing the Utility Hydraulic system code present in the previous 30 month cumulative list. The Engine Controls and Engine Hydraulic Start system codes have tied with the fifth highest abort rate.

Sikorsky Aircraft ---- - --- A.

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Table A-1 shows a continued high concentration of maintenance manhours to repair primary failures in four areas: powerplant, transmission, rotors and blades, and hydraulics. Taken together the systems in these four major groupings account for an observed 25,290.8 maintenance manhours to repair primary failures, 67% of the total 37,662.2 manhours to repair all primary failures in all aircraft systems.

The ten individual system codes with the most maintenance manhours for primary failure repair are as follows:

System Code	:Iomenclature	Maintenance Manhours to Repair Primary Failures
JFTD12A-4A	Turboshaft Engines	6359.2
151000	Main Rotor Head	3849.7
263510	Main Transmission	3139+5
450500	Cargo Hoist Hydraulies	2490.4
495020	Jargo Winch	1382.6
191500	Main Rotor Blade	1172.4
ire300.	Pae.	1168.8
1m1; m1=,1,A,	API	10 ⁸ 7.7
****	This Foot Blade	2777.
£5	Engine Exhausts	1045.0

Take: together these ten system codes account for 21,179.2 maintenance mannours, 56% of the total required to repair all primary faitures observed on the aircraft.

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Table A-1 shows a continued high concentration of elapsed maintenance time to repair primary failures in five areas: powerplant, transmission, rotors and blades, hydraulics and airframe. Taken together the systems ir these five major groupings account for an observed 15,526.3 elapsed hours for maintenance to repair primary failures, 69% of the total 22,530.9 hours to repair all primary failures in all aircraft systems.

The ten individual system codes with the most elapsed time for primary failure repair are as follows:

System Code	Nomenclature	Elapsed Time for Primary Failure Repair Active Maintenance
JFTD12A-4A	Turboshaft Engines	3158.9
263510	Main Transmission	1628.1
151000	Main Rotor Head	1310.5
4965bC	Cargo Hoist Hydraulies	949.9
151600	Tail Rotor Blade	732.2
* 293010	Engine Exhaust	715.7
+35020	Cargo Winch	711.8
ar, 5 :50	Fuel	716.8
151502	Main Rotor Blade	663.3
T-67 -T-16A1	APP	650.9
263560	Rotor Brake	637.4

Taken together these system codes account for 11869.8 elapsed nours, 53% of the total required to repair all primary rantures observed on the aircraft.

*The system codes present in the previous 30 month cumulative list have remained virtually the same, except the order has changed.

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COMPONENTS

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Table A-2, Section D of this report, provides the failure rates, reliabilities, and abort rates observed in this reporting period by component.

Within each system code Table A-2 arranges components alpha-numerically my Dikorsky and vendor part number of three levels of hardware, assembly, subassembly, and component. Corresponding federal stock numbers are also shown.

List R-1 in this section shows the ten assembly part numbers with the highest reported failure rates. Taken together they contribute 15% the total aircraft failure rate. There are no new additions or delectors to List R-1 for the last quarter.

R-1 printout entries correspond to the part numbers shown. In some cases Table A-2 reports additional failures of the same hardware against alternate part numbers so that the actual number of failures, component failure rates, and percentages are higher.

In general, the K-l printout reflects the hardware level at which component replacement was performed on the aircraft. Major components such as the main transmission, for which Table A-l shows a total .008043 failures per hour, do not appear since these failures are distributed among IJI separate lower level assemblies, each of which is repairable or replaceable on the aircraft.

h-1 entries for the engine exhaust tailpipe, tail rotor blade, and rotor brake support bracket identify the failed hardware meaningfully, in sufficient detail to show where reliability improvement at the component level can provide a relatively high yield in total failure rate reduction.

Other entries require additional explanation. Table A- ν in Jection L shows that:

Approximately 18% of all APP clutch malfunctions were traced to SB1125-1 bearings. An increase in failures in other subsystems has diluted the effect of the clutch problem relative to the total system.

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Approximately 41% of all engine malfunctions diagnosed below the assembly level are attributable to exhaust ducts, fuel controls, fuel pumps, and shafts. Note that Table A-1 shows 1032 failures against the engine system code, more than four times the number shown in R-1. The remaining 784 are distributed among alternate part numbers and engine component parts accessible for on-aircraft repair or replacement.

Approximately one-quarter of all rotor brake malfunctions diagnosed below the assembly level are attributable to brake pucks. Puck failures together with rotor brake support bracket failures account for almost one half of all diagnosed failures. Note that Table A-1 shows 404 failures against the rotor brake system code, more than four times the number shown in R-1. The remaining 319 are distributed among alternate part numbers and rotor brake component parts accessible for on-aircraft repair or replacement.

Approximately 20% of all anti-collision light failures are attribitable to MAC5338-7079 incandescent right failures. The Arrandows 313 failures against the exterior light system code, more than twice the number shown in R-1. The remaining 172 are distributed among alternate part numbers and various components accessible for on-aircraft repair or replacement.

Approximately 20% of all MGB oil cooler mulfunctions below the assembly level are attributable to the upper, lower and liter pulleys. Table A-1 shows 326 failures against the MGB oil cooler system code, more than twice the amount shown in P-1. The remaining 194 are distributed among various components accessible for on-aircraft repair or replacement.

A complete evaluation of ARC-54 failures is impossible because it requires additional data that is not currently available to ORE's. Meaningful identification of failure phenomenon requires electronic diagnosis within the receiver-transmitter to the component level. Current maintenance facilities at CH-54A operation sites do not permit such diagnosis. (The ARC-54 is being replaced by the ARC-131.)

The ARC-51 UHF receiver-transmitter is similar to the ARC-54 receiver-transmitter in that additional electronic diagnosis within these units is necessary for true component level reporting. Its failure rate is substantially lower and the effects of its failures upon mission reliability, maintenance manhours and elapsed maintenance downtime is substantially less. Depending upon the exact nature of the failure modes, failure rates may be reasonable and justified in light of the complexity inherent in this unit. Table A-1 shows an observed 461.5 hr MTBF for the ARC-51 system, - a level more than four times higher than the 100 hr specified by procurement specification MIL-R-22659B (AS).

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In order to identify problem areas and possible future problems, additional top ten lists are included for the first time. These new lists are identified by the suffix A, and include only the data received during the past 3 month period. In this way we can better determine what are the current problem areas and if a potential fix has been made, whether or not it is effective.

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List R-2 in this section shows the ten part numbers with the highest reported number of failures. This criterion spotlights cases where component failure rates below R-1's top ten combine with high quantities-per-aircraft to yield significant contributions to the total aircraft failure rate. Note that List R-1 accounts for approximately 21% of the total aircraft failure rate while list R-1 accounts for only 15%. Specifically List R-2 shows that:

6415-20209-041 Main Rotor Blade Tip Cap
6415-20201-041 Main Rotor Blade Assembly
65160-00001-045 Tail Rotor Blade Assembly
6435-60028-010 Tail Drive Shaft Support Assembly
71426 Rotor Brake Package Assembly

fall below List R-1's top ten on the basis of failure rates but contribute substantially to aircraft unreliability.

The Rotor Brake Package P/N 71428 is a new entry in R-2 replacing the M35 Jil Jeller V Belt P/N 3V600 present in the previous 30-month cumulative list.

List P-2A shows those items with the highest number of failures which have occurred during the past quarter. A review of the Monthly Accomplishement Report JEP 6+272-1, will describe the corrective action taken.

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		<u>-</u>	REV J					
PLIGHT TIME	47992.6	:	AIRCHAFT	SERIAL	AIRCHAFT SERIAL 140. RANGE	77	1	
COPPORENT P/N	COMPONENT P/N NOMEIKCLATUKE	MO. OF FAILURES	COMP. FAILURE RATE	PER A/C	TOTAL FAILURE RATE Befores	PERCENT OF A/C FAIL, RATE		,
626010 RT-348/ARC-54	ARC-54 VHF REC-TRANS.	312	.006501		105900*	2.7		
293010 643 6-8 0601-082	ENGINE EXHAUST TAIL PIPE ASSY	431	064400*	٨	.008961	, t		
26.3550 56137-91000-015	APP CLUTCH	140	-16200		.002917	5.2		
JFTD12A-4A 572200	TURBO-SHAFT ENG ENGINE	248	.002584	~	.005167	2,5		
616010 RT-742/ARC-518X	ARC-51 UHF	96	.001792	-	.001792	1.		
263560 6465-28016-612	ROTOR DRAKE SPT ROTOR ERAKE	58	144100.	-	.601771	<u> </u>		
579010	AFCS AMPLIFIER AMPLIFIER CONTR	r	.001500		.601500	ø.		
445510 HS25277-2	EXTERIOR LIGHTS LIGHT ANTI COLL	141	. 001469	N	.602938	1.2		
579030 5490-50131-011	REMOTE STICK REMOTE STICK	19	965100°	!	.00139£	9.	-	
263570 3V600	MGB OIL COOLER V BELT	132	.601375	~	.002750	1.1		
			 	1 1 1				
			!	(•			

LLIBRA INE	3001.2		AIRCHAPT	SERTAL	AINCHAFT SERTAL NO. RAMBE		
							•
į		% .0	COMP. FAILURE	PER	TOTAL FAILURE	PERCENT OF A/C	;
SSSSSSSSSSSSSSSSSSSSSSSSSSSSSSSSSSSSSS	CONTORCE TO BE CONTORCE CONTOR	*********	RATE	7:	KATE	FAIL, RATE	
93010 6430-60601-062	ENGINE EXHAUST TAIL PIPE ASSY	26	966100	~	966600*		
28010 RT-348/ARC-58	ARC-S4 YNF MEC-TRANS.	23	.004332	~	365+00°	1.9	
\$5558 \$6137-91000-015	APP CLUTCH	2	966500	, **	.003998		
79010	AFCS AMPLIFIER AMPLIFIER CONTR	•	.002664		.002665	N .	
263510 6435-20480-647	HAIN THANSHISION MAIN BEAR BOX	un	.001666		.001666	۲.	
26655 RT-623/ARC-131	MAC=131 REC=TRANS	•	.001666	-	.001666		
93020 6430-80326-101	ENSINE CONTROLS ACTUATOR SPEED	•	.001499	N	. 002999	m.	
F7012A-4A 571078	FUEL CONTROL	•	.001499	•	.002999	V•4	
79036 6490-60131-011	MENOTE STECK RENOTE STICK	•	.001333	-	.001333	9.	
*95010 XN20403H90-20	WIPER ASSY	•	.001333	~	.002646	1,2	

10N - ACL													
TO 760930 LOCATION	- ALL	PERCENT OF 101AL No. FAILURES		3.7	2,7		1.9	1.00	1.3	1.5	2.1	1.2	
FROM: 680101	SERIAL NO. RANGE -	OTY TOTAL PER FAILURE A/C RATE \$15 \$15 \$15 \$15 \$15 \$15 \$15 \$15 \$15 \$15	909099° 9-	2 .008961	1 .006501	2 .005167	\$99400. 4	41300. 9	5 .003105	2 .002936	1.002917	000000 0-	
7	Ľ,	COMP. EAILURE ES RATE	0000000	064400- 1	106500	* 00259*	191000.	.000736	.000621	.061469	116200:	000000	
List R.2		RO. OF FAILURES	LADE T/R 477	ST 431	315	ENG 248	BLADE 225	LADE FA/R 212	SHAFT [49	HTS COCT 141	140	ENSSY 134	
OF FAILURES	47992.6	HOMELICL ATUR	TAIL ROTOR BLADE BLADE ASSY T/R	ENGINE EXHAUST TAIL PIPE ASSY	ARC-S& VHF REC-TRAUS.	TURBO-SHAFT ENG	MAIN ROTOR BY	MAIN ROTOR BLADE BLADE ASSYS, H/R	TAIL ORIVE SHAF SUPPORT ASSY	EXTERIOR LIGHTS LIGHT ARTI COLL	APP CLUTCH	ROTOR GRAKE BRAKEPACKAGEASSY	
S TOP TEN - NUMBER	FLIGHT TINE -	COMPONENT P/N HOMELICLATURE	151600 65160-045	293010 6430-80601-082	626910 RT=3487ARC=54	JFT0124-4A 572206	151500 6415-20209-041	1515@0 6415-20201-041	263540 6435-60028-010	##5510 #\$25277~2	263550 56137-91000-015	263560	

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	3001.2		ATRCRAFT	SCRIBE	SERTHE NO. PRINCE		
			e de Co	Ę	10741	PEACENT	
CONFORCAT P7/A NOVEN	NONENCLATORE ************************************	HO. OF FATCURES	FAILUME	ěK:	FAILURE	OF TOTAL NO. FATLURES	
29301C CASO-1098 TAIL	EMBINE EXHAUST TAIL PIPE ASSY	8	866 100	N	965600.	5.4	
263396 TAIL D 6435-6028-010 SUPPO	TAIL DAIVE SHAFT SUPPORT ASSY	18	.001200	w	.005996	2.	
191988 6415-20201-041 BLADE	RTH ROTOR BEADE BLADE ASSY MR	13	**6000.	•	. 005664	2.5	
#25019 #EC-9	NC-St VIF	13	.004332	•	.004332	6.3	
CONTRACTOR OF THE CANADA CANAD	AP CLUTCH	3	966500.	*	.003996		
71426 SALIC	NOTOR BRANE BRANEPACKABEASSY	3	.000000	7	. 000000	•	
151906 65161-00001-041 TAIL	TATE NOTOR BLADE TATE ROTOR BLADE	3	.001000	•	966500	9 1	
151506 65166-0001-045 8LAD	TATL ROTOR BLADE BLADE ASSY T/R	4	. 000000	4	. 000000	0	
191900 6415-20209-041 CAP	MIN NOTON BEADE	92	.000555	•	.003332	1.5	
263626 6436-86326-101 ACTU	ENERGE CONTROLS ACTUATOR SPEED	•	.001499	*	.00200	2.0	
S		! :		9	A-X2		

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List R-3 in this section shows the ten component part numbers with the highest reported mission abort rates. Taken together they contribute 25% of the total mission abort rate.

The Cargo Hoist Up Pressure tube, P/N 6465-62051-061, is a new entry in R-3 replacing the Generator, P/N 28B139-33A, present in the previous 30 month cumulative list.

R-3 printout entries correspond to the part numbers shown. In some cases Table A-2 reports additional aborts of the same hardware against alternate part numbers so that the actual number of aborts, component abort rates, and percentages are higher.

R-3 shows 22% of the total mission abort rate concentrated in engine, APP, powerplant and engine control components necessary for the engine start cycle.

Virtually all R-3 entries are well defined. Components are identified meaningfully - in sufficient detail to show where reliability improvement at the component level can provide a reduction in the total abort rate. List R-3A shows those components with the highest report mission abort rates during the last quarter.

List R-4 shows the ten component part numbers with the most reported elapsed active maintenance time required to repair primary failures. R-4 highlights cases where the combined effects of high failure rates and lengthy times to repair have an overall large impact on the total maintenance required to support the aircraft. Taken together these ten components are responsible for approximately 26% of the total time required to repair all observed primary failures.

There has been virtually no change in List R-4 from the previous 30 month cumulative list.

List R-4A shows those components with the most reported elapsed active maintenance time required to repair primary failures during the last quarter.

FLISHT TINE -	47992.6		AIRCRAFT	SERIAL	NO. RAHOE	- ALL	
ara independent	MAAETUTI ATTIGE	*00 *00 *00 *00 *00 *00 *00 *00 *00 *00	COMP. ABORT	YES .	TOTAL ABORT	PERCENT OF A/C	
***********	24444444444444444444444444444444444444	3968696*	999999	200	4086808	20000000	
293030 55#5C3E23#000	ENGIHE HYD START HÖSE ASSY PRESS	17	.000354	. ••	*80000*		
JFT012A-4A 571878	TURBO-SHAFT ENG FUEL CONTROL	26	.000333	2	.000667	P.S.	
T-62-T-16A1 #4936-U	APP FUEL CONTROL TIPP	e,	262000?	-	*000242		
7-62-T-1641 37697-0	APP FUEL PRESS		.600271	-	.000271		
7-62-7-1641 37747-160	\$. 75	.000250	-	.000250	2.0	
263550 56137-91066-015	APP CLUTCH	-	.000229	-	*000229		
JFT012A-4A 572200	TURBO-SHAFT ENG		.000219	N	36 4000°	7.5	
243800 538Kg4GG1	APP HYD START STARTER APP	10	.600208		.000208	LI	
495@20 6456-62106-102	CARGO WINCH RELEASE CARGO	, :	. 000208		.000208		
456560 6465-62051-061	CARGO HOIST HYD. TUBE P HOIST UP	100	.000168	, \	.000188	1.3	
, si		,	, ;	6	7-7		

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TOP TEN - ABORT RATE	List	R-14	Rev 3	Ę.	FRON: 700701	10 700930	LOCATION - ALL
PLIBIT TINE	3001.2		ATRCRAFT	SERTAL	SERTAL NO. RANGE	Att	
		9	COMP.	7.0	TOTAL	PERCENT OF A C	
COMPONENT PAN	HORENCLATURE	ABORTS	FATE	¥:	RATE	MONT RATE	
FTD124-44 571078	TURBO-SHAFT ENS FUEL CONTROL	n	.000500	₩,	.00100.	10.7	
151000	MAIN ROTOR HEAD FLUID TANK COVER	-	.000333	-4	.000333	•	
263518 35016C	METH TRANSMISTOR	1	.000333	-	.000333	3.6	
263516 6435-20140-108	WIN TRANSHISTON COUPLING SPLINED		.000333	-	,000333	9,6	
26351G 6435-20400-647	WATH TRANSMISTON MAIN GEAR BOX		.000333	#	.000333	3.6	
293826 6430-66326-101	ENSINE CONTROLS ACTUATOR SPEED	•	. 000333	~	999000	7.1	
*56560	TUBE P HOIST UP	•	.000333	-	.000333	9.6	
495626 PT06SP22-21P	CONNECTOR PLUS		.000333	**	.000333	9.6	
*5040 6450-62352-104	CRANGE WINCH DECOUPLER	-	.000333	-	.000333	3.6	
495508 6490-60220-011	PANEL ASSY, FIRE	-	.00033	~	.000333	3.6	
		•					
	-			Pase	16E A-35	5	
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### ### ### ##########################	
TURBO-SHAFT ENG ENGINE 1352. MAIN TRANSMISION 754. TURBO-SHAFT ENG FUEL CONTROL 703.	
20400-047 MAIN TRAISMISION 754. A-4A TURBO-SHAFT ENG 703.	
TURBO-SHAFT ENG FUEL CONTROL 703.	
451600 65160-00001-045 BLADE ASSY T/R 683, 3.0	
293010 6438-80601-082 TAIL PIPE ASSY 646, 2.9	
## 348/48C-54 REC-TRAHS. 424. 1.9	
263540 TAIL DRIVE SHAFT 570. 1.6	
263559 APP CLUTCH 56137-91886-015 APP CLUTCH 329, 1.5	
151500 HAIN ROTOR BLADE 508. 1.4	
151590 HAIN ROTOR BLADE 596. 1.3	

LOCATION - ALL

FROM: 680101 TO 700930

10P TEN - ACTIVE ELAPSED MAINTENANCE IIME

*

TOP TEN - ACTIVE ELAPSED MAINTENANCE TIME

- PLEBRIT TERE

FROM: 708701 TO 700930

LOCATION - ALL

SOOL, 2. LIST R-4A REV J

COMPONENT PYN	COMPONENT-PTW NOMENCLATURE	ACTEVE ENT *******	PERCENT OF A/C TOTAL	
263510 6435-20400-047	MAIN TRANSMISION MAIN GEAR BOX	102.	8.1	
263540 6435-60028-010	FAIL DRIVE SHAFT SUPPORT ASSY	89	ຄຸ	
JF 1012A-4A 572200	TURGO-SHAFT ENGT	67.	: ; ; • • •	
JFT0124-44 571078	TURBO-SHAFT ENE FUEL CONTROL		4.7	
293010 6430-60601-0 62	ENGINE EXHAUST TAIL PIPE ASSY	5	9,6	
203390 56137-91000-0°5	APP CLUTCH	29.	2.3	
#63000	רטב. כבון דטבו	28.	1.9	
496510 51565-20421-10	PRIMARY SERVO SERVO M/R	20.	1.6	
131500 6415-20201-041	MATH ROTOR BEADE BLADE ASSY MR	19.		
JFT012A=4A 571076	TURBO-SHAFT ENG BUCT EXH TURBENE	19.	₩7.	
:		1		

List R-5 shows the ten component part numbers with the most reported maintenance manhours required to repair primary failures. R-5 highlights cases where the combined effects of high failure rates, lengthy times to repair, and required large complements of maintenance personnel have an overall large impact on the total aircraft maintenance burden. Taken together these ten components are responsible for 31% of the total maintenance manhour work load required to repair all primary failures.

The Turbo Shaft Engine Exhaust Duct, P/M 571076, is a new entry in R-5 replacing the AFCS Servo Assembly, P/N 86265-62551-10 present in the previous 30 month cumulative list.

R-5 printout entries correspond to the part numbers shown. In some cases Table A-2 shows additional maintenance required to repair primary failures of the same hardware against alternate part numbers so that the actual maintenance times and percentages are higher.

List R-5A shows those components with the most reported maintenance manhours required to repair primary failures, during the last quarter.

R-S Rev J	UNSCHED, PERCENT OF HANHOURS A/C TOTAL		1854, 4,9	1466, 3,9	1005. 2.7	954, 2,5	746, 2,0	724, 1.9	659, 1,8	657, 1.7	351.
47992.6	COPPOHENT P/N NOME (CLATURE	9N3 1:	MAIN TRANSMISSION MAIN GEAR BOX	TURBO-SHAFT ENG FUEL CONTROL	TAIL ROTOR BLADE BLADE ASSY 1/R	ENGLISE EXHAUST TAIL PIPE ASSY	HEAD ASSY HR	TAIL DRIVE SHAFT SUPPORT ASSY	MAIN ROTOR BLADE BLADE ASSYSIM	HEAD ASSY MR	TURBO-SHAFT ENG DUCT EXH TURBINE

LOCATION - AL	
FROM 786761 TO 788930 LOCATION - AL	
F.	ATRCRAFT SERTEE W
TOP TEN - UNSCHEDULED MAINTENANCE MANHOURS	FLIGHT THE - 3001:2

**************************************	NONENCLATURE	UNSCHED.	PERCENT OF	
263510 6435-20400-047	WATH TRANSMISION MAIN GEAR BOX	266.	611	
; '	TURED SHAFT ENG ENGINE	795		
6435-66028-010	TATL DRIVE SHAPT SUPPORT ASSY	138.	6.0	
371078 571078	TURBO-SKAPT ENE- FUEL CONTROL	105.	6.7	
293016 6436-662	THE PIPE ASSY	99	2.7	
191986 6415-25281-641	METH ROTOR BLADE BLADE ASSY HR	57.	2.5	
132536 6425-50102-014F	MITH LANDING OCKN. STRUT ASSY	58.	8.8	
243510 6435-20460-627	MAIN TRANSKISTON MAIN GEAR BOX	3	. 6.4	
4430-42094-013	כבוד צחבר מבר	33.	2,3	
JF7012A-0A 571076	TURES SHAFT ENG DUCT EXH TURSINE	25	8.9	
		:		
23		726	E 4-40	

Mean Time Between Removals (MTBR)

(Data Item 08-010-2)

The component control table, Table A-3 in Section D, provides MTBR's for all on-condition and TBO components listed in TB 55-1500-307-25, October 1968.

For each component, the analysis combines the reported number of unscheduled removals beyond local repair, the accumulated component flight time, and the TBO or retirement interval currently in effect to project long term estimates of mean time between removals.

Table A-3 continues to show the effect of secondary failures and damage on the MTBE of relatively few components.

Component

Effect of Secondary Failures and Damage on MTBR

Secondary Failure and Damage Rate Primary Failure Rate

Main Rotor Blade	1.89
Cargo Hoist Cable Assembly	1.19
Main Rotor Head	1.08
Engine Assembly, Turbo	.72
Cargo Hook	.26
Main Gear Box	.24

Eleven other component MTBR's are slightly affected by secondary failure and damage. The effect on these components is less than CDF of the primary failure rate.

Relative to the last quarterly report Table A-3 shows 18 components with lower MTRR's and 8 with higher MTPR's. As outlined above, except for relatively few components the effect of adding secondary failure and damage removals is clight. In general, lower MTBR's are attributable to higher rates of primary failure requiring overhaul or scrappage.

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Table A-3 identifies the following as the lowest projected MTBR items:

Component	MTBR Based on 30 Month Cumulative Data	MTBR Based on 33 Month Cumulative Data
Main Rotor Head Assembly	322 hr.	291 hr.
APP Clutch Assembly	309 hr.	311 hr.
Tail Rotor Blade	374 hr.	345 hr.
Main Rotor Damper Assembly	391 hr.	395 hr.

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MAINTAINABILITY

ANALYSIS

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MEMORY NO SER-64276 Rev. J

MAINTAINABILITY

SUMMARY

1

This section provides detail reporting of the following program requirements:

- Average Active Maintenance Downtime/Flight Hour
- On-Aircraft MTTR (Mean Time to Repair) for Components, Subsystems, and System
- · Average Manhours/Active Maintenance Downhour
- · Active Maintenance Mannours/Flight Hour

The data inputs are compiled and tabulated using electronic data processing with programming techniques to provide detailed runs for the above items. The computer programs for maintenance, utilization and availability data are equipped to process data on ten million total cumulative elapsed nears and manhours and 100,000 corrective or preventive maintenance actions. These programs provide averages and rates directly applicable to the contract data items.

Hased on analysis of the 33 months accumulated data from all locations, the resultant values of the above characteristics are summarized as follows along with the net change from that of the previous quarterly report:

	CHARACTERISTICS	Value	Trend
·.	Average Active Maintenance Downtime/Flight Hour	2.3	40.1
2.	Elapsed Mean Time to Repair (Corrective, elapsed)	1.9	<u>+</u> 0.0
3.	Average Manhours/Downhour	2.8	±0.0
4.	Active Maintenance Manhours/Flight Hour	6.4	±0.0

Organization codes cited on the Tables in Section D are identified in Amendment 1 of the ORE Handbook.

Average Active Maintenance Downtime per Flight Hour (Data Item 08-010-4)

The presentation of this data item has been expanded to display (1) the current calendar quarter and (2) the total cumulative data. The analysis is further subdivided to permit comparison of maintenance activity characteristics between USAREUR, RVN and CONUS operations for the above calendar periods.

Based on all contract data inputs for 33 calendar months, the cumulative average active maintenance downtime per flight hour (for corrective and preventive maintenance actions) is as follows:

	CONUS	RVN	USAREUR	ALL LOCATIONS
Corrective Maintenance DH/FH Preventive Maintenance DH/FH	0.7 1.6	0.5 <u>1.8</u>	0.5 2.0	0.5 <u>1.8</u>
Total Maintenance DH/FH	2.3	2.3	2.5	2.3

The complete analysis is presented in Table B-1 of Section D.

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On-Aircraft Component and System Mean Time to Repair (MTTR) (Data Item 08-010-5)

The MTTR for corrective maintenance actions, as defined in the ORE Handbook, is presented in Tables B-1 and B-2 of Section D. The analysis is presented by total aircraft and major subsystem for (1) the current calendar quarter and (2) the total cumulative data. The analysis is further subdivided to permit repair time comparisons between USAREUR, RVN and CONUS operations for the above calendar periods. The analysis for component MTTR is an extensive data run and therefore is presented only for the cumulative 33 month period at all operating locations combined.

Based on corrective action data inputs from all locations for the 33 months of the program, the cumulative average active elapsed repair time for the total CH-54A system is as follows:

CONUS -	RVN	USAREUR	ALL LOCATIONS
1.7 hrs	2.0 hrs	2.0 hrs	1.9 hrs

Refer to Tables B-2 and B-3 of Section D for major subsystem breakout and component analysis data run. Also, the MTTR_{e} and MTTR_{m} for the major subsystems is graphically displayed in Figure B-1, page B-5.

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CH-54A Model

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FLIGHT CONTROLS THIS S HYDRAULIC 1111131 AIRFRAME 1111/31 APP 111/22 LANDING GEAR HEATERANTI-ICE 7719 NAVIGATION 113 AFCS / 10 ELECTRICAL

ROTORS & BLADES

SYSTEM .

FUEL SYSTEM

TRANSMISSION

POWER PLANT

FURNISHINGS

INSTRUMENT

COMMUNICATION

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William .

MITTELL 42

1111377.43

MEAN. TIME TO REPAIR

ELAPSED HOURS (MTTR.)

M' MANHOURS (MTTRJ)

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24

HOURS

FIGURE B-I:

MEAN CORRECTIVE MAINTENANCE TIME -ALL LOCATIONS -33 MONTH AVERAGE

Page Sp.

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Average Manhours per Active Maintenance Downhour (Data Item 08-010-6)

The average active manhours per active maintenance downhour is presented for the total CH-54A system in Tables B-1 and B-2, and for subsystems and components in Table B-3, Section D of this report.

The analysis is presented for (1) the current calendar quarter and (2) the total cumulative data. The analysis is further subdivided to permit comparison between USAREUR, RVN and CONUS operations for the above calendar periods.

Active maintenance manhours per flight hour are also of prime interest in evaluating the weapon system characteristics. This value is cited along with active manhours per downhour in the following summation of the 33 months accumulated data.

	MH/DH		MH/DH		USAR MH/DH			MH/FH
Corrective Maintenance Preventive Maintenance	1.2 3.4	1.15 5.36	1.9 3.0	0.91 5.46	1.4 2.4	0.72 4.80	1.8 3.0	0.95 5.41
Combined	2.9	6.51	2.8	6.37	2.2	5.52	2.8	6.36
Spares Cannibalization		0.13		0.07		0.20		0.09
Total		6.64		6.44		5.72		6.45

Data input totals for the above calculated values are shown in Tables B-1 and B-2 of Section D.

A further analysis by maintenance levels of the above active MH/FH for the 32 months accumulated data, excluding cannibalizations, is as follows:

	CONUS	RVN	USAREUR	All Locations
Org. Level - Corrective MH/FH Org. Level - Preventive MH/FH Sub-total	0.78 <u>5.32</u> 6.10	0.68 <u>5.28</u> 5.9	0.25 4.76 5.0	0.68 5.27 5.95
Direct Support - Corrective MM/FH Direct Support - Preventive MH/FH Sub-total Total	0.37 0.0 <u>4</u> 0.41 6.51	0.23 0.18 0.18		
B:	-6 1 No.			S-49

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AVAILABILITY AND UTILIZATION
ANALYSIS

MEPONY NO. SER-64276 Rev. J MODEL CH-54A

Availability and Utilization

SUMMARY

7

The data submitted within this section includes the following categories:

- Inherent Availability
- . Achieved Availability
- . Operational Availability
- . Mean Configuration Change Time
- . Average Flight Hours
- . Average Flight Duration
- . Average Turnaround Time

Each additional recurring quarterly report will be provided with an increasingly larger sample of accumulated data on which to base these tabu-lations and averages.

Included in this report are tables showing the types of missions flown as coded in the field and identified in the ORME Handbook, Appendix 1~5. These tables identified as Aircraft Utilization - Flight Time and Mission Type (Tables C-18 thru C-34) are located in the Appendix Section for reference.

Flight data as shown in D-B and D-C Tables reflects only that flying time on the aircraft under cognizance of the Operations Reliability Engineer in the field and not the total flying hours of all CH-54A aircraft for the program period.

based on analysis of 33 months accumulated data, resultant values of the above characteristics are summarized as follows along with the net change from that of the previous quarterly report.

CHARACTERISTICS	Value	Trend
Inherent Availability	57.2	-10.7%
Achieved Availability	89.2%	+0.3\$
Operational Availability	54.3%	+0.2%
Mean Configuration Change Time (Elapsed Hours)	0.4	±0.0
Average Flight Hours/Quarter/Aircraft	69.3	-1.0
Average Flight Duration-Hours	2.6	+0.1
Average Turnaround Time (Elapsed Hours)	0.2	+0.0

The operational and inherent availability is graphically displayed in Figures C-1 and C-2, pages C-9 and C-10, respectively.

C-2

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Sikorsky Aircraft ----- A.

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Inherent Availability (Data Item 08-010-7)

The inherent availability, as defined in the ORE Handbook, is a measurement of availability in terms of inherent reliability (MTBF) and average repair times for those malfunctions used to calculate that reliability. It is expressed by:

$$A_i = \frac{MTBF}{MTBF + MTTR_e}$$

The inherent availability is shown below for the total 33 month cumulative data:

	Cumulative Data 33 Months All Locations	<u>3rd Qtr 1970</u>
Flight Time, Hours*	47,394	3,001
Quantity of Primary Failures**	11,640	667
MTBF, nours	4.12	4.49
Downtime for Failures**, Hours	37,662	2,247
MTTE, Hours +	3.23	3.36
Innerent Availability	56.1%	57 .2%

The namulative (33 months) inherent availability has dropped 11.7% owing to a significant increase in MTTR. The 3rd quarter inherent availability has also dropped (12.2%) ending an upward trend which was apparent since the 4th quarter '69. The 3rd quarter 70 MTTR has also increased significantly as has the failure rate and downtime relative to quantity of primary failures. The inherent availability trend by calendar quarters is shown in Figure C-2, page C-10.

From Table B-1

^{**} From Table A-1, excludes corrective actions not classed as primary failures. Total corrective actions cited in Tables B-1 and B-2.

Sikorsky Aircraft -----

Achieved Availability

Achieved Availability (Aa) as defined in MIL-STD-778 differs from Inherent Availability (Ai) in that Ai deals only with equipment operating time, primary failures and the associated failure repair time, whereas, Aa includes operating time, ready time, failure repair and preventive inspection time. Therefore, one explanation of Aa is to define it as a more inclusive version of Ai, with no new factors introduced which are not directly a function of the designed reliability and/or the pre-planned maintenance cycles. Achieved Availability is expressed as:

Aa = MTBM

where:

MTBM = Mean-Time-Between-Maintenance consisting of (for a given calendar interval) the sum of the operating time and operationally ready time divided by the sum of the corrective and preventive maintenance actions performed.

 $\overline{\mathrm{M}}$ * Mean Active Maintenance Downtime consisting of (for a given calendar interval) the sum of the active corrective and preventive maintenance downtime divided by the sum of the corrective and preventive maintenance actions performed (excluding cannibalization actions and associated downtime) and where all supply, support equipment and administrative downtime is considered to be operationally ready time.

thus:

Operating Time + Ready Time
Corrective Actions + Preventive Actions

Aa = -

Operating Time + Corrective Downtime + Preventive Downtime Corrective Actions + Preventive Actions

- Operating Time + Ready Time
 Operating Time + Ready Time + All Maintenance Downtime
- Operating Time + Ready Time
 Total Elapsed Time

Using the above definition for MTBM and \overline{M} and the further derivation for Aa, it is seen that Aa can also be defined as Operational Availability (as defined by the ORE Handbook and MIL-SID-778) with the supply, support equipment and administrative downtime treated as operationally ready time.

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The Achieved Availability shown below for the current quarter and for the total 33 month cumulative data is based on the above definition and data from Tables C-2 through C-17 of Section D.

	3rd Quarter 1970	Cumulative Data 33 Months
Operating Time + Ready Time (hrs)	38.74 7	514,531
Corrective Actions Downtime (hrs)	3,144	69,881
Preventive Actions Downtime (hrs)	2,381	32,789
*Administrative Downtime (hrs)	10,718	169,349
*Supply Downtime (hrs)	13,554	159,461
*Support Equipment Downtime (hrs)	240	815
Total Operationally Ready Time	63,259	844,153
Total Elapsed Time	68,784	946,823
Achieved Availability	91.90%	89.2%

^{*}Treated as Operationally Ready Time

Sikorsky Aircraft ---- - --- U

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Operational Availability (Data Item 08-010-8)

The Operational Availability, as defined in the ORE Handbook, considers flight and ready time and all downtime for maintenance, supply, and administrative reasons. The detailed summations are presented in Tables C-1 through C-17, Section D. The trend by calendar quarter is shown in Table C-1 and graphically in Figures C-1 and C-2, pages C-9 and C-10, respectively.

The tables of Section D present the data for (1) the current calendar quarter and (2) the total cumulative data. The analysis is further subdivided to show comparisons between RVN, CONUS, and USAREUR operations for the above calendar periods.

The data inputs show the following operational availability, along with the change from the previous quarter:

		3rd 0	uarter	1970				All	
		conus	Δ	RVN	Δ	USAREUR	Δ	Locatio	ons Δ
1.	Operational Availability:	53.5%	-13.7%	62.2%	+4.7%	48.7%	-25.3%	56.3%	-6.6%
2.	Not Ready Due to:								
	a. Prev. Maint.b. Corr. Maint.c. Supplyd. Admin.	4.2% 3.5% 29.4% 9.4%	+0.9% +1.0% +11.4% +0.4%		+0.5% -6.6% -6.8% +8.0%	1.2% 1.8% 32.0% 16.3%	05% +0.2% +21.4% +4.2%	3.5% 4.6% 20.0% 15.6%	+0.4% -3.7% +5.5% +4.4%
	Total Not Ready:	46.5%		37.8%		51.3%		43.7%	
		33 Mont	h Cumul	ative					
1.	Operational Availability:	54 .6%	+0.2%	52.1%	+0.6%	66.9%	-2.9%	54.3%	+0.2%
2.	Not Ready Due to:								
	a. Prev. Maint. b. Corr. Maint. c. Supply d. Admin.	3.5% 4.1% 22.0% 15.8%		3.8% 9.8 14.9% 19.4	±0.0% -0.2% -0.3% -0.1%	15.3%	±0.0% -0.1% +2.9% +0.1%	3.5% 7.4% 16.9% 17.9%	±0.0% -0.2% +0.3% -0.3%
	Total Not Ready:	45.4%		47.9%		33.1%		45.7%	
			c. 6						

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The operational availability presentation readily shows excursions from previous quarterly report averages. Examination of the Tables of Section D permits further isolation of gross changes by operating theater to specific activities.

3rd Quarter 1970

CONUS - The decrease (-13.7%) in operational availability is due to increases in maintenance, supply, and administrative downtime.

RVN - Operational availability has increased (+4.7%) as a result of decreases in mai: tenance and supply downtime.

USAREUR - The operational availability has decreased significantly (-25.3%) primarily due to increases in supply downtime (+21.4%) and less significant increases in administrative downtime.

ALL LOCATIONS - The overall operational availability showed a slight decrease (-6.6%) as a result of an increase in supply, preventive maintenance, and administrative downtime.

Cumulative - 33 Months

CONUS - The cumulative operational availability increased (0.2%) as a result of a general decrease in administrative and corrective maintenance downtime.

RVN - An increase (+0.6%) in the cumulative operational availability is the result of a reduction in corrective maintenance, supply, and administrative downtime.

USAREUR - Overall operational availability decreased lightly due to a small increase in supply downtime.

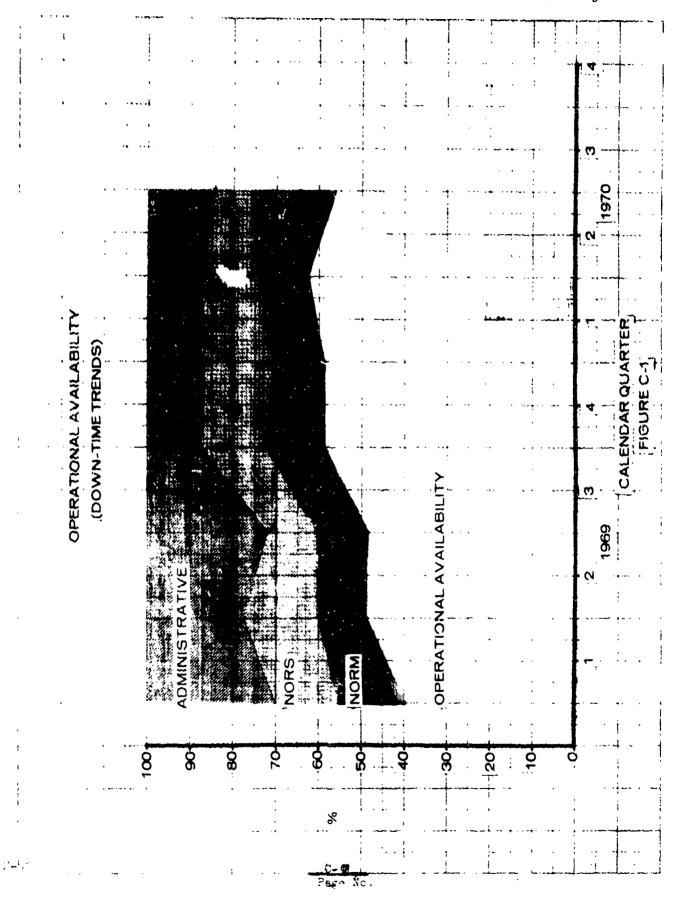
ALL LOCATIONS - The cumulative operational availability increased (+0.2%) as a result of a decrease in administrative, and corrective maintenance downtime.

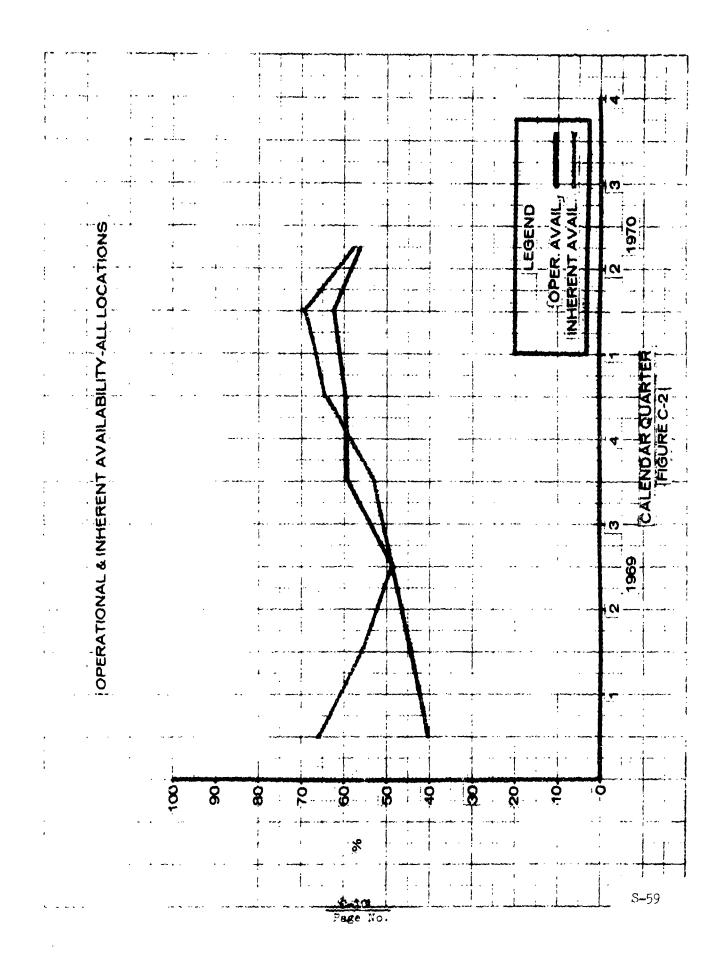
Analysis of sireraft downtime reported for supply shortages of components was performed and the following list cites the top ten contributors to operational unavailability for supply reasons over the 33 month period of this report. Items are ranked in descending order for the combined operational theaters, and show the reduction of overall availability in the specified theater due to shortages of the listed component.

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Sikorsky Aircraft ---- - --- A.

Rank	Component	CONUS	RVN	USAREUR	ALL LOCATIONS
1	Engine Fuel Control P/N 571076 FSN 2915-928-3906	0.7%	0.9%	4.3%	1 . 2%
2	Tail Rotor Head Assy. F/N 65111-07000-047, -045 65110-07000-047 FSN 1615-975-0475	2.6%	0.1%	0.4%	0.9%
3	Clutch Assy. APP P/N S6137-91000-015, -016, -013 FSN 1615-915-7142	2.3%	0.3%	0.0%	0.8%
4	Tail Rotor Blade Assy. P/N 65160-00001-045,-042,-041 FSN 1615-986-6051	0.3%	1.1%	1.3%	0.8%
5	Engine Model T73-P-1 P/N 572200 & 6430-81100-043 FSN 2840-904-2461	0.75	0.7%	0.0%	0.7%
6	Main Rotor Head Assy. P/N 6410-20004-014,-015,-016 -017,-023,-027 FSN 1616-915-7142	0.1%	1.0%	0.0%	0.5%
7	Speed Actuator P/N -0433-86326-101 PSN 2995-891-8461	1.0%	0.0%	0.4%	0.5%
ŧ	Support Assy:, Bearing P/N 6435-60:18-010 SS9003-001 FSN 1615-915-7013	1.5%	o.e%	0.1%	C:.4%
9	Main Rotor Blade Assy. F/N 6415-20201-041 FON 1615-842-6277	0.5%	0.5%	0.0%	0.4%
10	Core, Flex Shaft P/N 572781 FSN 2995-914-5940	0.2%	0.5%	0.0%	0.4%





Sikorsky Aircraft -----

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Average Flight Hours per Aircraft (Data Item 08-010-10)

Analysis of data processed from the Daily Flight Records, SA 978-3, is shown in Tables C-18 through C-26 of Section D. The data is presented for (1) the current calendar quarter, and (2) the total cumulative data.

The analysis is further subdivided in these tables to show each characteristic by USARBUR, RVN and CONUS to compare operational theaters.

The average flight hours accumulated on each aircraft by serial number and location is shown in Table C-18. For all reported aircraft combined, the information is as follows:

	3rd Quarter	33 Months
Average Flight Hours Accrued Per Aircraft	68.2	761.8
Average Flight Hours Accrued - (Standard Deviation)	46.5	469.6

This shows a monthly average flight near per aircraft of 23.1 hours based on the 33 month average.

Sikorsky Aircraft --- - --- A.

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Average Flight Duration (Data Item 08-010-11)

The average flight duration, with standard deviation, is displayed in Table C-18 of Section D for each aircraft and all aircraft combined. The data is presented by (1) the current calendar quarter and (2) the total cumulative data.

Further subdivisions are displayed in Table C-13 to show average flight duration in USAREUR, RVN and CCNUS for comparing operational theaters.

For all reported aircraft combined, the information is as follows:

	3rd Quarter 1970	33 Months
Average Flight Duration	1.81	2.56
Average Flight Duration -	1.17	1.07

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SYS.EM ANALYSIS

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LOCATION - ALL

TABLE

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Sikorsky Aircraft -----

SER-64276 Rev. I J

Table A-3 COMPONENT CONTROL

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Table A-3 (Cont)

TBO or JR Retirement MTBR	19,1970 191970	500 311	1655 1655	50 1200 989
Quantity of Unscheduled Removils MIBUR	19,1	480 94 F.	7 2000000	3000
NOT	1560-052-0467 1560-932-3655 1560-932-3655	1615-960-1543 1615-915-7142 FSN Pending	1080-878-5215 1680-938-3100 1680-936-2408 1030-930-2408	17.15-002-6801
Part Number	\$P7063-3 \$P7063-5 6420-60017-105	\$6137-91000-013 \$6137-91000-015 \$6137-91000-016	6450-62352-104 4SS-3089-0013 6450-62352-103 4SS-3501-001 6450-62352-102 1640-62356-041	6435-66003-040
Nemerclature	Cargo Lashing Reels, Load Leveler	Clutch Assy, APP	Decoupler Device Cargo Hoist	*Gear Box and Servo Assembly

 $^{4}\mathrm{S}/\mathrm{N}$ of gear box is to be used as assembly S/N .

Page No

Table A-3 (Cont)

Nomenclature	Part Number	NCM.	Quantity of Unscheduled Remowals	MTBUR	TBO or Retirement	MTBR
Engine Assembly, Turbo	JFTD12A1 410400 772200 T73-P-1 JFTD12A4A	2840-919-7975 2840-919-7975 2840-904-2461 2840-904-2461 2840-904-2461	0 0 8 1 0	667	800	99 ¹ 1
Gear Box, Cargo Hoist	6435-63001-013 6435-63001-016 6435-63001-016	1680-831-0480 1680-936-2391 1680-781-6655	000	23996		23996
Gear Box, intermediate	6435-66400-042 6435-66400-042 6435-66400-043	1615-901-1914 1615-902-5092 1615-986-6169	°°° 5	1778	1200	873
Gear Box, Main	6435-20400-041 6435-20400-046 6435- 20 400-047	1015-984-5589 1615-984-5605 1615-983-0065	0 0 78	615	800	844

Table A-3 (Cont)

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MTBR			291
TBO or Retirement		•	0 0 1
MTBUR		6	5
Quantity of Unscheduled Removals	0		E10 40 400
FSI	2840-988-0181		1615-895-4509 1615-895-5373 1615-938-1711 1615-717-7667 1615-809-2380 FSN Pending FSN Pending FSN Pending
Fart Number	6430-80007-07		6410-20004-011 6410-20004-013 6410-20004-015 6410-20004-023 6410-20004-023 6410-20004-023 6410-20004-016
Nomenclature	Lug Assy. Eng.	Main Rotor Head Assy	

D-A258 Page No.

DA-259 Page No.

Table A-3 (Cont)

œl			47993	1959	923	672 ' '
MTBR	395		<u>L</u> 1	~	J,	
TBO or Refirement	004					1000
MTBUR	15156		k7993	1959	923	11711
Quantity of Unscheduled Removals	25.	7007	ч	15 50 15 15	0 2 5	17
FSN	1615-983-7321	1015-005-5311 FSN Pending FSN Pending 1615-982-0554	1650-993-5462	FSN Pending	1650-831-0273 1650-831-0273	6615-829-8443
Part Number	170-50292-0179	6410-25200-043 6410-26001-102 6410-26001-103 6410-26000-012	PMF-117B006A	6430-91000-011 6430-91000-012 6430-91000-041 6430-91000-047 6430-91000-042	1PV-093L001-5 6465-20021-101	s6265-62551-10
Nomenclature	Dam per Assy, Main Rotor	Cylinder, Damper	Motor, Hyd., Cargo Hoist	Particle Separator Eng Air Inlet	Pump and Actuator, Cargo Hoist	Servo, AFCS

(Cont)	CONTROL
A-3	ENT
Table	COMPO

MTBR	33996	11998	751	2182
TBO or Retirement			1000	
MTBUR	23996	11998	1655	2182
Quantity of Unscheduled Removals	00 ₀ 0	# 0 0 N #	87	17 5 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1
PSN	1650-934-8448 1680-934-8434 1650-069-3344 1680-857-3285	1650-938-8380 1650-857-3286 1650-934-8447 1650-069-3355 1650-069-3344	1615-975-0355	1560-854-0505 1620-83-1122 1620-898-9587 1620-934-8424 1620-852-6688
Part Number	6465-62100-015 6465-62100-017 6465-62100-017 6465-62100-021	6465-62100-018 6465-62100-022 6465-62100-016 6465-62100-020 6465-62100-019	81565-20431-10	6425-50102-011 6425-50102-014 6425-50102-013 6425-50102-012 6425-50102-015
Nonenclature Servo Cylinder Assv.	Load Leveler, Short	Servo Cylinder Assy, Load Leveler, Long	Servo, Main Rotor Primary	Strut and Fork Assy, Main Ldg Gear

D-A260 Page No. Table A-3 (Cont)

Tart Number
6425-50502-011 6425-50501-011
65110-07000-047 64110-07000-013 65111-07000-045 65111-07000-047
05112-07002-046
64-7155-001 6450-60131-101 32-0351-7
6430-62045-101 2915-897-4078 861245

D-A261 Page No.

UN-24A Total System On-Aircraft Maintenance Downtime per Flight Hour Table b-1 Rev. J. Third Quarter 1970

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	ous	3.5	6.0	5.2 5.8 8.5	0	322.8	Report	No. SER 64
Totai	Locations	47,993.5	25,600.0 13,536 1.9 45,724.3 3.4 1.8	85,410. 26,445 3.2 259,598 3.0 5.41	39,981 39,981 1.9	2.3	7.6 2.8 6.36	ook)
	USAREUR	2226.6	1,114.6 564 2.0 1587.i 2.8 1.4 0.72	1,536.5 1,944 2.3 10,£85.5 2.4 4.80	5651.1 2508 2.0	2.5 12,272.6	4.9 2.2 5.52	ir to ORE Han actions. ort Activitie
33 Month Cumulative	RVN	34,966.2	17,136.3 8,731 2.0 31,725.4 3.6 1.9	63,674.1 17,823 3.6 191,070.2 3.0 5.46	80,810.4 26,554 2.0	2.3 222,795.6	8.4 2.8 6.37	
	CONUS	10,799.8	7,349.1 4,241 1.7 12,411.8 2.9 1.7	17,199.8 6,678 2.6 57,843.2 3.4 5.36	24,548.9 10,919 11.7	2.3 70,254.9	6.4 2.9 6.51	ive arive
A11	Locations	3,001.2	1,678.7 849 2.0 3034.7 3.6 1.8	4,614.0 1,590 2.9 11,210.1 2.4 3.73	6,292.7 2,439 2.6	2.1 14,244.8	5.8 2.3 4.7	corrective maintenary Manhours, for prevent actions at both Org.
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	KVN	1,693.5	860.8 381 2.2 1721.2 4.5 2.0	2,703.2 644 4.2 1,999.1 1.8 2.95	3,564.u 1025 3.5	2.1 6,720.6	6.6 1.9 3.9	d or Manhours, for Time, Elapsed or definition.)
	CONUS	938.4	619.9 359 1.7 1040.5 2.9 1.7	1294.8 674 1.9 1.9 4,24.7 3.3 4.50	sintenance 1914.7 1033 1.9	2.0 5,265.2	w 01 w 14.00	Elapsed or Manh cenance Time, El ok for definitio scheduled (TBO)
		Total Flight Hours	Corrective Maintenance a) Active Elapsed Hours b) Corrective Actions c) MTTR (1) d) Active Manhours e) MTTR (1) f) Avg. Manhours/Down Hours g) Active MAH/FH	Preventive Maintenance (3) a) Active Elapsed Hours b) Preventive Actions c) MPMT (2) d) Active Manhours e) MPMT (2) f) Avg. Manhours/Down Hour g) Active Manhours/Fit. Hour	Combined Corrective/Freventive Maintenance a) Active Elapsed Hours b) Total Maintenance Actions c) Avg. Active Elapsed Hours/ Maintenance Action d) Avg. Active Down Hour/Flight	<pre>Rour e) Active Manhours f) Avg. Manhours/Maintenance</pre>	Action (3) g) Avg. Manhour/Down Hour h) Active Manhours/Flight Hours	Notes: (1) Mean Time to Repair, Elapsed or Manhours, (2) Mean Preventive Maintenance Time, Elapsed (Refer to ORE handbook for definition.) (3) Includes on-aircraft scheduled (TBO) remon
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Fromming for the 3 kmonth cumulative data from all locations combined in the Josephent Corrective Maintenance Cumbary, Table B-3, Pages D-B4 through D-B43.

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Table C-1 Rev J

Operational Availability and Downtime Trends

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ALL LOCATIONS	Ę	뇖	%.		2.68	8.0K	16.2		13.00	\$0.78		\$2.9		3.68	3 5.5	17.06	0. LE	19.0	\$6.0g
777	12	겳	\$9.00		2.8	10.66	16.78 16.28	0.0 0.LS	11.78	11.0		8.3		3.0g	7.58	16.88	9.18	21.38	19.58
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1010	7.	겲	74.08		H.1	1.68	10.6	0.0g	12.15	26.0g		38 .69		1.4	1.98	12.48	\$0.0	14.58	% .0€
USANGUR	191	沟	\$4.05		2.98 1.78	2.08 1.68	16.2% 10.8% 10.6%	0.0 \$0.0	30.3	16.06		\$2.69		1.25 1.35 1.45	1.5% 1.8% 1.9%	24.01 27.01 29.01	0.0% 0.0% 0.0%	15.05	30.08
1		13	84.68 54.08 74.08		 M	1.68	16.2	0.0	16.58 30.38 12.18	35.66		73.48		1.8	1.58	\$9.21	0.0	11.38 15.08 14.58	
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RVE	1	湖	58.3 62.68 57.58 62.38		5.3	16.65 12.45 13.15 6.75	14.45	0.2	8.3	37.15		\$1.67		3.9		15.0% 15.0% 15.0% 14.9%	30.0 \$0.0 \$1.0 \$1.0	23.1% 21.4% 19.5% 19.4%	50.3\$
2001	ş	뉡	\$8.2		2.3	16.65	12.9	\$0.0	10.08	26.88 37.48 42.58 37.88		48.05 49.75 51.55 52.15	c	5	89.6	15	\$1.0	23.1\$	\$2.0\$
ļ	12	긖	\$3.5\$		X	3.58	% 7.6√	0.0	9.48	43.48 32.88 46.58		52.48 54.48 54.68		3.5\$	4.18	\$0.55	0.0	15.8	84.54
1970 1970	Pu	기	\$5.85 \$1.70 \$0.00		3.08 3.38 4.28	6.18 2.58 3.58	22.5\$ 18.0\$	0.1% J.US	11.78 9.08	32.8		54.48		3.48	\$2.4 \$4.4	21.8% 21.4% 22.0%	0.1% 0.0% 0.0%	17.7\$ 16.6\$ 15.8\$	45.6
SI WEST	184	빏	\$0.00		3.08	6.1\$	22.5\$	0.1\$	11.78	43.48		\$2.4		3.68 3.48	¥1.4	₹8.1%	0.1\$	17.78	89.17
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	- And the Awardability -	design (Fig. 1)		C. Wittige due to:	A. ireventive Maintenance	8. Corrective Maintenance	C. Supply - NORS	P. Cupport Equipment - NORS	E. Administrative	S. Total Will Ready	Speration Availability Cumulative Summation by Quarters	. Operational Availability	Downtime due to:	A. Preventive Maintenance	B. Corrective Maintenance	C. Capply - NORS	E. Support Equipment - NORS	E. Administrative	s. Total Not Ready

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Sikoreky Aircraft -----

Table C-18 Rev. I CH-54A Utilization Characteristics

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TITLE EIGHTH (8th) QUARTERLY CH-53 READINESS REPORT

REPORT NUMBER

PS 65-K-8

PREPARED UNDER

N000 19-68-C-0471 MOD P00102

REPORT DATE

31 DECEMBER 1971

MEPORT PERIOD

APRIL 1971 - JUNE 1971

This report is applicable to the following strongly medals) and contract(a): MODEL CONTRACY

Present by Cas	Canner	B. Protoring	1 1 1. 1. 1.	
C. A.	Canner/B.	Bickering Bickering	J. S. White	

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REPORT NO. PS 65-K-8

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ABSTRACT

A total of thirty (38) assemblies have been presented and discussed in the CH-53 Readiness Program over the preceeding 2 year period. In this the eighth (8th) and last report under the terms of the current contract, we will summarize some of the major items which include:

- 1. Continue mini-course and audi-scan training programs to help insure that maintenance personnel can attain a high degree of proficiency in the support of the various systems encompassed in the CH-53 helicopter.
- 2. Review possibility of improving structural integrity of lower personnel door.
- 3. Approve VECP 7383 to expedite availability of long spline drive shaft for the utility system hydraulic pump.
- 4. Approve Sikorsky Letter SE 5064 requesting ECP coverage to authorize carburizing internal areas of nose gear box gears.
- 5. Continue evaluation of PPG all glass and Goodyear composite windshield panels.
- 6. Expedite concurrence with ECP 1HS-T62-029 to introduce improved APU pressure switches into the supply system.
- 7. Modify in service clutch assemblies per ECP 7418.

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Introduction

This report represents the eighth and last submittal under Sikorsky Aircraft's CH-53 Readiness Program. These quarterly reports authorized by MOD P00102 to Contract N00019-68-C-0471, have been prepared and distributed by the Readiness Group within the Product Support Department under direction of the CH-53 Model Manager,

The major statistical input of this group was 3M data supplied by the Maintenance Support Office (MSO) through NATSF. Both manual and machine processing was used in reducing the data for analysis. 3M data was used to determine high cost items on the CH-53 in terms of manhour expenditures and component repairs/replacements. NORS and NORM data was analyzed and top problem items in NORS, NORM and 3M reported component failure areas identified. Once these top problem areas were identified, further analysis was conducted to determine the exact nature of the problem. Data inputs from a Sikorsky Readiness Representative. stationed at NARF, North Island, supplemented 3M data with information concerning depot level maintenance. This supplemental data was sifted and analyzed in order to pinpoint possible problem areas. Once identified. these problems were attacked from a number of directions. Areas were investigated with a view toward possible recommendations for:

(a) changes or revisions to MIMS and other handbooks, (b) development of Audi-Scan programs to assist in improving field maintenance techniques. (c) initiation of SICR action to change procurement levels for parts/components showing usage differing from programmed levels. (d) changes to priority listings for kit deliveries. (e) ECP action to improve current designs in order to increase readiness rates. Both short and long term solutions were investigated with the intent of providing the most effective and expedient solution possible.

Close coordination was maintained between the Readiness Group and other areas of Sikorsky Aircraft. Programs. Engineering. O&R.and areas of Product Support including Supply Support. Field Support and Technical Publications were kept abreast of the group's efforts to insure coordinated and meaningful action on the part of Sikorsky Aircraft to improve operational readiness of the CH-53 helicopter.



Report Format:

There are three basic sections within this report: abort rate data. maintenance manhour data, and NOR hour data are included in the first section. This information, gathered from the 3M system, is presented in a graphic format.

The second section contains: (a) impact analysis information on selected components. Impact Analysis being a study of the logistics connected with certain time control components. Adequacy of spare parts provisioning is studied taking into account various parameters such as Time Between Overhaul (TBO), Aircraft Utilization Rates. Actual Mean Time Between Removals for Overhaul (MTBR for Overhaul). Depot Turn Around Time (TAT), aircraft and parts deliveries, etc. The output of the study is a comparison of projected parts/component requirements versus projected parts availability. Obviously, any major difference between the two outcomes would be cause for remedial action. (b) is devoted to problems analysis of areas affecting the Operational Ready Rates for the CH-53A/D aircraft. The format consists of an investigation summary and a number of action sheets stating particular problems, their effect on readiness, maintenance manhours, etc. and recommended action to alleviate these problems. Where an ECP is referenced, a flow chart is

included to reflect its status. 3M data is used as an information source and an analytical study of this data indicates those areas where further research is required. The data is ranked by systems as contributors to NORS, NORM and component failure burdens for the aircraft. The major problems are further studied in order to determine what actions can be taken to improve the system or component. This analysis forms the basis of the action sheets presented.

The third section reflects the status of suggested actions to improve readiness of areas discussed in carlier reports. These are presented in narrative form and include charts or graphs where their use adds clarity to the presentation.

Details and background information, including the ranking determined from 3M data, are presented in the appendices. In this way the cursory reader is spared the maze of numbers and charts while the information is made available for those who want, or have, to be aware of those details.

Current Report

NOR and failure data for this report have an identical time frame: lanuary 1971 through June 1971. The Abort Summary covers April 1971 through June 1971.



The Airframe, Rotor System, Landing Gear System, Transmission System, Flight Control System and Power Plant Support System occupy the first (6) positions in the system performance chart, and are responsible for 58, 12% of all aircraft failures, based on MSO 4790, A2142-01 of 20 August 1971. All have been discussed in earlier reports.

Thirty-eight (38) assemblies responsible for significant contributions to CH-53 failure and NOR statistics have been discussed during the past two years in the readiness reports. In this the eighth (8th) and last report under the terms of the current contract, we will summarize some of the major points presented in lieu of introducing additional problem items.

- 1. Perhaps the greatest single item affecting aircraft readiness is the quality of maintenance available at the field level. This of course relates directly to the need for dynamic training programs. The personnel attrition rate imposes considerable strain on any squadron's qualified roster but sophisticated systems such as those encompassed in the CH-53 cannot be maintained in the same manner as those aircraft designed and fabricated a decade or two ago. This was evidenced when 3M data was analyzed for the many assemblies we have discussed, such as:
 - a. The high cannibalization rate of AFCS components.



- The frequent entry in the action taken block "No Defect -Checked OK. "
- Mission aborts due to tires with "Bad or Worn Tread", "Skin Cracks" in the ramp. These should be detected and corrected during scheduled aircraft maintenance periods and not left for the flight crew to locate.

The training recommended by the contractor includes Audi-Scan and Mini-Courses on selected trouble spots and OJT on all phases of maintenance tailored to the CH-53 helicopters.

- 2. The process from "Need for an Improvement to Incorporation of that Improvement" is too costly timewise. Analysis conducted during preparation of these reports emphasized the need for more expedient methods for completing ECP actions. (i. e.)
 - a. Sikorsky Letter of Intent SEL 5154 was forwarded to NASC in October 1970. The contractor is not in receipt of either confirmation or rejection correspondence. Letter SEL 7733 is similarly in process having been forwarded to NASC in January 1971.
 - Sikorsky Letter SE 593 dated 12 February 1968 started the ball rolling to modify engine nacelle aft panels which were becoming charred due to exhaust impingement

encountered under certain operational conditions. It was not until November 1970 that improved panels were installed on production aircraft. Kits for retrofit of in-service aircraft are scheduled for availability in February 1972.

It became apparent, shortly after deployment of the C. CH-53, in 1967, that the matri-switches in the AFCS control panel would not function in the sandy environment of SEA. An ECP was submitted to NASC in June 1971 which recommended installing protective boots to preclude dust contamination of these assemblies.

These few incidents have been mentioned only to point out the length of time required to complete ECP projects and amplify the need for an accelerated procedure to implement beneficial modifications to an aircraft system.

3. The abort rate for the CH-53 has displayed gradual improvement over the 3 years (84, 317 flight hours) reviewed under this contract as noted in the abort graph in section one (1) of this report. The new or short plot of lines shows that aborts, when analyzed and adjusted to exclude erroneous entries from the 3M base data. have reached the Sikorsky predicted MTBA of 50 flight hours. (, 020 Aborts /Hr)

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The balance of the report is devoted to problems reviewed previously to highlight areas where additional effort might further improve aircraft readiness.

Fleet wide operationally/ready rate statistics have been omitted from this report in order to maintain its unclassified status. Readiness information is available from other sources and unless a strong need for this type of information becomes evident, it will not be included in this or future reports.

DEFINITIONS

Mean Time Between Removal for Depot Overhaul/Repair (MTBR)

The Mean Time Since New or Overhaul of components being returned to a depor level facility for any reason. Components returned without TSO information are disregarded. NOTE: The number so generated cannot be used as a true reliability figure for the component because it will include returns for such items as maintenance or handling damage, etc.

3M Reported Failure

Maintenance Actions reported in 3M card codes 11, 21, and 31 having Action Taken Codes 1 through 9, B, C, or Z.

Depot Turn Around Time (TAT)

Time elapsed from receipt of component at depot facility until component returned to RFI status.

"Timely Tips"

A Sikorsky developed and prepared directive designed to keep our Field Support Representatives abreast of new maintenance techniques, etc.

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"Sound Off"

An internal document used to provide comments from our representatives in the field to up date and improve Sikorsky publications.

Abreviations and Definitions

AFC	Airframe Change
ASO	Aviation Supply Office
BUNO	Bureau Number
ECP	Engineering Change Proposal
IGB	Intermediate Gear Box
IMA	Intermediate Maintenance Activity
LES	Local Engineering Specification
MAG	Marine Air Group
MEA	Maintenance Engineered Analysis (MEAR)
MGB	Main Gear Box
MR	Main Rotor
MTPR	Mean Time Between Removal for Depot Overhaul/Repair
NARF	Naval Air Rework Facility
NATSF	Naval Air Technical Services Facility
NASC	Naval Air Systems Command

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NOR Not Operationally Ready

NORIS North Island, California

Not Operationally Ready -NORM

Maintenance

Not Operationally Ready - Supply **NORS**

Overhaul and Repair O & R

OJT On Job Training

PMRC Periodic Maintenance Requirement

Cards

Ready for Issue RFI

South East Asia SEA

Supply Item Change Record SICR

Sikorsky Standard SS

Turn Around Time TAT

Time Between Overhauls TBO

Tail Gear Box TGB

Tail Rotor TR

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SECTION 1

ABORTS - NOR - MAINTENANCE MANHOURS

This section of the Readiness Feport presents Abort, Not Operationally Ready, (NOR) and Maintenance Manhour (MMH) data in a readily understandable graphical form. The data is grouped by two (2) digit work unit codes (WUC), i.e.: aircraft sub-system -- airframe, flight controls, drives and transmissions, etc. -- and is presented in WUC order. Aborts, NOR and MMH charged to each work unit code are shown as a percentage of total in their particular category. The abort period covered by this report is April, May, and June 1971, the information having been retrieved from 3M data tapes received by Sikorsky. The graph presented in this section reflects aborts per hour (experience versus predicted) for the CH-53A and D. The abort rate line is computed using as a starting point September 1969 and 84-837, 4 total flight hours.

During the period October 1969 - December 1969 the abort rate was , 03904 per 9,784.0 flight hours (total flight hours 94,621.4) or one (1) abort every 25,613 flight hours.

During the period January 1970 - March 1970 the abort rate was . 03353 per 8, 766, 8 flight hours (total flight hours 103, 388, 2) or one (1) abort every 29, 819 flight hours.



During the period April 1970 - June 1970 the abort rate was . 03021 per 13, 370, 5 flight hours (total flight hours 116, 758, 7) or one (1) abort every 33, 095 flight hours.

During the period July 1970 through September 1970 the abort rate was . 04100 per 9, 999, 5 flight hours (total flight hours 126, 758, 2) or one (1) abort every 24, 389 flight hours.

The abort rate during the period October 1970 through December 1970 was , 03744 per 9, 132, 5 flight hours (total flight hours 135, 891, 0) or one abort every 26, 704 flight hours.

The abort rate during the period January 1971 through March 1971 was . 03286 per 10, 133, 6 flight hours. (Total flight hours 146, 024, 6) or one abort every 30, 431 flight hours.

The abort rate during the period April 1971 through June 1971 was . 04485 for 9386.7 flight hours. (Total flight hours 155.411.3) or one abort every 22.297 flight hours; which represents an increase in the abort rate for this report period.

A detailed analysis of the data base covering both flight and ground aborts revealed that 44.89% of the recorded abort actions were the direct result of poor maintenance techniques. lack of aircraft familiarization, or inequities in the 3M reporting system. The last chart in this section

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of the report includes additional "Plots" which reflect the "Adjusted" abort rate.

Attention is directed to this curve, covering four (4) quarters. July 1970 through June 1971. While the "Recorded" abort actions continue in an erratic course the "Adjusted" curve reflects a steady decline. This clearly highlights the need for a continuing vigorous training program to keep all field level personnel knowledgeable and highly efficient so that the need for maintenance can be detected and accomplished during scheduled maintenance periods and not left to be identified by flight crews which invariably results in aborted missions.

NOR data was extracted from 3M tapes covering October 1970 through March 1971. The maintenance manhour data base is a 3M report generated by MSO and also covers CH-53 operations from January 1971 through June 1971. Reference MSO-4790, A2142-1 655-02 of 20 August. 1971.

In this report maintenance manhours for the CH-53A and CH-53D aircraft are grouped together since the relative rankings by WUC are nearly identical. See the Chart of Appendix C. Independent rankings will be made for each following report and if any significant differences occur they will be highlighted.

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This section provides an accurate indication of which areas of the CH-53 are consuming manhours and reducing availability through aborts and NOR conditions.

15

PAGE

ABORTS, MAINTENANCE MANHOURS, AND NOR BY SYSTEM

				LEGEND	ABORTS	MMH					
	i									18	
										14 16	(ABORTS (MMH (NOR
			1	,						12	OTAL
	***************************************	;				1			•	01 8	PERCENT OF TOTAL
		•				i				ø	PERCE
										7	
 I		II.		E	11;					0	
NOMENCLATURE	Airframe	Fuselage Comp.	Landing Gear	Flight Controls	Rotor System	Engines	APP (Airborne)	Drives/Trans.	Power Plant Su pt.		
WUC	11000	12000	13000	14000	15000	22000	24()(0)	2(4)(X)	24000	S-9	95

(ABORTS (NOR) (NOR)

PERCENT OF TOTAL

٧,

ABORTS, MAINTENANCE MANIFOURS, AND NOR BY SYSTEM

NOMENCLATURE

WLIC

C-34

Hydraulic System Fuel System	Lighting System	(·	Elect. System
		Lighting System Hydraulic System	Elect. System Lighting System Hydraulic System

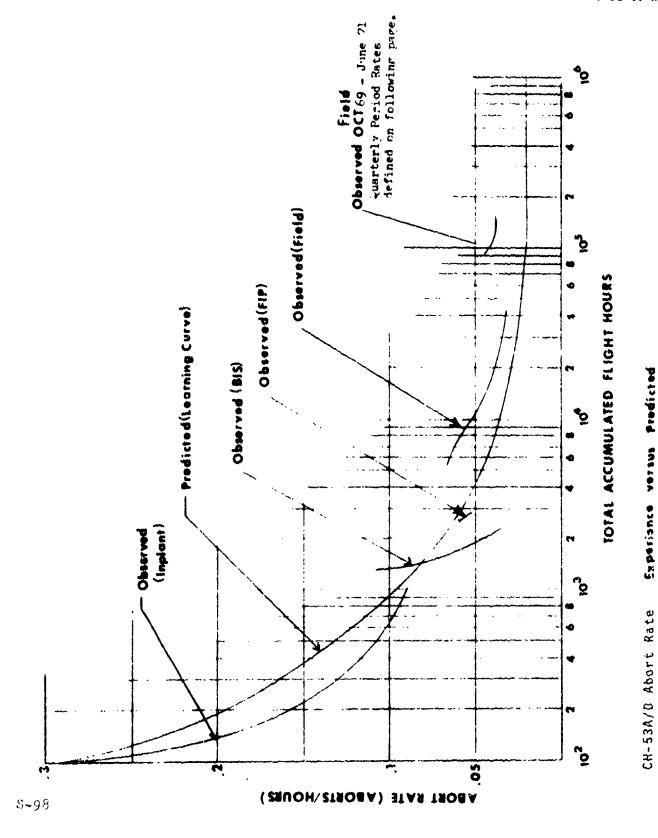
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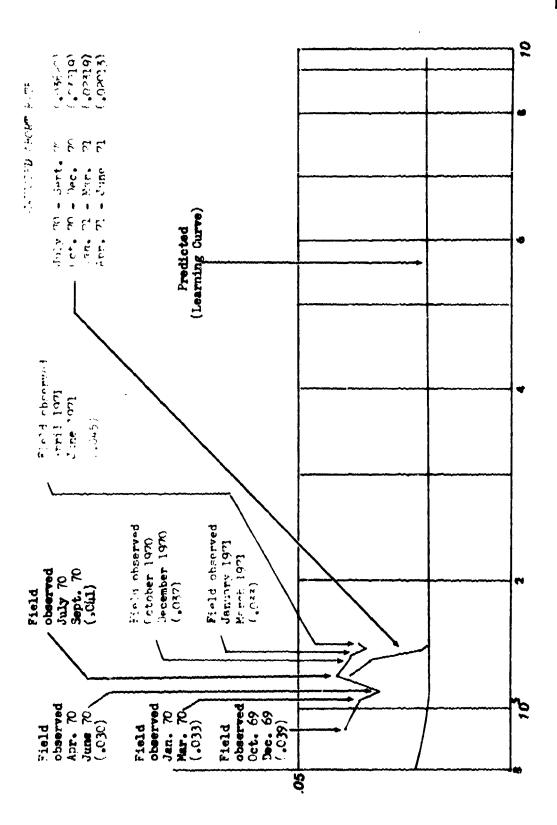
while of each

ABORTS MMH NOR LEGEND (ABORTS (MMH (NOR * PERCENT OF TOTAL 70 Ø Ø N UNF Communications VHF Communications HF Communications NOMENCLATURE Emergency Equip. Integ. Comm/Nav. IFF System Inter Phone Radar Nav. Radio Nav. S-97 67000 71000 720KKI 01000 65000 00049 00019 62000 63000 ₩UC:: 18

ABORTS, MAINTENANCE MANHOURS, AND NOR BY SYSTEM



19



8

X

ABORT RATE (Aborta/Hours)

S-99

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SECTION II

IMPACT ANALYSIS - INVESTIGATION SUMMARY

The Impact Analysis section of the report studies the logistic considerations of time control components of the CH-53. The concept is not complex but the outcome is significant.

Impact analysis starts with an estimate of fleet requirements for time control components for a specified period. The object is to determine the number of new or overhauled spare components that will be required to support 100% utilization in the fleet. There are several parameters that must be taken into consideration. These include such items as: number of aircraft, new aircraft deliveries, monthly flight hour standards, depot outputs, etc. The other major parameter is defined as Mean Time Between Removal (MTBR) for Overhaul and is the Time Since Overhaul (TSO), for components returning to a depot for any reason. This number is not a reliability figure for the component because it will include returns for such items as handling or maintenance damage, etc. What is determined is the length of time that an average component is available at the user level. Components which are removed for local repair are not considered since they remain at or near the usage site and are expected to be available on a short turn around time.

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Fleet requirements can be estimated by dividing the flight hour estimate by the MTBR for Overhaul/Repair. This number of components must then be supplied from the output of Depot facilities and from new spare deliveries. Any difference between requirements and projected deliveries is cause for further analysis and remedial action.

A description of the derivation of the actual numbers, flight hours, and MTBR for overhaul, is contained in Appendix B.

The component investigation portion presents a comprehensive analysis of systems, sub-systems, or components which are adversely affecting aircraft readiness.

3M data forms the base for this section of the report. Two different 3M reports are used to generate the data. A special read-out of the 3M tape supplied to Sikorsky Aircraft provides NOR data. Report number MSO-4790. A2142-01 655-02. "Reliability and Maintainability Summary" provides failure, maintenance action, and manhour data. The data is ranked by contributions to NORS, NORM and component failures and then cross-indexed to show interrelationships between the three catagories. Top problem areas are then chosen for analysis. See Appendix C.

Analysis starts with a search for specific reasons or causes which account for the high ranking of the component. Sikorsky Field Support

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Representatives reports and reports from the Sikorsky Readiness Representative at NARF, North Island provide much of this information.

Once specific causes are isolated, a search begins for possible solutions. Solutions are analyzed with the assistance of Product Support and Supply Support and recommendations are formulated.

The text of this section describes the problem areas and presents the recommendations. Following the text are Action Sheets which summarize individual problems and the required action to alleviate that specific problem. Flow Charts are included to reflect the actual status of referenced ECP's highlighting required action and established responsibility. However, since no new items are being introduced in this, the eighth (8th) report, no impact analysis or investigation summary will be presented.

APPENDIX A

ABORT/MANHOUR DATA

	mouse that 1771 innocon June 1971	MANHOURS January 1971	January 197		THROUGH June 1971	MSO 4790-A2142-01	-0 <u>.</u>
WUC	SYSTEM NOMENCLATURE	NO. ABORTS	% TOTAL ABORTS	RANK	53 A/D MANHOURS	% MANHOURS	KANK
11000	Airframe	23	5, 46	9	11.840	16.66	-
12000	Fuselage Compartments	7	1.66	17	1.464	2.06	14
13000	Landing Gear System	23	5.46	r ~	5.379	7.57	ស
14000	Flight Controls	89	16, 15	-	6, 533	9, 19	ణ
15000	Rotor System	46	11. 93	က	10, 511	14. 79	7
22000	Engines	35	8.31	4	4, 526	6.37	9
24000	APP	20	4.75	œ	1.661	2.34	12
26000	Drives/Transmission	09	14. 25	2	5, 627	7.92	4
29000	Power Plant Support System	28	6. 65	ιĊ	3.063	4.31	o
41000	Engine Anti-Ice Comp.	0	0	23	430	.61	24
42000	Electrical System	15	3,56	01	810	1.14	17
44000	Lighting System	æ	1.90	74	1, 202	1.69	15 3
S-10	Hydraulic Power Supply	13	3.09	12	926	1.37	65-K-6
)3							5

WUC	SYSTEM NOMENCLATURE	NO. ABORTS	% TOTAL ABORTS	RANK	53 A/D MANHOURS	% MANHOURS	RANK
46000	Fuel System	œ	1.90	15	737	1.04	19
49000	Miscellaneous Utilities	∞	1.90	91	609	98.	21
51000	Genera! Instruments	12	2.85	13	1,711	2.4}	11
26000	Flight Reference	۵	0	24	806	1.13	38
57000	Integrated Guidance	19	4.51	6	3, 386	4.76	œ
00019	IIF Communications	4	. 95	81	2, 258	3, 18	10
62000	VHF Communications	4	. 95	61	253	.36	25
90069	UHF Communications	14	3, 33	11	1,614	2.27	13
64000	Inter Phone System	4	. 95	20	611	98.	22
92000	IFF System	0	0	25	503	17.	23
71000	Radio Navigation		. 24	21	3, 849	5. 42	1~
72000	Radar Navigation	0	C	26	623	88.	20
91000	Emergency Equipment	-	. 24	22	25	6.	PS 692
TOTAL		421	100, 99		71,043	th '66	

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APPENDIX B

IMPACT ANALYSIS DATA

1. Derivation of MTBR for Overhaul

A survey of all components processed through the depot facilities since the beginning of the CH-53 program is constantly being conducted. Inputs are being received from Sikorsky Readiness Representatives at NARF, North Island and from the Sikorsky O&R Production Control Department. Components received at a depot without Time Since Overhaul information are disregarded unless the time can be otherwise ascertained.

It should be noted that the numbers so generated do not reflect component reliability, since all causes for return to a depot facility are considered, including no-defect components, handling or maintenance damaged components, etc., are included in the survey. The intent here is not to define a reliability number for the component but to accurately study the loss of RFI components from the fleet supply system for any reason.

Computation is affected on the date noted on the chart. This data is used as an additional tool to assist in isolating areas for analysis and is considered when selecting assemblies to discuss in the Readiness Report.

MAJOR COMPONENT MEAN TIME BETWEEN REMOVAL HOURS (MTBR)
Statistical Data Accrued from 1967 Through the Period Noted

COMPONENT	JULY 1970	MARCH 1971	JUNE 1971	SEPTEMBER 1971	DECEMBER 1971
Main Gear Box	416. 22	502, 36	490, 69	492.36	499, 26
Intermediate Gear Box	728. 43	673.88	732. 98	729, 98	752.98
Tail Gear Box	499, 62	602.17	578.07	606, 90	619. 92
Accessory Gear Box	518, 16	550, 79	558.81	579, 38	573.66
Nose Gear Box	490,00	529, 11	540. 40	536, 26	537.37
Main Rotor Head	329, 13	382, 20	383, 98	383, 40	383, 30
Swashplate	416.13	499, 46	472.73	476, 15	477.37
Main Rotor Damper	243.11	285, 25	280, 95	294, 64	295. 20
Sleeve and Spindle	390, 75	403, 43	374, 87	285, 92	315, 63
Tail Rotor Head	465, 36	509, 00	484, 86	483, 30	464.06
Tail Rotor Servo	549, 94	540, 20	531. 47	584, 09	Not Reported
Primary Servo	325, 22	377.21	399, 88	417. 40	Not Reported

COMPONENT	JULY 1970	MARCH 1971	JUNE 1971	SEPTEMBER 1971	DECEMBER 1971
AFCS Servo	344. 52	399, 96	418.18	495.84	Not Reported
Main Rotor Blades	418.40	453, 33	442.96	490.85	482, 52
Tail Rotor Blades	372.00	326, 99	375.05	383, 25	383, 89

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2. Derivation of Predicted Flight Hours

As of 30 November 1971, 232 aircraft were in inventory (strike aircraft having been eliminated). It is assumed that approximately 5 aircraft will be added to inventory during the balance of calendar year 1971. Based on past history, 2 additional strikes are assumed for 1971. A Utilization Standard of 30, 00 flight hours per month per aircraft has been used.

Predicted flight hours per month are obtained by multiplying the average number of aircraft in the fleet for each month by the utilization standard. A summation of monthly totals leads to a gross estimate of 54, 360 flight hours for the year with allowances for anticipated NARF PAR induction schedules and known storage periods considered. It should be noted that the flight hour estimate assumes 100% utilization.

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APPENDIX C NORM, NORS AND FAILURE ANALYSIS

Reference:

:

- (a) Reliability and Maintainability Summary - MSO-4790,

 A2142-01 dated 20 August 1971. The failure statistics reflected are based on maintenance and flight data for the period from January 1971 through June 1971. This summary was selected for the generation of data for the eighth CH-53

 Readiness Report and provides the latest complete accumulated information available.
- (b) High NORM/NORS Data Base - read out of 3M tape supplied to Sikorsky Aircraft reflecting data on all fifth level WUC's. This summary also covers the period from January 1971 through June 1971.
- 1. NORM, NORS Items Ranking
 - (a) Identification and ranking of sub-system WUC's is based on the contribution of the WUC item, measured in hours, to the total reported NORM hours. The percentage of contri-

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bution the item makes to the total NORM hours is also given.

(b) WUC ranking for NORS items is developed in the same manner as for the NORM items.

UNSCHEDULED NORM ITEM RANKING

	WUC	NOMENCLATURE	NORM HRS.	% OF NORM	RANK
	15110	Rotary Wing Head	3, 256, 3	14.17	-
	14410	Forward Cabin Flight Control Components	1, 293, 1	5.58	7
	22600	T-64 Engine	1, 101. 5	4.79	හ
	14A10	R/W Pylon Hydraulic Components	966. 7	4.21	44
	57560	Automatic Flight Control System	873.8	3, 80	κ
	15310	Rotary Wing Blades	776.1	3, 38	9
	26270	Main Gear Box	606. 6	2.64	7
	22660	Main Fuel System (T64)	585.1	2.55	ယ
	26830	APP Clutch Components	478.3	2.08	6
	71430	AN/ARN 52 Tacan Set	454.9	1.98	10
	13110	MLG Mechanical Components	398.0	1.73	11
	45110	Utility Hydraulic System Components	385, 9	1, 68	12
	15220	Blade Positioning Components	381.7	1.66	13
S -1	51130	Engine/Gear Box Instruments	378.2	1.65	14
.11	26720	Nose Ccar Box Components	341.8	1.40	15

ö

NORS ITEM RANKING

WUC	NOMENCLATURE	NORS HRS	SGON BO F	
15110	Rotary Wing Head	9, 453, 4	7.21	KA.WK
71430	AN, ARN52(V) Tacan Set	6, 471-6	;; ;; ;;	- (
15220	Blade Positioning Components	SC 1/4		7 .
12710	Cargo Hook System Components	5.306.6	47	~ ;
14410	Forward Cabin Flight Control Components	5. 234. 4) v	प ।
12610	Cargo Winch Components	4, 410, 2	3.45	n (
44110	Exterior Lights	4.096.9	† <u>†</u>	ا ۵
612EO	AN/ARC 131 VHF/FM Radio Set	3, 976, 4	3, 5, 1,	`
26830	APP Clutch Components	3, 786, 6	, , , , , , , , , , , , , , , , , , ,	x o (
14A10	R, W Pylon Hydrauiic Components	3.763.0	2.93	- - 5
29510	Engine Ignition, Starting Components	3.517.9	2. 2.	2 :
15100	Rotary Wing Head	3, 340, 9	1 0	Ι :
22660	Main Fuel System (T-64)	3. 283. 1	2.54	
51130	Engine Gear Box Instruments	3, 282, 0	2, 5, 4,	Ç
49510	APP Heater Fire Extinguisher Components	3.052.7	2.36	

0-112

286, 268, 4	•	TOTAL NOR HOURS
112, 151, 7	1	TOTAL AWAITING MAINTENANCE HOURS
129, 302, 6	1	TOTAL NORS HOURS
22, 987. 1	,	TOTAL UNSCHEDULED NORM HOURS
21.835.1	•	TOTAL SCHEDULED NORM HOURS

Reference 3M Tabulation NOR Summary - January 1971 - June 1971

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2. Failure Ranking

(a) Twenty-seven (27) system work unit codes are ranked by the number of failures the specific WUC contributed to the overall number of failures reported. The percentage each system contributed is also shown.

SYSTEM PERFORMANCE BY WORK LINIT CODE AND RANKING

::

RANK	WUC	NOMENCLATURE	PREVIOUS REPORT	TOTAL FAILURES	₽5	TOTAL MAINT, ACT.	9	TOTAL	Ð
	11000	Airframe	~	1. 975	17.43	2, 337	13.05	11.840	99 91
2	15000	Rotor System	2	1,219	10.76	1, 942	10.85	10, 511	14. 79
8	13000	Landing Gear System	9	1.020	9.00	1, 407	7.86	5, 379	7.57
₩.	26000	Transmission	4	881	7.78	1.344	7.51	5, 627	7, 92
ıc	14000	Flight Controls	ĸ	844	7.45	1.370	7.65	6, 533	9.19
9	29000	Power Plant Support	9	646	5.70	938	5.24	3,063	4, 31
SU	SUB-TOTAL	-1		6, 585	58. 12	9, 338	52.16	42, 953	60.44
7	71000	Radio-Navigation	10	489	4.32	954	5, 33	3,849	5. 42
æ	51000	Instruments	7	487	4.30	832	4.65	1,711	2. 41
ن	22000	Turbo Shaft Engine	œ	468	4, 13	734	4.10	4, 526	6.37
01	57000	Integrated Guidance	6	434	3, 83	835	4.66	3,386	4.76
	44000	Lighting System		389	3, 43	260	3, 13	1.202	1.69
12	12000	Fuselage Compartment	12	375	3.31	582	3, 25	1.464	2.06
S-115	Total of	Sub-Total of those work unit codes accounting for a least (5) percent of all system failures.	counting for a	least (5) perce	ent of all	system failures	å		PS-K-8

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SYSTEM PERFORMANCE BY WORK UNIT CODE AND RANKING (continued)

RANK	WUC	WUC NOMENCLATURE	PREVIOUS REPORT	TOTAL FAILURES	<i>6</i> %	TOTAL MAINT. ACT.	8%	TOTAL MANHOURS	96
13	91000	HF Communications	15	319	2.81	636	3,55	2, 258	3, 18
14	24000	APP (Airborne)	13	311	2,74	614	3, 43	1,661	2.34
15	45000	Hydraulic Power	14	239	2.10	371	2.07	926	1.37
91	63000	(HF Communications	91	226	1, 99	498	2.78	1,614	2.27
17	42000	Electrical System	17	182	1.60	315	1.76	810	1.14
82	26000	Flight Reference	20	153	1,35	307	1.71	806	1.13
19	49000	Misc. Utilities	61	140	1,24	286	1.60	609	98.
20	64000	Interphone System	88	125	1.10	279	1.56	611	.86
21	46000	Fuel System	21	115	1.01	217	1.21	737	1.04
22	92000	IFF Systems	23	83	. 73	183	1.02	203	.71
23	72000	Radar Navigation	24	7.7	89.	127	.71	623	. 88
24	62000	VHF Communications	22	51	. 45	86	. 48	253	. 36

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SYSTEM PERFORMANCE BY WORK UNIT CODE AND RANKING (continued)

	8		ö. 7	39.30	60.44	69. 94				
TOTAL	MANHOURS	430	ξ. Σ	28, 054	42, 953	71,007				
	86	44	<u> </u>	47.62	52.16	99.78				
TOTAL	MAINT. ACT.	42	33	8.528	9, 338	17,866				
	88	. 44	. 12	41.68	58. 12	99.80				
TOTAL	FAILURES	S	14	4,727	6, 585	11, 312	13, 621	11, 331	17, 905	073
PREVIOUS REPORT	THOUSE I	25	26				13,	11,	:	71, 073
WUC NOMENCLATURE		Surface (ce Contro)	Emergency Equipment		•		TOTAL FLIGHT HOURS	TOTAL FAILURES	TOTAL MAINTENANCE ACTIONS	TOTAL MANHOURS
WUC	41000	307	00016				TOTAL 1	TOTAL 1	FOTAL A	rotal n
RANK	25		97				•	-	•	ι

Sikorsky Aircraft ----- A.

NEPORT NO. PS 65-K-8

- 3. High NORM, NORS and Component Failure Ranking
 - (a) The preceding NORM, NORS and Component Failure Charts have been combined here to facilitate comparison. The high fourteen (14) WUC's for each category were selected.

 (Ref. Chart One).
 - (b) The second chart shows the interrelationship of the WUC's referenced on their respective NORM, NORS and Component Failure Rankings. The 42 codes were consolidated into 15 parent system WUC's for this presentation.

HIGH NORM, NORS, AND SYSTEM FAILURE RANKING

		tenor 'moo	Own, word, and statem FAILC'RE KANKING	KANKINC	
	NORM		NORS	SYST	SYSTEM FAILURES
N.L.C	NOMENCLATURE	WLIC	NOMENCLATURE	WL'C	NOMENCLATURE
1 =000	Rotor System	15000	Rotor System	11000	Airframe
14000	Flight Controls	14000	Flight Controls	15000	Rotor System
26000	R/W Drives/Trans.	12000	Fuselage Compartment	13000	Landing Gear System
22000	Turbo Shaft Engines	26000	R.W Drives /Trans.	26000	R/W Drives/Trans.
11000	Airframe	71000	Radio Navigation	14000	Flight Controls
24000	APP (Airborne)	61000	HF Comm. System	29000	Power Plant Inst'l.
13000	Landing Gear System	11000	Airframe	71000	Radio Navigation
57000	Integrated Guidance	22000	Turbo Shaft Engines	51000	Instruments
2 × 000	Power Plant Inst'l.	24000	APP (Airborne)	22000	Turbo Shaft Engines
51000	Instruments	29000	Power Plant Inst'l.	57000	Integrated Guidance
71000	Radio Navigation	44000	Lighting Systems	44(XX)	Lighting System
42000	Electrical System	49000	Misc, Utilities	12000	Fuselage Compartment
46000	Fuel System	13000	Landing Gear System	61000	HF Comm. System
00 S~119 54	Hydraulic Power Supply	42000	Electrical System	24000	APP (Airborne)

FAILURES
SYSTEM
NORS,
NORM,
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INTERRELATIONSHIP OF NORM, N

S-120

		•		
WUC	NOMENCLATURE	NORM	NORS	SYSTEM FAILURES
11000	Airframe	×	×	×
12000	Fuselage Compartments	0	×	×
13000	Landing Gear System	×	×	×
14000	Flight Controls	×	×	×
15000	Rotor System	×	×	×
22000	Turbo Shaft Engines	×	×	×
24000	APP (Airborne)	×	×	×
26000	R/W Drives	×	×	×
29000	Power Plant	×	×	×
42000	Electrical System	×	×	0
44000	Lighting Systems	0	*	×
21000	Instruments	×	0	×
57000	Integrated Guidance	×	٥	×
61000	HF Communication System	0	×	×
71000	Radio Navigation	×	×	×
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The 15 system work unit codes described above are derived by consolidating the WUC's shown on the previous page NORM, NORS, SYSTEM FAILURE RANKING CHART to the system level. Ranking in the above chart was determined by the items appearance on two or more of the 3 reports.

Indicates item did not appear on the respective list.

Indicates item appeared on respective NORM, NORS or FAILURE LISTING. × o